



CONSULTING ENGINEERING SERVICES FOR THE CITY OF NORTH YORK - TRANSPORTATION DEPARTMENT

DOWNTOWN PLAN SOUTH OF SHEPPARD AVENUE

ENVIRONMENTAL STUDY REPORT

TRANSPORTATION
INFRASTRUCTURE
REQUIREMENTS

SEPTEMBER, 1996

APPENDICES





APPENDIX A

ENVIRONMENTAL ASSESSMENT STUDY
STATUS REPORT



CONSULTING ENGINEERING SERVICES FOR THE CITY OF NORTH YORK - TRANSPORTATION DEPARTMENT

SOUTH DOWNTOWN SECONDARY PLAN REVIEW

ENVIRONMENTAL ASSESSMENT STUDY

STATUS REPORT

OCTOBER, 1995

PREAMBLE

INTRODUCTION

In January, 1992 Council directed staff to commence with a draft plan for the South Downtown area of the North York Centre. The planning process which followed has been extensive and the road requests in support of the various planning scenarios are documented in this report.

North York has employed a Master Plan approach to address land use and transportation concept for the South Downtown. The approach allows the process requirements of the Planning Act and the Environmental Assessment Act to be considered concurrently which is consistent with recent MOEE recommendations.

This document was originally compiled in a "draft" form in June 1995, and was finalized in a more complete form in October 1995. It is a "status report" which documents the process, the progress and the extent of the work undertaken by Cole, Sherman & Associates up to June of 1995. It was prepared recognizing that North York Council could be directing staff to report on a plan which could have significant change to the plan being proposed at that time.

In view of North York Council's decision in January, 1996 to reduce the scale of development in the South Downtown, this document forms the "Background" to an evolutionary planning process arriving at an Environmental Study Report.

This report is an Appendix to the Environmental Study Report for the Transportation Infrastructure Requirements for the Downtown Plan South of Sheppard Avenue. It has not been endorsed by North York Council as a "stand alone" report, therefore it does not have official status. Further, it cannot be considered a completed environmental assessment study for the transportation infrastructure required in support of the "vision" developments levels.

Planning objectives and principles which guide the land use policies reached in the Secondary Plan act in part as a screen to the systematic analysis and evaluation of transportation alternatives under the EA Act. Master Planning attempts to analyze and evaluate alternative land use and transportation scenarios in parallel, establish a balance, and report them in a traceable manner. Exhibit P.1 outlines the Master Planning process. This ensures that infrastructure improvements are considered at the same time as land use matters providing for a more comprehensive planning approach. The result is that the infrastructure improvements are not predetermined during the land use exercise, but are part of this exercise.

Council's decision to embark on a Master Planning approach for the South Downtown commenced in October, 1992 when Council made a commitment to process the Secondary Plan and Class EA for the South Downtown together as a comprehensive approach. This approach allows for land use, density, policy and undertakings such as roads and transit improvements to be viewed and documented concurrently and to avoid the duplication encountered in sequential processes.

The Master Planning approach hopefully allows the public to understand more fully the relationship and implications of land use and transportation decisions made throughout the process. The resulting Environmental Study Report is a product of the Master Plan approach and may not reflect a typical Class EA process. The Official Plan Amendment, south of Sheppard Avenue, is being processed in parallel with the Class EA. Individuals that are interested in the final outcome of the Master Plan process are encouraged to review the OPA application in conjunction with the Class EA.

MASTER PLAN APPROACH Investigation and Documentation of Alternatives (development scenarios and alternative solutions) Public/Community Review and Input Identification of Master Plan Elements Preparation of Environmental Study Report Preparation of Secondary Plan Continue under Environmental Continue under Planning Act Assessment Act

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1.0 INTRODUCTION

1.1 BACKGROUND

The City of North York and Metropolitan Toronto have consistently promoted the development of a major metropolitan centre along the Yonge Street corridor between Highway 401 and Cummer/Drewry Avenues (see Exhibit 1.1).

During the early 1970s, North York restructured its Official Plan planning areas to separate the City into five Planning Districts at which time District Plan 11 for the Yonge Street area was approved. In 1979, Council adopted an amendment to District Plan 11 (Official Plan Amendment D-11-48) which was confirmed by the Ministry of Municipal Affairs and Housing and the Ontario Municipal Board (OMB) in October 1980. OPA D-11-48 forms the basis to planning in the "North York Centre" and provides a framework for the review of individual development proposals in and around the City Centre.

In 1986, the City of North York separated the City Centre into two distinct planning areas, the "Downtown" and the "Uptown" areas. Subsequently, Council further recognized the "South Downtown" planning area (see Exhibit 1.2). Together, the three planning areas form the "North York Centre" which is a metropolitan urban centre consistent with the planning objectives of Metroplan, (1990).

Approval for the Downtown Secondary Plan were granted by the OMB in March, 1989. Following the approval, the City of North York undertook a separate Schedule 'C' Class Environmental Assessments for the transportation networks. Approval of the Class EA was granted in August 1991.

The Uptown Plan followed an approach whereby the Official Plan Amendment and the required road infrastructure were considered concurrently. That process was consistent with the new requirements of the Class E.A. for Municipal Road Projects i.e. Master Plan.

The Uptown Plan was approved by Council and the Class E.A. for the road network was granted approval in December, 1993.

Since 1992, the City of North York has been engaged in a Master Plan process which will lead to the approval of an Official Plan Amendment and Class Environmental Assessment for the corresponding transportation network. The proposed multi-use

EXHIBIT 1.1

METROPOLITAN CENTRE

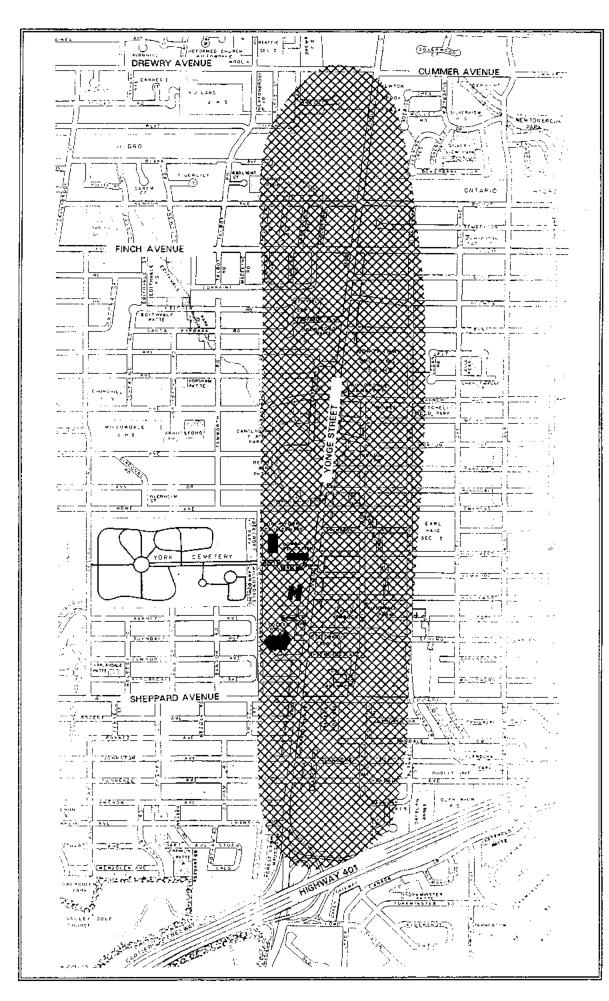
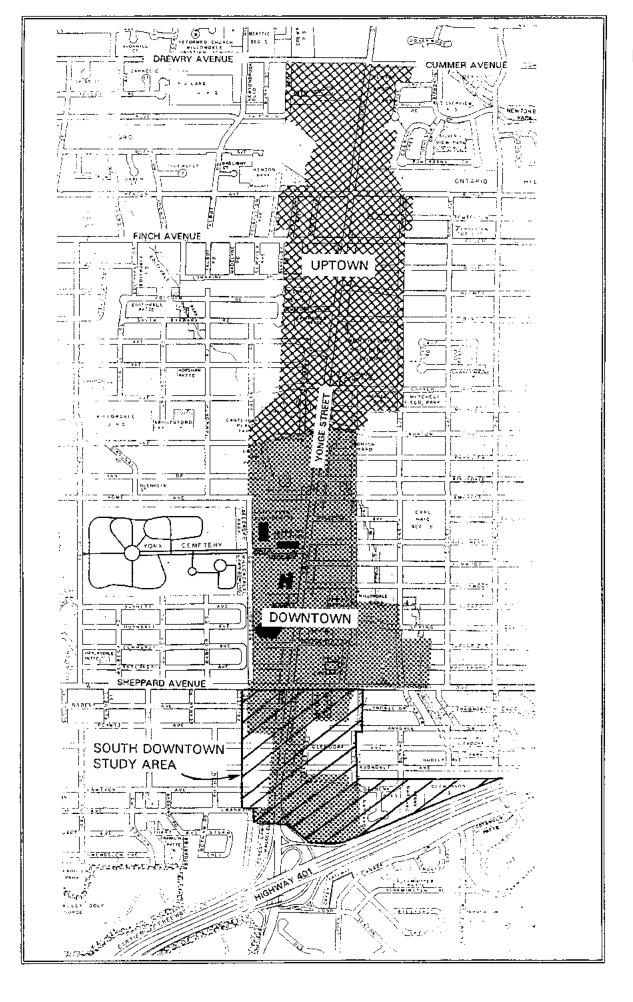


EXHIBIT 1.2



South Downtown area which North York is aiming to achieve cannot be developed without a balanced transportation network. The existing road network is not sufficient to allow carefully planned growth of this area and must be upgraded in conjunction with other transportation plans.

1.2 SOUTH DOWNTOWN SECONDARY PLAN

Subsequent to applications for amendment to the Official Plan and Zoning By-law made on behalf of Westnor Limited to redevelop its lands on the northeast corner of Highway 401 and Yonge Street, Council directed Planning Staff in 1992 to review the lands south of Sheppard Avenue along Yonge Street to Highway 401 (see Exhibit 1.2). The application by Westnor created the impetus for the review, not the need for it.

A Steering Committee was established consisting of several members of Council and the Planning Advisory Committee along with selected Staff from the Planning and Transportation Departments. Guided by the Steering Committee, a number of Technical Committees and the Community Consultation Committee were created.

The Secondary Plan Review consisted of regular meetings of the Technical Committees and the Steering Committee and periodic newsletters to local area residents and land owners. Open houses and public meetings were held to ensure that the process was open to all of those impacted.

The Secondary Plan Review has set as its goal or "Vision" the following statement:

"The conclusion of the South Downtown Secondary Plan review process should result in the development of a Secondary Plan which is sensitive to the needs and desires of all residents and property owners in the area, as well as others traveling through and around the South Downtown. It will provide a gateway to the City Centre, while adding to the vitality and viability of the City Centre as a whole. It will provide for development of a human scale, pedestrian friendly environment, which is compatible with and complements the surrounding residential areas. It will strive to create a community where people will want to live and work."

The South Downtown Secondary Plan Review initially took on two distinct phases or levels of development which have different transportation infrastructure implications. The Phase One Plan would permit development to proceed according to a redistribution of the existing Official Plan density levels without having to undertake

extensive transportation improvements. The second phase (the "Vision") would envisage much higher densities which would require significantly greater transportation infrastructure support. The timing of infrastructure improvements and ultimate phasing of related development would be controlled by financial feasibility.

Through the cooperation of Westnor Limited, Anndale Properties and Crestview Investments, an application to the Canada, Ontario Infrastructure Works (COIW) program to fund some of the transportation infrastructure improvements was made in May 1994. As a result, the Secondary Plan was drafted to set the goals, objectives and planning principles for the ultimate development (vision) for the South Downtown area. The Class EA must then assess the transportation improvements needed to support this development.

The South Downtown Secondary Plan has been reviewed by City Staff and undergone extensive community consultation and input. The details of the Community Consultation will be outlined in Chapter 2. Draft Secondary Plan, completed in September of 1994, incorporates the community input that was received and is now awaiting completion of the Environmental Assessment for the transportation improvements.

1.3 RELATED STUDIES

As part of development of the Phase Two development, the City of North York Transportation Department has undertaken a transportation analysis. Along with traffic analyses that have been completed by Westnor representatives (for local development), this environmental assessment reviewed the supporting documentation when analyzing the most appropriate transportation system to allow for development of the South Downtown area. The Transportation Department's transportation capacity analysis was based on a variety of land use and density scenarios developed by the Planning Department for the Secondary Plan. These scenarios are detailed in Chapter 3.

A study completed by the Transportation Technical Committee and the Transportation Department includes a detailed analysis of the proposed Service Road alignment. Further studies that were used in developing the Secondary Plan include a Fiscal Impact Study, a Retail and Market Analysis and a Ravine and Urban Landscapes Connected Spaces Study.

1.4 PURPOSE OF THE UNDERTAKING

The transportation analysis undertaken in support of the land use Vision demonstrated that significant transportation network improvements are required. The Undertaking must therefore provide the transportation network capacity that is needed for the proposed development levels. When constructed, the Undertaking would satisfy the metro centre planning aspiration of the City of North York and Metropolitan Toronto, secure development potential in the South Downtown area and provide a level of certainty in the minds of those impacted by the change.

1.5 CLASS EA PROCESS AND RATIONALE

The Undertaking proceeded as a Schedule 'C' project under the Class Environmental Assessment for Municipal Road Projects. The rationale for proceeding in this manner is described below.

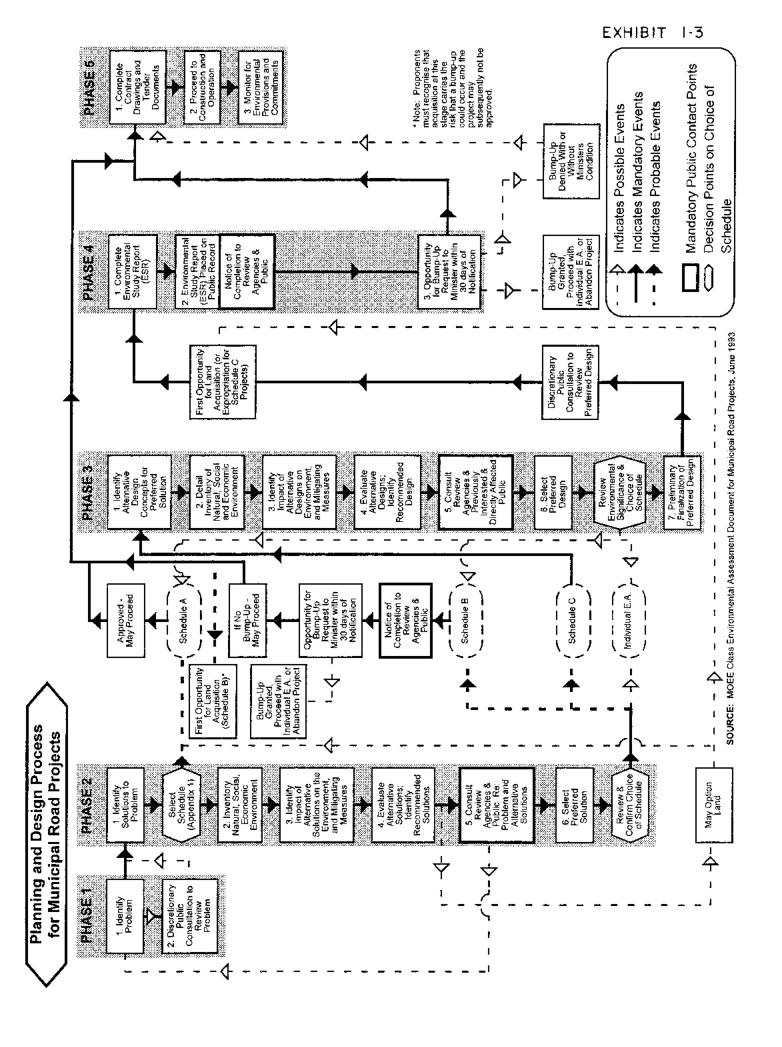
In the initial appraisal of the Undertaking, a number of components were identified as falling within the category of a Schedule 'A' type project, including such elements as the reconstruction and normal maintenance of existing roads. Other elements of the project fell within a Schedule 'B' type project and include such actions as the retiring of existing roads and related facilities to accommodate the overall road network.

More importantly, elements such as the construction of new roads, new intersections, grade separations, road widenings, and the establishment of new rights-of-way fall within a Schedule 'C' type project. Therefore, as this schedule has the more prominent ranking, the scope of this report embodies all elements within Schedules A, B, and C.

The process followed in the planning and design of this Class EA is illustrated in Exhibit 1.3. The chart incorporates steps considered essential for compliance with the requirements of the Act which may be summarized as follows:

- Phase 1 Identifies the problem or deficiency the Undertaking must address.
- Phase 2 Identifies alternative solutions to the problem. Factors to be taken into consideration before selecting a preferred solution include the existing environment, and public/agency review and input.
- Phase 3 Examines alternative designs of implementing the preferred solution. Factors taken into consideration include: the existing environment, public and government agency input, anticipated environmental effects and methods of minimizing negative effects and maximizing positive effects.
- Phase 4 Documentation in an Environmental Study Report (ESR), that includes: a summary of the rationale, and the planning, design and consultation process of the project as established through the above Phases 1 3 (see Section 1.6).
- Phase 5 Completion of contract drawings and documents. The Undertaking then proceeds to construction and operation; during this time construction monitoring for adherence to environmental provision's also carried out.

The planning and design process has been undertaken in such a way as to allow a reviewer to trace easily each step of the process.



1.6 ENVIRONMENTAL STUDY REPORT

One of the key principles of successful planning under the EA Act is:

"to provide clear and complete documentation of the planning process followed, to allow for the "tractability" of decision making with respect to the project."

Documentation of the planning and design process followed in developing a Schedule "C" project is, a mandatory requirement of the Class EA process. Schedule "C" projects, therefore, carry the requirement for the preparation of a formal Environmental Study Report (ESR).

When completed, the City of North York is required to place the ESR with the City Clerk for inspection by the public, government agencies, and private agencies for a period of 30 calendar days. Any person/party objecting to the contents or the conclusions of the ESR is required to bring those concerns to the attention of the City. Should the issues be of such a nature that they cannot be resolved to mutual satisfaction, then the person/party may, in that 30 day period, request the Minister of the Environment and Energy to "bump-up" the project to an individual environmental assessment. The Minister shall consider both sides of the argument and make a decision. If there are no objections to the ESR, the project will proceed.

1.7 STUDY TEAM

As the Master Plan process evolved, a Project Team was formed to guide the Class EA process. Unlike the Downtown and Uptown ESRs, which were completed "in-house" by North York staff, the ESR for the South Downtown is being prepared by an outside consultant, Cole, Sherman & Associates Ltd., on behalf of the proponent, North York. The Project Team consists of representatives from the following:

- North York Transportation Department;
- North York Planning Department;
- North York Public Works Department;
- North York Parks and Recreation Department;
- North York Legal Department;
- North York Property and Economic Development Department and;
- Cole, Sherman & Associates Ltd.

Cole, Sherman has expertise in the fields of transportation and roadway engineering and environmental planning/consultation. This group of experts has led the EA process for the South Downtown area by conducting detailed analysis and public participation programs.

In the areas of noise and air quality assessment, the Cole, Sherman Team retained the services of the following sub consultants:

- S.S. Wilson & Associates (Noise Assessment);
- R.W.D.I. (Air Quality Assessment).

2.0 PUBLIC PARTICIPATION

2.1 INTRODUCTION

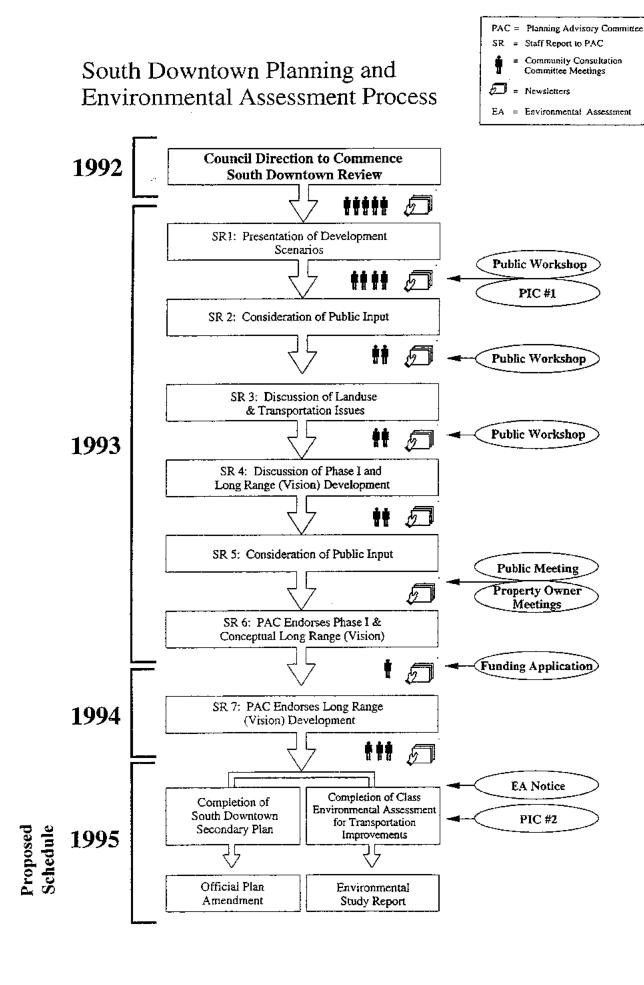
Throughout the Master Planning process, North York has undertaken considerable efforts to obtain public input to both the South Downtown Secondary Plan and Class EA. Since early 1992, North York Staff and Technical Committees have met with various land owner groups and public agencies to elicit feedback as the Secondary Plan review progressed. This process involved the initial Public Information Centre (PIC) required under the Class EA as well as seven (7) public record reports to the Planning Advisory Committee and Council and seven (7) installments of the South Downtown Secondary Plan Review newsletter that were mailed to all stakeholders (see Exhibit 2.1). Beginning in January of 1995, ten (10) additional stakeholder meetings were held to obtain valuable input. The second PIC, as required by the Class EA, was scheduled for March of 1995, however the PIC was postponed until further notice.

The overall objective of the consultation process is to involve as many stakeholders in an interactive process of goal setting for the South Downtown Plan. This has included involvement in the Secondary Plan process as well as the Class EA. Combined, this input forms the feedback for the Master Planning process. Other techniques used included the formation of the Community Consultation Committee which was made up of local area representatives and provided a critical link between area residents/landowners and the project team guiding the Master Planning process. Focus groups or workshops were also held and attended by City Staff and Cole, Sherman. These workshops acted to give more detailed information on specific issues from the general surveys that were distributed at the first workshops. Public input was considered to be essential to establishing the policies of the South Downtown Secondary Plan.

2.2 STAKEHOLDERS

The following is a general listing of those interested in or impacted by the South Downtown Secondary Plan.

- Municipality of the City of North York
- Metropolitan Toronto
- Ministry of Transportation
- Toronto Transit Commission
- Province of Ontario- Ministry of Transportation, Ministry of Municipal Affairs, Ministry of the Environment and Energy



- North York Board of Education and the Metropolitan Separate School Board
- Residents of Wards 8, 9, 11, Central Willowdale Ratepayers Association, Lansing Community Association, Yonge Ridge Homeowners Association, Avondale Ratepayers Association, Residents of the "Transition" and Redevelopment" areas
- Developers
- Land owners
- Workers in the area using the transportation network
- Utilities-Bell, Hydro, Consumers Gas etc.
- Metropolitan Toronto and Region Conservation Authority

2.3 CONSULTATION PROCESS

As described previously, the overall consultation process consisted of public meetings, focus groups, newsletters, Community Consultation Committee and regular staff reports. The following briefly outlines the various components that made up the public participation process. Summary tables have been created to document more specific comments received during the community input process.

- Seven (7) public Staff reports to the PAC and Council. Each elicited feedback from interested parties.
- In view of the scope and complexity of certain components of the study area, seven (7) "Technical Committees" were formed to focus on the general principles of specific issues.

These Technical Committees included the following:

- Transportation
- Servicing
- E.A.
- Land Use and Urban Design
- Parks and Open Space
- Economic and Finance
- Community Consultation

The Committees met on a rotational basis approximately once every six weeks. Minutes of the meetings were forwarded to interested parties. However as the review evolved, and certain issues overlapped the mandate of several committees, the need for the individual committees came to closure when the "project" focused on one general concept and the various elements "meshed" together.

- Seven (7) Newsletters were sent to area land owners and other stakeholders summarizing the Staff Reports and the Technical Committee meetings. These also served to give notice of public meetings, open houses and workshops.
- The workshops and open house meetings were specifically arranged to inform the public and elicit input into the process. Numerous other public PAC meetings were held to receive and discuss the Staff Reports as they were completed. These meetings were well notified and attended by stakeholders.
- Ten (10) stakeholder meetings were held with specific interests to obtain more in-depth information that may not have been shared during larger public meetings.

Note: From the initiation of the Secondary Plan Review Process, all correspondence, notice and minutes of meetings included information on the proposed transportation improvements and the requirement for a Class EA.

2.4 MEETINGS/WORKSHOPS/PUBLIC INFORMATION CENTRES

Open Houses, Work Shops and Public Information Centres (PICs) were held on the following dates:

Workshop January 30, 1993 PIC February 18, 1993

Open house May 20, 1993 Workshop June 5, 1993

Community Meeting September 27, 1993
Public meeting October 27, 1993

Feedback and comments received during and as a result of these meetings were analyzed and addressed by Staff and discussed in subsequent Staff reports to the PAC. These public meetings included information on the proposed transportation infrastructure improvements so that they constitute part of the EA public participation process.

Stakeholder meetings were held with the following to introduce the alternative roadway design concepts which would be considered in the Environmental Assessment Study:

Avondale Ratepayers	January 25, 1995
Transition Areas Residents	January 30, 1995
Yonge Ridge Homeowners	February 1, 1995
Central Willowdale Ratepayers	February 7, 1995
Ward 8 Ratepayers	February 20, 1995
Redevelopment Area Residents	February 23, 1995
Marathon Realty	January 17, 1995
Westnor Properties	January 23, 1995
Anndale/Crestview	February 6, 1995
Business Interest Group*	February 13, 1995

^{*}Includes; North York Board of Education, Seneca College, Petro-Canada, Premium Properties, Colonial Life.

Other business interests that were contacted directly regarding the study include: First Professional Management, Gemeiner/Irez, Sunlife, Ivanhoe Developments.

This input was used in concert with the previous public consultation feedback to develop criteria of evaluation to be used in assessing various alternative infrastructure improvements being considered by the City.

2.5 Issues/Concerns

The following lists some of the concerns raised during the overall public consultation process;

- Alignment of the Service Road,
- Transition zone, redevelopment pressure,
- Buffering from Service Road alignment,
- Density and height along Yonge Street and Sheppard Avenue and relation to stable residential areas,
- Access to neighbourhoods without excessive through traffic,
- Community Cohesion,
- Angular planes (%),
- Property values,
- Noise
- Air Quality

- Study Area boundary,
- Appropriate mix of land uses (residential/commercial),
- Appropriateness of regional retail component,
- Urban design guidelines built term, massing and phasing,
- Open space and parkland,
- Visual impact of Flyover.

These concerns were raised during open houses and workshops but also through surveys, comment sheets, petitions, form letters and private letters. Each was addressed by Staff directly as well as being summarized and responded to in Staff Reports to the PAC and in subsequent Newsletters.

Exhibit 2.2 outlines the detailed input gained throughout the stakeholder meeting process as part of the Class EA study. These comments were considered when developing evaluation criteria for the infrastructure improvements.

NORTH YORK SOUTH DOWNTOWN CLASS ENVIRONMENTAL ASSESSMENT HIGHWAY 401 / YONGE STREET SERIES OF WORKSHOPS ISSUES AND CONCERNS

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ISSUE/CONCERN	COMMENTS	ISSUE/CONCERN	COMMENTS
1) NOISE	 single family homes that do not redevelop will be heavily impacted by noise generated by service road noise will change the character of old established neighbourhood transition area homes should be protected like "stable residential" if mitigation such as berms, walls etc. cannot be provided, more landscaping is requested 12 metre buffer is inadequate if noise impact is beyond Provincial standards, we may request bump up would prefer linear park along the road more trees and landscaping may be better than distance want to see noise isobar mapping for the area to compare impact to existing Hwy. 401 noise will be generated from flyover and tunnel under Yonge Street flyover will cause echoing in ravines south Hwy. 401 at 12 lanes is already too noisy, flyover will make it worse 	2) AIR QUALITY 3) TRAFFIC	 4-lane road throughout neighbourhood will decrease air quality for temaining single family homes not enough buffering address air quality in analysis where do fumes go from the flyover major 4 lane road with heavy traffic through the middle of our neighbourhood pedestrian safety residents do not want or need change to roads and traffic - this is all for the developers do developers really need roads and traffic to go through our neighbourhood restict 401 connection to Westnor site do not want infiltration of Hwy. 401 traffic through our area link to Hwy 401 will make the service road very busy we want to maintain access to Yonge/Sheppard 60% modal split seems arbitrary, more research to support it should be done do not signalize Bales and Avondale intersection neighbourhood accessibility is critical, want to be able to get in and out of area pedestrian access to Yonge Street and area amenities is why we live in the Avondale area

NORTH YORK SOUTH DOWNTOWN CLASS ENVIRONMENTAL ASSESSMENT HIGHWAY 401 / YONGE STREET SERIES OF WORKSHOPS ISSUES AND CONCERNS

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ISSUE/CONCERN	COMMENTS	ISSUE/CONCERN	COMMENTS
3) TRAFFIC (contd)	 consider more specialized pedestrian friendly amenties such as walkways cross walks, for access and safety what about the termination or through 		 rush hour traffic is a concern concerned Service Road will become a speedway
	 traffic generation assumption of 1,200 sq.ft. units is too large, likely they will be smaller and therefore more abundant. Limit density by number of units as well 	4) PROPERTY VALUE	 density assigned is not enough to provide for viable re-development once. Scryice Road is built real estate agents cannot sell our homes now due to uncertainty. We cannot leave
	as sq.ft. • show worst case traffic scenario at full build out to account for uncertainty of timing		 home beside alignment that is not expropriated looses value transition area homes value plummets increased density is not enough
	 consider/look at decking of Yonge St. concerned about potential for increase in cars/lane/hour (700) as used in uptown and downtown studies southbound traffic on Yonge Street from northern area will still cause 		 compensation may want to stay in single family residence for a long time, property value will decline over whole area do not want to be stuck with decreasing home values
	·-		want to remain pleasant and inviting place to live transition area should be east of Service Road and treated as stable residential opposed to expropriation
	moves very quickly and has increased in volume making Lord Scaton congested • traffic coming north uses Old Yonge to by-pass Yonge Street traffic, this will not change	5) TIMING OF CON- STRUCTION	 long time until build these roads and see development. This leaves residents with a lot of uncertainty in the interim if COIW input does not come Ibrough, go with Phase I only. With COIW, must
			come into our area sooner. We are not ready to sell. • We need to know when the road will go through our houses.

NORTH YORK SOUTH DOWNTOWN CLASS ENVIRONMENTAL ASSESSMENT HIGHWAY 401 / YONGE STREET SERIES OF WORKSHOPS ISSUES AND CONCERNS

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ISSUE/CONCERN	COMMENTS	ISSUE/CONCERN	COMMENTS
6) FINANCING 7) PROCESS	 we do not want to pay for the infrastructure through realty taxes. It is the developers who benefit, they should pay if COIW financing is not available, ESR remains useful for 5 years roads can be completed in functional section as development occurs through development changes what is the process and where else do we get to have input what constitutes an objection how do we apply for a "bump up" request explain staging of analysis do not look at Tradewind as the only eastern alignment if it goes over Marathon's land since that is prohibitively expensive. Another route further east would not incur this cost and might be more attractive should evaluation criteria be weighted solution should come first (i.e., alignment) then assessment of the cost if sudy is bumped up, can we drop it due to cost? comments can be made after PIC #2 and newsletter do not turn this into a popularity contest (i.e. more people against Midblock 	8) CHANGE IN LAND USE PATTERNS	 would like a 3D model at PIC #2 to make proposed changes clear want the EA and the road pattern reviewed every 5 years similar to the OPA fear Westnor is driving this process request additional meetings after evaluation, however, hefore a recommendation comes forward at PIC #2 access to Lord Seaton area is difficult, address this in the EA study we want certainty from OPA so we can plan we do not want to be a transition area, want to be considered stable residential. Highest and best use may be single family residential not necessarily opposed to development, we want to ensure compatible development. Do not want development development area bout to meet any alterations to Stanly Park (Poyntz & Beecroft) concerned about homes that are in the loop of the Service Road (redevelopment area) if decide to stay single family residential want to ensure road system accounts for proper land use mix (either 50/50 or 60/40 residential/commercial) close Bales Ave. for redevelopment

NORTH YORK SOUTH DOWNTOWN CLASS ENVIRONMENTAL ASSESSMENT HIGHWAY 401 / YONGE STREET SERIES OF WORKSHOPS ISSUES AND CONCERNS

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ISSUE/CONCERN	COMMENTS	ISSUE/CONCERN	COMMENTS
9) SERVICE ROAD ALIGNMENT Transition Area	 prefer Tradewind to Mid-block so it does not go through our neighborhood 	10) 401/YONGE STREET INTERCHANGE	 flyover ramp will cause tremendous visual disruption north and south along Yonge Street this is the gateway to North York. Flyover
Avondale	• prefer Mid-block to Tradewind. Consider Bales Avenue again so the Service Road is as far away from our neighbourhood as possible		• fear that flyover with 1 lane and 2 wide shoulders could become 2 lanes if future demand warrants
	 Tradewind should not be an alternative. Will fight this alignment want a minimum of 46 meters from the stable residential to the pavement of the Service Road 		figure or under a stridge where it doe
Central Willowdale Lansing	 do not want E-W link to continue through to Bayview or up to Sheppard concerned that E-W link in the uptown may be a long time before it is completed and will hinder the effectiveness of the Service Road in total 		 Hyover will come into Yongeridge neighbourhood without buffers perhaps lower cost to upkeep tunnel may offset construction cost flyover will ruin the gateway effect of the Yonge/401 interchange could Lord Seaton traffic and EB ramp be separated?
	 concerned about west alignment curve to protect heritage site want as little infiltration into neighbourhood as possible through 	11) SERVICING	 concern that there is not enough servicing capacity in the North York sanitary trunk sewer
Yongeridge	road loops and closure • realign Beecroft west to Hwy, 401 as a ramp	12) NATURAL EN- VIRONMENT	 criteria for natural environment only accounts for existing vegetation, not for making it better through this process
Rcdevelopment Area	 prefer Tradewind Alignment, Mid-block severs our neighbourhood community 		

3.0 PROBLEM STATEMENT/NEEDS ASSESSMENT

3.1 Introduction

The Class Environmental Assessment for Municipal Road Projects asks proponents to identify and describe the problems or opportunities which the project (undertaking) expected to address. In this instance, the transportation network capacity/deficiency may or may not be obvious to the public, nevertheless it is necessary to document the rationale which leads to a conclusion that certain improvements are needed.

As stated in Section 1.4, the purpose of the original undertaking was to provide the transportation—network capacity that is needed to support the development aspirations of the South Downtown Plan.

There are three "rationales" which demonstrate the need for the Undertaking:

i) The "Transportation Network Capacity" Rationale

The existing transportation network contains an integrated highway, arterial road collector road, local road and transit system. When viewed as whole, the transportation system will not have the capacity during rush hour periods to adequately support the development associated with the South Downtown Secondary Plan.

ii) The "Planning" Rationale

Municipal planning undertaken by both the City of North York and the Municipality of Metropolitan Toronto recognizes the need for development of a metropolitan centre in North York. The studies and official plans undertaken in this regard all recognize the need for this project.

iii) The "Cost Sharing" Rationale

Improved access to North York Centre will support and provide an impetus for the economic growth and commercial activity associated with the continued development of a city centre. Funding for the greater undertaking will require significant support from the private sector partners which may or may not exist in the future.

3.2 DESCRIPTION OF THE PROBLEM

3.2.1 Transportation Network Capacity Rationale

The Transportation Department of North York is responsible for monitoring the transportation patterns in the North York Centre. An annual cordon count of traffic in and around this area is used to monitor the changes in the traffic patterns. In addition to the cordon count program, a biennial survey of employee travel patterns assists in determining changes of the mode of travel, distribution, etc.

The existing components of the transportation network are illustrated in Appendix A-Traffic Study and are described below. Details of all transportation analysis are outlined in Appendix A.

<u>Public Transit</u> - The Toronto Transit Commission (TTC) Yonge Subway is the backbone of the North York Centre transit system. It supplies a vital public transit service for employees, customers, clients and the residential population as a whole. Development has generally been approved to take advantage of this major transit facility. The TTC Sheppard Station provides the most immediate access to the South Downtown area.

The TTC bus service particularly on Sheppard Avenue is another integral part of the public transit system, albeit, presently lacking the passenger capacity to accommodate the demand. Developments focusing towards the Yonge/Sheppard node rely on this service.

The Transportation Analysis for the South Downtown Plan, as prepared by North York, assumed a future <u>overall average</u> modal split of 60% in favour of public transit, which includes a Sheppard Subway. (See Appendix A-Traffic Study)

<u>Highway and Expressways</u> - Yonge Street provides access to the provincial highway system. Highway 401 is a major east/west distributor of medium to long distance trips and provides the necessary link to the regional expressway system. During certain periods within the established rush hours, access to Highway 401 is reaching capacity.

<u>Arterial Roads</u> - The primary arterial roadways within the Study Area are Yonge Street and Sheppard Avenue. These major roadways are within the jurisdiction of Metropolitan Toronto.

Yonge Street is the north/south artery of the South Downtown and is recognized as North York's main street. It is the critical segment of the North York Centre road network and has been traditionally recognized as an accepted route south to the Central Business District of Toronto, and its interchange with Highway 401 provides access and attracts traffic to the Provincial highway system. Much of the traffic is neither generated by nor destined for the South Downtown, and was identified in the Transportation Analysis as background traffic. Background traffic restricts, significantly the free movement within the South Downtown. During certain periods within the established rush hours, the arterial roadway is reaching capacity.

Sheppard Avenue is also an integral part of the road network. In 1991, Metropolitan Council directed the preparation of an ESR to address the need to widen this roadway to six lanes. Approval was finalized in 1992.

Notwithstanding the available capacity on the collector roads and local roads, the transportation network as a whole is an interlocking system and must be assessed in its entirety.

<u>Collector Roads</u> - The collector road network are within the jurisdiction of the City of North York. North York's monitoring program shows that the collector road network is currently not operating at capacity even during rush hours.

<u>Local Roads</u> - North York's monitoring program indicates that, generally, the traffic patterns on the local road network have been stable over time.

The analysis of transportation requirements conducted by the City in relation to the development of the Downtown and the Uptown Plan, determined that the assumed road and transit networks serving them would not have sufficient capacity to accommodate additional development.

3.2.2 Planning Rationale

While the specific planning policies for the South Downtown falls within the jurisdiction of the City of North York, the Official Plan of Metropolitan Toronto sets out the broader planning principles and policies of the urban structure which include such elements as population, household and employment activities, and it commits Metropolitan Toronto to the coordination of the physical infrastructure necessary to permit forecasted growth. This infrastructure includes the Metropolitan transit system, the Metropolitan road system, water supply and sewage treatment facilities and the Metropolitan open space system.

The Official Plan of Metropolitan Toronto obliges the local municipalities to be responsible for the designation of land uses, zoning and development control. The Metropolitan Planning Department reviews the local planning policies and their implementation to ensure conformity with Metroplan.

3.2.2.1 Metropolitan Toronto - Metropolitan Centre Planning

In 1972, Metropolitan Toronto initiated a program which consisted of a series of background planning policy reports and formed the basis for the Official Plan for Metropolitan Toronto. The program was known as "Metroplan".

In May, 1976, a report entitled <u>Concept and Objectives</u> identified a number of goals and policies for the development for the urban structure. The policies included the development of Metropolitan Centres located along rapid transit facilities.

In October 1978, the Planning Committee of the Municipality of Metropolitan Toronto presented a document known as the <u>Plan for the Urban Structure: Metropolitan Toronto</u>, which was adopted by Metropolitan Council on January 15, 1980, and approved by the Ministry of Housing on October 10, 1980. That plan is based upon a multi-centred urban structure and it identifies North York Centre as one of the Major Metropolitan Centres.

A Major Centre is multi-functional in land use, compact and pedestrian oriented in its internal organization and design, and intensive in its development relative to those areas which are not centres.

The designation of the South Downtown (part of the North York Centre), for redevelopment consistent with these criteria is therefore, in accordance with the goals, aims and policies of the Metropolitan Toronto Official Plan.

Recently, a new draft of Metroplan has been prepared. That plan continues to recognize the importance of a multi-centred metropolitan structure with urbanization occurring primarily in the Major Metropolitan Centres, including North York.

3.2.2.2 North York - City Centre Planning

In 1976, the North York Department of Planning and Development prepared the framework for future development in North York by developing planning policies. The proposal to establish a "centre" in the Yonge Street corridor between Highway 401 and Cummer/Drewry Avenues ("the Yonge Street Centre") was specifically identified. The preparation of these planning policies was in keeping with the concept and objectives of the planning policies being developed by Metropolitan Toronto.

Subsequently, the <u>Yonge Street Redevelopment Study</u> report was prepared. It described many of the constraints and/or advantages of attempting to create a Yonge Street "Centre" (North Yonge Centre). The report was first considered by the North York Planning Board in June, 1977, and by Council in July, 1977. In July, 1977 a joint meeting of the Planning Board and Council conducted a hearing and presented the report to the public which can be considered as the start of a lengthy and complex planning process in respect of the redevelopment of the North York Centre. This process has, at all stages, included extensive public consultation and participation.

In February 1978, a report entitled <u>Yonge Street Centre Strategy</u> was presented to the Planning Board and recommended policies which attempted to settle areas of conflict while promoting the desired planning goals. In September 1978, Council directed that an official plan amendment be prepared to address the planning goals and policies

for the North York Centre based on the conclusions of the Yonge Street Centre Strategy. This gave rise to District Plan Amendment D-11-48 as previously mentioned, which formed the foundation for the redevelopment of the North York Centre.

The approval of this District Plan Amendment was subject to a five year review. This review was initiated in April of 1983, and included recommendations to expand the limits of the North York Centre and to increase maximum densities on a number of sites.

In January 1985, a transportation analysis conducted by Metropolitan Toronto, found that the proposed amendments to the plan would necessitate a "ring" road system from Poyntz Avenue to Cummer Avenue among other road improvements to facilitate traffic circulation and access. The analysis suggested that the ring road could serve one of two purposes. It could be used either to provide an arterial function (thus freeing Yonge Street to operate as an arterial road) or to provide a collector function. The analysis recognized that both concepts had merit, but concluded that the former should be preferred, because it would be easier to implement.

The transportation analysis concluded, more specifically:

- the predicted traffic volumes associated with the development of the North York Centre indicated a specific need for a transfer of traffic, particularly shorter distance trips destined to the Centre from Yonge Street to a parallel route;
- (ii) as traffic volumes increase, Yonge Street would not be able to support additional direct site access and maintain its role as an arterial road; and
- iii) if the ring road was not implemented, severe congestion on Yonge Street and the connecting arterial roads would promote inappropriate and extensive infiltration of the adjacent residential neighbourhoods.

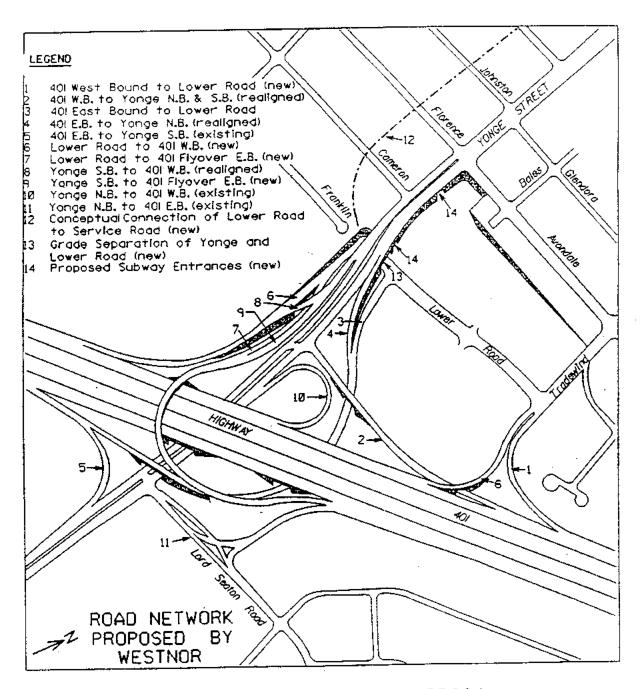
The scale of the proposed road improvements provoked considerable reaction from the residential communities which resulted in Council directing that the North York Centre Plan be separated into two plans, the "Downtown" Plan and the "Uptown" Plan.

3.2.2.3 Developing the South Downtown Secondary Plan

Council first directed staff to commence drafting a plan for the South Downtown Area in January of 1992 in order to complete the North York Centre initiative and in response to the development proposal made by Westnor Limited on lands previously recognized as the McLean Hunter site.

Staff completed the background, research, committee and community consultation and documentation for the first of seven (7) reports in November 1992. Report Number One outlined the land use, the density and transportation network capacity scenarios generated by discussions with the committees and the conceptual work of Westnor's Transportation Consultant, BA Consulting Group. Planning staff initially developed seven (7) land use scenarios with varying densities and land use splits between residential and commercial uses. As part of the Master Planning Process, the Transportation Department, examined minimum, medium and maximum transportation capacity scenarios based on the seven (7) conceptual secondary plan options. Because of the number of combinations of conceptual secondary plan options, three possible scenarios were initially chosen as the basis for further study. Evaluation for each of all three scenarios assumed a 50/50 split between residential and commercial land uses, and a 50% modal split. The evaluations were also based on a road network shown in Exhibit 3.1 as prepared by BA Consulting Group for Westnor. It should be noted that for analysis purposes, it was considered acceptable if any component of the network was over capacity by less than 5%.

The three initial transportation capacity scenarios and a subsequent fourth (average option) are presented below:



INITIAL ROAD NETWORK PROPOSAL

1. The Maximum Scenario

The Maximum Scenario included approximately 1,250,000 m2 (13.5 million square feet) of gross floor area, representing a Floor Space Index (F.S.I.) of 4.5 over the entire area. It should be noted that this gross floor area is in addition to gross floor area permitted by the existing Official Plan.

In this scenario, all parallel routes were over capacity. Even though they were over by less than the 5% acceptable limit, this scenario was not pursued further because <u>all</u> parallel routes were over capacity.

2. The Medium Scenario

The Medium Scenario included approximately 700,000m² (7.5 million square feet) of gross floor area, representing a variation in Floor Space Indexes across the study area from 1.5 to 4.5 As with the maximum scenario, this gross floor area is in addition to that currently permitted by the Official Plan. In this scenario, all routes were within acceptable capacity limits with room to maneuver.

3. The Minimum Scenario:

A Minimum Scenario of 580,000m² (6.2 million square feet) of gross floor area was also evaluated. This evaluation revealed that only Yonge Street was slightly over capacity.

4. The Average Scenario

Due to the amount of maneuvering room available in the Medium Scenario, a fourth scenario based on 75% of the Maximum Scenario was also evaluated. It included approximately 900,000 m² (9.7 million square feet) of gross floor area and represents the maximum capacity that the road network could support, at a 50% modal split. As with the Medium Scenario, all routes were within acceptable limits of capacity.

Further analysis of the Average and Maximum Scenarios, assuming a 60% transit modal split for the South Downtown, revealed that the Maximum Scenario at 60% of modal split had similar results to the Average Scenario at a 50% modal split. A 60% modal split could be achieved through the realization of a Sheppard Subway line.

Staff also analyzed the Maximum and Average scenarios with and without the southbound Tradewind to westbound Highway 401 ramp. The Maximum Scenario without this ramp put some components of the road network over capacity and Sheppard Avenue, both east and west of the North York Centre, over capacity, which indicated that the diverted trips cannot be managed. This was the case in each scenario tested. It has therefore been concluded that this ramp is crucial.

3.2.2.4 Conclusion of the South Downtown Capacity Analysis

North York's Capacity Analysis set the parameters within which detailed land use and density evaluations could be undertaken. The maximum gross floor area figure of 900,000 m² (9,687,836 square feet) presented by the Average Scenario was considered to be the ceiling for further consideration and would require certain network improvements as previously discussed.

Staff indicated that a subway station at Avondale Avenue and Yonge Street would be desirable if a high density commercial development close to Highway 401 is to be pursued. Concerns were raised that the subway station in combination with a major "node" or focus south of Sheppard Avenue could detract from the existing focus between Sheppard Avenue and Park Home/Empress Avenues. The south entrance to the Sheppard Station is at the north end of the Proctor and Gamble building, two blocks from the Westnor site. Staff concluded that, at this time, Council not pursue this new station.

Once the Average Scenario was established as the maximum and optimum land use and transportation option, North York began its elicitation of public input.

Having completed Report Number One for Public review, North York requested that public comment on the scenarios be obtained. A public workshop was held on January 1993 and an official Public Information Centre in February, 1993 to provide the public an opportunity to see the options and give feedback to staff.

In March, 1993 staff presented Report Number Two to the PAC which detailed all of the comments received during the public consultation process. Comments, where appropriate, were integrated into the conclusions of Report Number One.

Report Number Three was brought before the PAC in May, 1993 which narrowed the alternative transportation network based on comments received from the public and the Technical Committees. An open house and public workshop were held in May, 1993 and June, 1993 respectively to obtain feedback on the preferred option set out in Report Number Three. The results of these public meetings gave rise to Staff's Report Number Four which was presented to the PAC in July, 1993. Report Number Four outlined the Phase One Plan and the Vision (as previously outlined) for the land use and transportation infrastructure for the South Downtown area.

3.2.3 The "Cost Sharing' Rationale

During the preparation of Report Number Four concern was raised over the financial feasibility of the ultimate transportation infrastructure for the Vision. As a result, in Report Four, Staff recommended that only the Phase One Plan be pursued with a view to completing the Vision when funding could become available.

In October, 1993 the PAC received Report Number Five which outlined the responses regarding the recommendations of Report Number Four to proceed with the Phase One Plan only. A public meeting of the PAC was held in October, 1993 to receive public submission regarding Report Numbers Four and Five. At this meeting, members of the PAC endorsed the Phase One Plan and directed staff to meet with the Technical Committees, Community Consultation Committee and property owners. These meetings were held in November 3, 1993.

In December of 1993 the PAC received and endorsed staff Report Number Six which discussed densities for the Transition Areas using the Phase One Plan.

In May, 1994 Westnor, Anndale Properties and Crestview Investments offered to contribute the municipality's share of a Canadian Ontario Infrastructure Works project should an application be successful. Council accepted such offer, and a formal COIW application was submitted for the transportation infrastructure improvements required to support the long term Vision for the South Downtown Secondary Plan.

Finally on July 13, 1994 the members of the PAC received and endorsed the recommendations of Report Number Seven which suggested that the long term Vision for the area be pursued assuming that funding would be available through the COIW program.

3.2.4 The Problem Statement Summary

For purposes of the greater undertaking, the Problem Statement was prepared and presented to the stakeholder groups as follows:

"A road network has been developed to support the existing and future development level in the North York Centre as defined in the current Official Plan. However, this network will not have sufficient capacity to support auto traffic that will be generated by future development in the South Downtown as proposed in the Draft South Downtown Secondary Plan."

The comments received during the presentation of this problem statement to the public indicated that Stakeholders generally agreed with the statement and the fact that future development proposed in the Draft South Downtown Secondary Plan could not be supported with the proposed road network. Constituents did not necessarily agree with the densities of development being proposed, however, did agree that some level of development is appropriate for the south downtown and that infrastructure improvements are required to lessen the impact of such development on the surrounding neighbourhood.

4.0 EXISTING AND FUTURE CONDITIONS

4.1 BACKGROUND

The establishment of an existing and future baseline environmental condition is integral to the prediction of net environmental effects. By definition, the description of the environment must consider natural social, economic and cultural features. The existing and expected future conditions within the study area are used as baseline conditions from which to project the likely impacts of various roadway alignments including socio-economic factors and the character of the existing development. Certain socio-economic elements have been reviewed throughout the South Downtown Secondary Plan process, however, this report looks at the specific impacts of the transportation infrastructure improvements on the neighbouring properties.

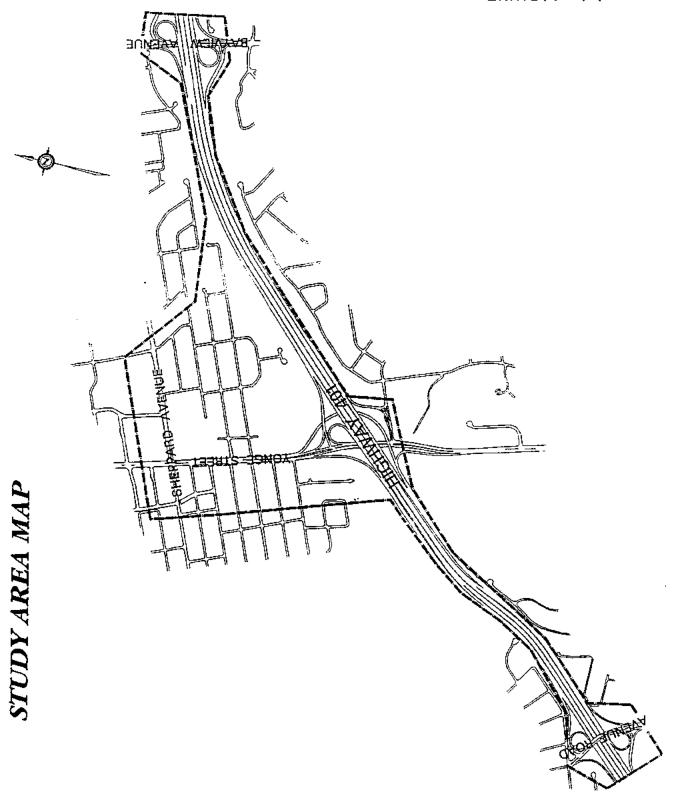
4.2 STUDY AREA

For the purposes of the South Downtown Secondary Plan and this report, the overall study area is depicted in Exhibit 4.1. The boundaries of this study area have evolved through numerous community consultation and feedback sessions with area landowners. As it is currently delineated, the study area encompasses the "Vision" of the South Downtown Secondary Plan, including all areas that might potentially be affected by the Plan, and the roadway infrastructure alternatives.

4.3 THE NATURAL ENVIRONMENT

With exception to the west Don River Tributary, little remains of the natural environment endogenous to the study area. The Draft Secondary Plan endeavors to rectify this situation by requiring extensive buffering and linked park open space throughout. Also, through future development applications, the City will secure open space to contribute to the natural environment.

The valleyland associated with the West Don River tributary that flows under the Hoggs Hollow bridge is the most prominent natural environment found within the study area. It appears that the Hoggs Hollow bridge west to Avenue Road is required to be widened in order to accommodate the new ramping system to Highway 401 from Yonge Street. Impacts to the valleyland under the Hoggs Hollow bridge may occur if this improvement is undertaken.



The Metropolitan Toronto and Region Conservation Authority, (MTRCA) provided flood plain mapping for the Hoggs Hollow area. Exhibit 4.2 shows the limit of the floodline under the Hoggs Hollow bridge between Yonge Street and Avenue Road. Physical obstructions are not permitted within this zone and will place certain restrictions on the construction alternatives for the bridge design.

The MTRCA also provided the following information with respect to surficial geology, recreational uses and valley vegetation:

Surficial Geology: The majority of the Yonge Street/Highway 401 area is covered by Till; a silt to clayey silt (Halton, Kettleby, Sunnybrook, Meadowcliffe). The area immediately below the Hoggs Hollow bridge closest to the river bed is Alluvium which consists of sand, silt, clay and muck including Pleistocene Alluvium. Surrounding the flood zone, the earth consists of Undifferentiated Glacial and Interglacial Deposits. Exhibit 4.3 delineates surficial geology zones.

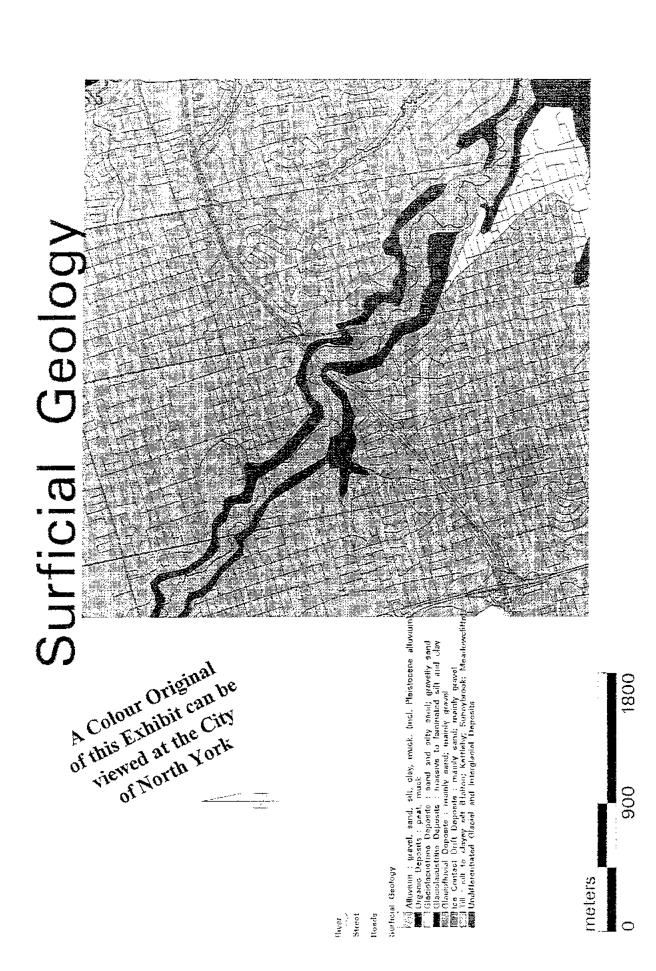
Valley Vegetation: The Hoggs Hollow valley corridor contains a variety of vegetation types including; manicured, meadow, successional and woodlands. There are no significant wetland designations or environmentally significant sites. Exhibit 4.4 shows the limits of vegetation types within the Hoggs Hollow bridge area

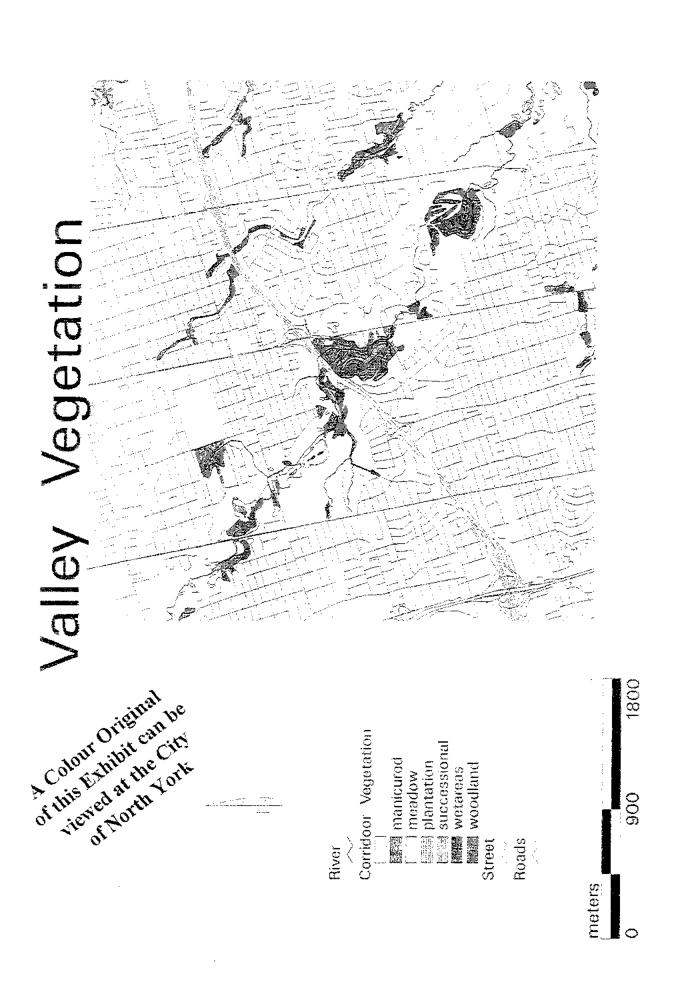
Recreation: Exhibit 4.5 provides a view to the various recreational uses in the Don River Valley. The Hoggs Hollow bridge area is entirely used for the Don Valley Golf Course which is a public course owned by the Municipality of Metropolitan Toronto.

4.4 THE SOCIO-ECONOMIC ENVIRONMENT

4.4.1 Existing Land Use

The South Downtown area is characterized by a mix of low density residential housing, large commercial developments, institutional uses and strip retail businesses associated with Yonge Street activity. While







primarily residential in nature, it is a vibrant and changing neighbourhood, full of viable enterprises that attract workers, users and residents to the area. However, upon examination, there is evidence of instability in the South Downtown, specifically associated with Yonge Street.

There are a number of absentee landlords who own residential property in the vicinity of the South Downtown. This suggests that the owners could be speculating on the possibility of seeing a change in land use designations in the next few years. The incidence of absentee landlords seems to decrease with distance from Yonge Street, suggesting that this area is in fact in transition and should be considered for residential intensification and redevelopment. Moving further away from Yonge Street, the residential area becomes more stable with residents of the area who have displayed less affinity for transitional movement.

Along Yonge Street there exist a number of large developments that provide a commercial element to the South Downtown. These include: the Proctor and Gamble site (.73 ha, 1.8 ac), the North York Square site (1.21 ha, ac), the Warner Bros. building (.28 ha, .69 ac) and the National Grocers / Westnor site (9.47 ha, 23.4 ac.) being the best examples. These developments and others commercial businesses along Yonge Street, south of Sheppard Avenue provide employment for the South Downtown and the City of North York.

Yonge Street, south of Sheppard Avenue also hosts a variety of lower density mixed use developments such as the Willowdale Plaza (Miracle Food Mart, National Sports), a funeral home, a mausoleum, several gas stations, fast food and sit in restaurants and a number of other convenience, commercial and retail businesses.

There are a number of vacant parcels of land, some of which are under construction and others that have applications for redevelopment pending. These "special sites" are detailed in section 4.4.2, Proposed Development-Special Sites.

4.4.2 Proposed Development-Special Sites

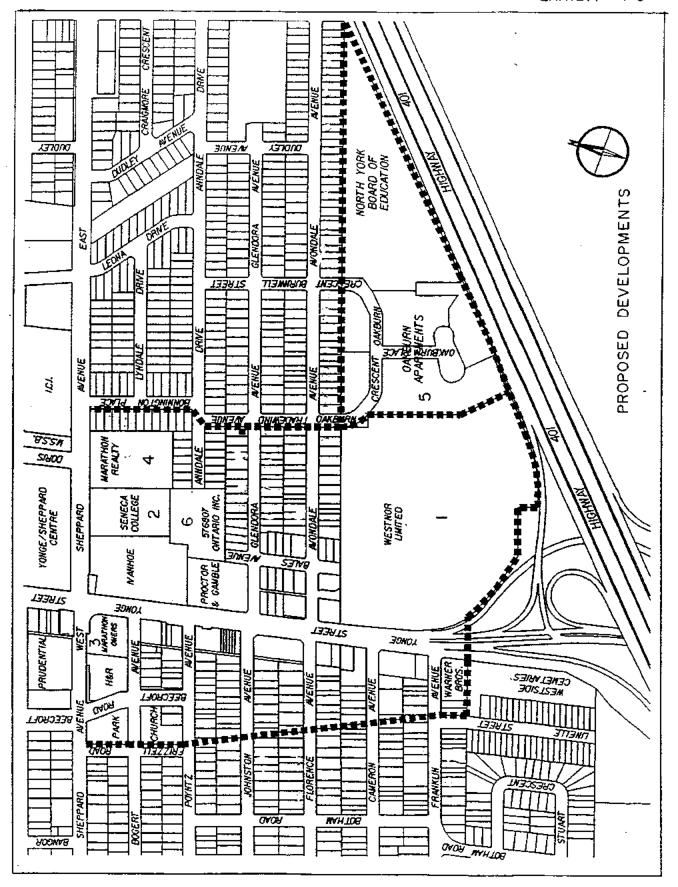
The are a number of development applications either pending or under construction in the South Downtown area that warrant discussion here (see Exhibit 4.6).

1) Westnor Limited owns a significant property assembly in the north east quadrant of Yonge Street and Highway 401 which consists of approximately 9.47 hectares (23.4 acres) of gross site area. An application was made by the owners on June 10, 1994 and has since been revised to account for public input. Circulation of the application commenced in December of 1994 and is yet to be completed. Westnor has referred its application to the Ontario Municipal Board for consideration. It is the Westnor site that provided the momentum for the South Downtown Secondary Plan Review. In order to accommodate the proposed density of use proposed for this site, certain infrastructure improvements are required.

The applicant is proposing to develop the site for a large, high quality, mixed use project that will function as the "gateway" to the City of North York. Uses are to include office and residential, retail and hotel to a total of 5.5 million square feet and a maximum density of approximately 5.0 times the area of the site. In order to construct this project, both Official Plan and By-law amendments are required.

Seneca College owns land located on the south side of Sheppard Avenue immediately east of Yonge Street comprised of 0.98 hectares (2.47 acres). An application for rezoning has been submitted, however, the applicant continues to search for financial partners prior to proceeding. The proposal consists of two parts; the office portion (43,665 square meters, 470,021 square feet) and the school portion (14,642 square meters, 157,610 square feet). Approval has been granted for the school portion only.

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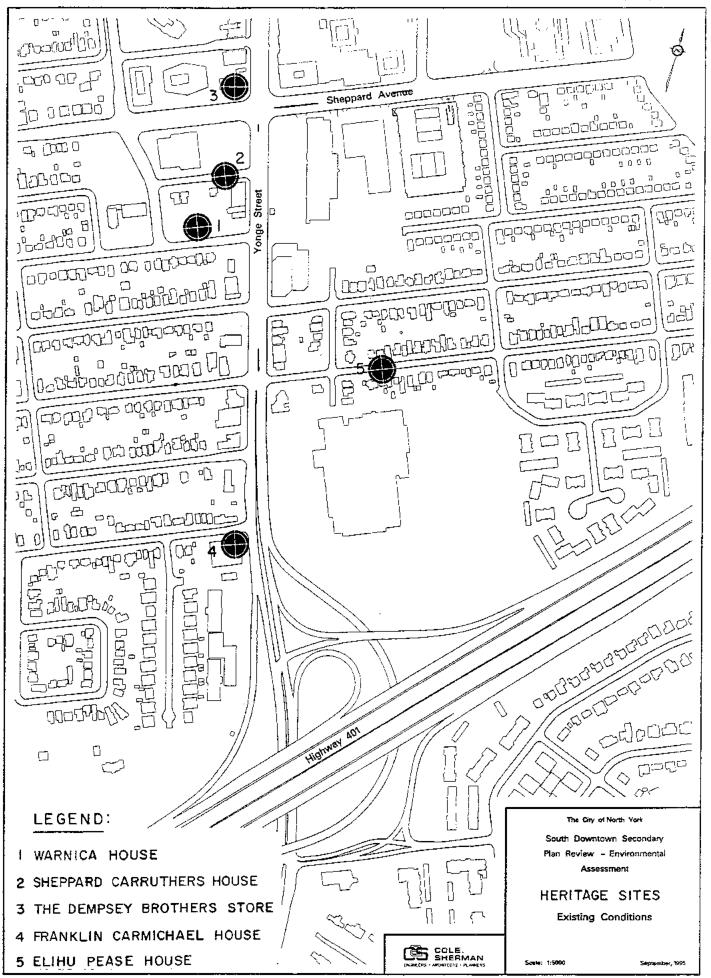
- One application has received approval and is currently under construction on the south west corner of Yonge Street and Sheppard Avenue. Southwest Sheppard Investments Ltd. have commenced construction of a 1,002 sm (10,785 sf.) retail and 33,407 sm (359,601 sf.) office project on a 0.44 hectare (1.08 acre) site adjacent to Yonge Street.
- 4) Marathon Realty has received approval for a 3,937 sm (42,379 sf.) retail and a 34,933 sm (376,028 sf.) office building on 0.40 hectares (0.98 acres) on the south side of Sheppard Avenue immediately west of Yonge Street. Construction has not yet commenced.
- 5) Anndale Investments Limited and Crestview Investment Corporation own the lands bounded by Oakburn Crescent and Highway 401 known at the Oakburn Apartment Site. The site is approximately 3.9 hectares (9.65 acres) in area housing 26 low-rise residential buildings containing 286 rental housing units. A proposal has been developed by the owners for 1,500 residential units both condominium and rental type and a certain amount of open space. The application for Official Plan Amendment is currently being reviewed along with the South Downtown Secondary Plan Review. An application to amend the zoning and an application under the Rental Housing Protection Act is expected by City of North York Staff.
- 6) Finally, discussions have occurred with the owner of a block of land known as the Lansing Court Apartments located at the north end of Bales Avenue and the west end of Anndale Avenue. The proposal would consist of three (3) high-rise apartment buildings and some street townhouses along the service road frontage with a maximum gross floor area of 4.5 time the area of the lot. The site's zoning currently permits only 3.5 GFA. Applications have not yet been submitted for this site.

4.5 THE CULTURAL ENVIRONMENT

The City of North York, in concert with the North York Historical Board have developed an inventory of historically and architecturally significant sites and buildings that contribute to the cultural environment of the South Downtown area, (see Exhibit 4.7). There are five (5) such sites within the study area, two (2) of which have been demolished, two (2) of which exist but are not designated and one (1) of which is fully designated as an historically significant site. To be designated, a site must have undergone a public process which includes public input and the passing of a site specific by-law which ultimately is registered on title. Once designated, the property cannot be demolished without considerable delay, or altered in any way that would jeopardize the heritage values recognized in the underlying reasons for the designation. A designation does not prohibit demolition, however it makes the process extremely cumbersome.

The two demolished properties include the Warnica House (1915) at 40 Poyntz Avenue and the Sheppard-Carruthers House (1865) at 25 Sheppard Avenue West. The two properties that are of some importance however, have never been designated include The Dempsey Brothers Store (1860) at 4804 Yonge Street and the Franklin Carmichael House (1920) at 21 Cameron Avenue. The Franklin Carmichael House is so named for its early owner, Franklin Carmichael of the Group of Seven. He lived in the house until his death, along with his wife. His daughter is the current owner of the home. A Heritage Structure Report was presented to the Historical Board in 1991 for consideration.

Finally, the one designated property is the Elihu Pease House (1834) at 34 Avondale Avenue (designation by-law #31251). The Pease House is a rare survivor of the rural Village of Lansing and has connections with important early North York settlers, the Pease and Cummer families. It preserves the scale and ambiance of an Upper Canada home and a vanished way of life. The house has been moved from its original location, however remains on the original farm lot. The Pease family built the tannery business at Yonge Street and Sheppard Avenue in 1834.



4.6 TRANSPORTATION

The existing transportation infrastructure consists of a combination of roadway, highway, subway, bus and pedestrian facilities.

The arterial roads within the study area include Yonge Street (six lanes) and Sheppard Avenue (four basic lanes being widened to six). Bayview Avenue and Avenue Road are at the limits of the study area and as such are unaffected by this project. To the east and west of Yonge Street there exists minor arterial, collectors, and local roads that serve stable residential neighbourhoods.

Highway 401, a major core/collector freeway, runs east-west at the south end of the study area. Yonge Street and Highway 401 meet at a full interchange configured in a modified partial cloverleaf design.

The Yonge Street TTC subway line runs under the Yonge right-of-way and serves the area through the Sheppard Subway Station. The Sheppard Subway line is currently under construction and is assumed to be in operation for the future conditions. It will also serve the area through the Sheppard Subway Station.

There is skeleton bus service on Yonge Street, including all-night service from downtown Toronto. On Sheppard Avenue, there is very high frequency all-day bus service, that will be replaced, at least in part, by the Sheppard Avenue subway line.

Due to the existing transit modal split and the high density in this area, pedestrian activity is relatively significant and is assumed to increase in the future. All arterial and collector roads in the area have concrete sidewalks on both sides of the street. Pedestrian access is maintained through the east portion of the Yonge Street and Highway 401 interchange by use of the tunnel for the ramp W-N.

5.0 ALTERNATIVE SOLUTIONS TO THE UNDERTAKING

5.1 INTRODUCTION

The need for the South Downtown Secondary Plan was created through the joint commitment by the City of North York and Metro Toronto to create an urban centre along Yonge Street. In preparing the policies for the South Downtown Secondary Plan, North York has prescribed a level of development that will create a significant influx of traffic congestion. This traffic generation will ultimately exceed the capacity offered by the existing transportation network. This results in the problem statement as set out in Chapter 3.

In order to generate alternative solutions to this problem, this report has assessed the following options:

- Do Nothing (i.e., assumes future development will be accommodated by the existing road network and provides a benchmark against which all other alternatives are assessed);
- Transit Improvements (i.e., increase Subway, Municipal Bus and/or Provincial Bus Service beyond a 60% modal split); and
- Roadway Improvements (i.e., construct new and/or widen Local, Collector, Arterial and Provincial Roads).

5.2 DO NOTHING

The 'do nothing' alternative represents what is expected to happen if none of the alternatives being considered are carried out. Normal ongoing roadway maintenance or improvements (including the Sheppard Avenue widening) and a 60% transit modal split, are included as part of the 'do nothing' alternative.

Impacts on South Downtown vehicle access and circulation caused by the 'do nothing' alternative would be unacceptable to the public and transportation authorities involved in this study because of severe traffic congestion and higher safety risks (i.e., North York, Metropolitan Toronto and the Ministry of Transportation).

As indicated in Chapter 3, Section 3.1-Planning Rationale, the Uptown, Downtown, and South Downtown planning areas together form the North York Centre. A transportation analysis conducted by Metropolitan Toronto in

1985 for the North York Centre concluded that a "ring" road system would be needed to facilitate circulation of traffic, particularly shorter distance trips destined for the Centre from Yonge Street. If the ring road was not implemented, severe congestion on Yonge Street and the connecting arterial roads could promote inappropriate and extensive infiltration of traffic into the adjacent residential neighbourhoods. Therefore, the evaluation of alternatives must take into consideration transportation requirements of both the South Downtown area and North York Centre as a whole.

5.3 TRANSIT IMPROVEMENTS

As previously noted, the City of North York and the Toronto Transit Commission (TTC) have analyzed the potential improvements of the transit system in the South Downtown area. Aside from the Sheppard Subway (which is already scheduled for construction) the most significant improvement to transit could be the addition of a subway station south of Sheppard Avenue at Avondale. Since the entrances to the Sheppard station on the Yonge line are at Poyntz Avenue, it is unlikely that a new subway station would improve the transit modal split beyond the assumed 60%. Furthermore a review of transit modal split information (1986-91 Transportation Tomorrow Survey) for areas with development and transportation characteristics similar to those proposed for the South Downtown (e.g., Bloor/Yonge, St. Clair/Yonge, Eglinton/Yonge), has indicated that the assumed 60% modal is an acceptable target but is unlikely to be exceeded. Consequently, the ideal of improved transit to solve the future traffic congestion was eliminated as an alternative to the to the problem identified in Chapter 3.

5.4 ROADWAY IMPROVEMENTS

After screening each alternative, it has been concluded that roadway improvements are needed to address the peak period capacity deficiency problem previously identified. Improving the road network will allow auto traffic to move through intersections and along roadways efficiently. In keeping with the previous studies and the analysis of future baseline traffic conditions the study team concluded that the improved road network would have to incorporate the following characteristics to provide sufficient traffic capacity:

- extensions of the east and west service roads
- grade separated connection of the service roads across Yonge Street.
- new and/or improved ramp access to and from Highway 401.

5.5 CONCLUSION

In summary, throughout the Secondary Plan review and identification of the problem statement for this undertaking, it has been demonstrated that the alternative of improving the road network is the one that best satisfies the goals of the Plan and the municipality. Chapter 6 will outline the generation of alternative road network improvements to be used in the evaluation process.

6.0 ALTERNATIVE DESIGNS

6.1 INTRODUCTION

As concluded in the previous section, roadway infrastructure improvements are required to solve the problem. These will include reconfiguration of the Yonge Street and Highway 401 interchange as well as additional service road links and improvements to Yonge Street. This chapter of the report will describe the criteria used to generate the alternatives, describe the alternatives which were generated and analyze/evaluate the alternate roadway networks developed.

6.2 ROAD NETWORK DESIGN OBJECTIVES

Roadway networks were developed to meet the future development objectives of the North York South Downtown Area. This process was divided into five sections: i) East Service Road, ii) West Service Road, iii) East-West Link (Lower Service Road) iv) Yonge and 401 Interchange and v) Hogg's Hollow Bridge Widening/Highway 401 capacity.

Alternatives were developed for these portions of the total network following the "Rationale Used to Select Alternatives Studied" as shown below.

East Service Road (North-south continuation of the existing Service Road in the Downtown, east of Yonge Street)

- · Must connect to Doris Avenue at the north end
- Must connect to east-west link and Highway 401 ramps at the south end
- Alignment far enough east of Yonge Street to allow a signal at Avondale Avenue
- Capacity sufficient to service the proposed development in the South Downtown, the Downtown and the Uptown Official Plans

West Service Road (North-south continuation of the existing Service Road in the Downtown, west of Yonge Street)

- Must connect to Beecroft Road at the north end
- Must connect to east-west link and Highway 401 ramps at the south end
- Alignment far enough west of Yonge Street to allow a signal at Florence Avenue
- Capacity sufficient to service the proposed development in the South Downtown, the Downtown and the Uptown Official Plans

East-West Link (Lower Service Road) (East-west link between the West Service Road and the East Service Road)

- Alignment far enough north of Highway 401 to allow the ramps to terminate at signals
- Capacity sufficient to service the proposed development in the South Downtown, the Downtown and the Uptown Official Plans
- · Grade separated at Yonge Street
- · Acceptable traffic delays during construction

Interchange

- · Provide additional E-N ramp into the Westnor site
- · Provide additional N-W ramp out of the Westnor site
- · Provide access to East-West link from the west
- · Provide new free-flow N-E ramp off of Yonge Street
- · Provide access to 401 east and west from the West Service Road
- Ramp capacity sufficient to service the proposed development in the South Downtown, the Downtown and the Uptown Official Plans
- Acceptable traffic delays during construction

Hogg's Hollow Bridge Widening - Highway Capacity

- Must provide an extra westbound-collector lane over the valley to allow proper lane continuity and balancing
- · Acceptable traffic delays during construction

6.3 GENERATION OF ALTERNATIVE ROAD NETWORK DESIGNS

Using the rationale discussed above, alternative designs were generated to solve the problem.

There were many alternatives considered for the interchange including i) N-E ramp tunnel, ii) N-E ramp inner loop (south-west quadrant) iii) N-E ramp from the East Service Road and iv) N-E ramp under the Hogg's Hollow Bridge. All of the above were considered at a draft level of detail and screened due to geometric constraints (e.g. not buildable to acceptable standards). The remaining interchange alternative as seen in Exhibits 6.1, 6.2 and 6.3 was developed to a higher level of detail and matches into any of the service road scenarios considered.

Only one east-west link design was considered, for the following reasons. To service future development, it was determined that the link should be between Avondale Avenue and the terminus of the additional Highway 401 ramps. As well, it was necessary to grade separate the link with Yonge Street, while avoiding the existing Yonge subway tunnels. These criteria placed the east-west link in its position as shown in Exhibits 6.1, 6.2 and 6.3.

Analysis of the lane balancing, continuity, weaving and operations of Highway 401 show that an additional westbound collector lane is required over the Hogg's Hollow Bridge (Appendix A). Various lane realignment and structural alternatives were considered including substandard shoulders widths and a cantilever off of the existing structure. The only acceptable widening technique was determined to be structural widening utilizing additional piers to the valley floor.

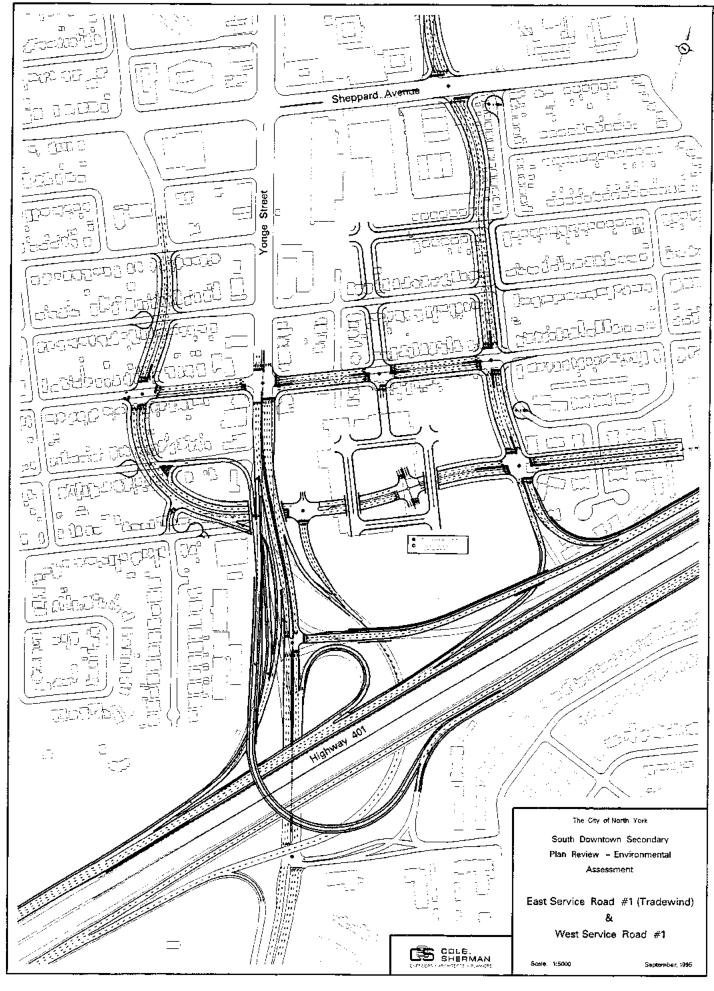
All of the service road alternatives carried forward to the evaluation stage can be seen in **Exhibits 6.1**, **6.2** and **6.3**. For the East Service Road these include 3 alternatives namely, Tradewind, the Combination and the Midblock. For the West Service Road Alternatives #1 and #2 were carried forward.

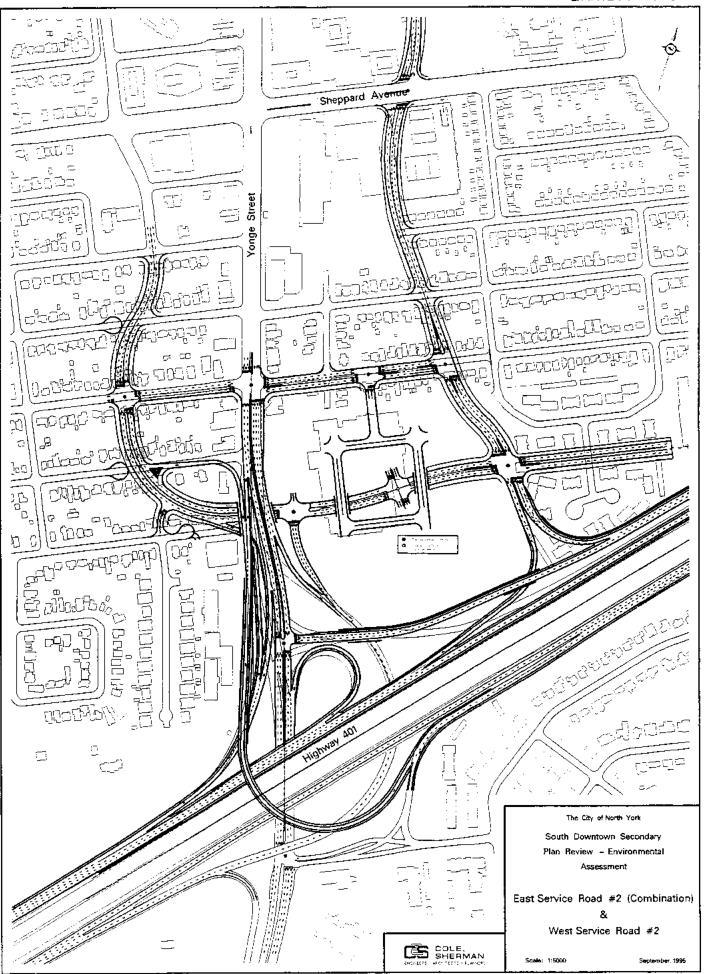
6.4 EVALUATION CRITERIA

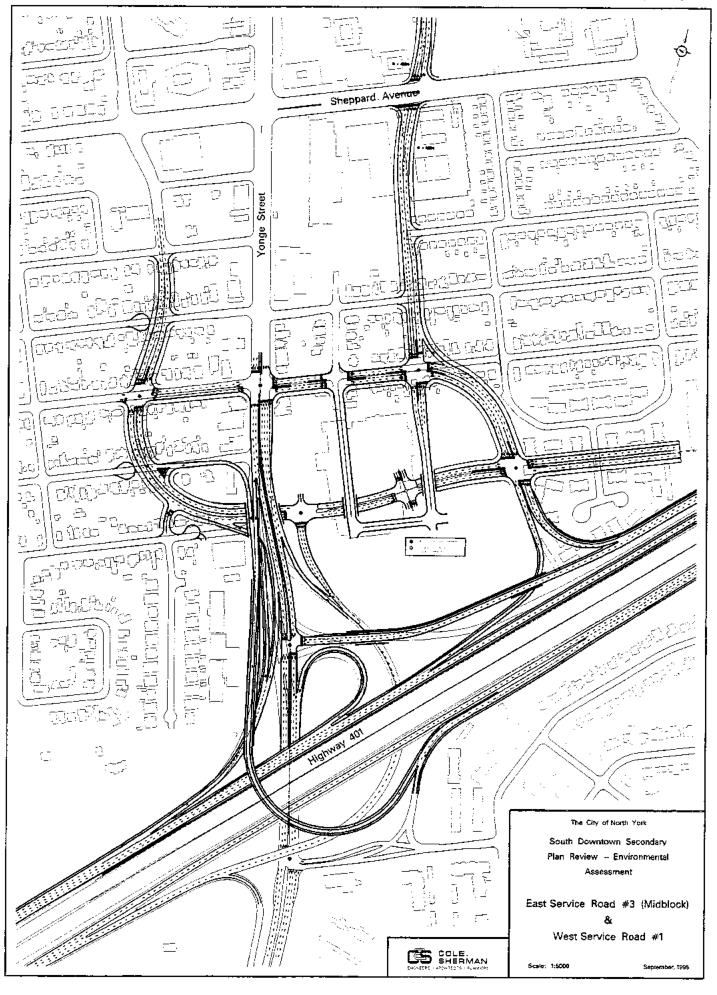
The criteria used to evaluate the alternatives were developed by the study team utilizing evaluation factors from "South Downtown Secondary Plan Review Report 1 to 7", the comments received from stakeholders (stemming from initial stakeholder meetings) and other relevant Environmental Assessment factors. This criteria considers the traffic operations, natural environment, socio-economic environment, cultural environment and the cost of each alternative. The criteria used in the evaluation can be seen in Exhibits 6.4, 6.5, 6.6 (The evaluation matrices)

6.5 EVALUATION OF ALTERNATIVES

Only the East Service Road and the West Service Road were taken to the evaluation process. Therefore as discussed above, alternatives for the east-west link and the interchange were screened during the alternative generation process.







The City of North York SOUTH DOWNTOWN SECONDARY PLAN REVIEW Environmental Assessment Study Service Road Analysis/Evaluation

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	a Control Aire	1	1 Service Rulau Alternatu	Ш	West pervice Road Alternatives	au Alternatives	
EVALUATION FACTOR	INDICATOR	Alternative #1 Tradewind Alignment	Alternative #2 Combination Alignment	Alternalive #3 Midblock Alignment	Alternative #1	Afternative #2	KATIUNALE
Transportation a. Local Traffic Operations	subsuper of movements with insufficient queue lengths	Esst Service Rd/Avondale E AM ttaffic moving south / bound through right	East Service Rd/Avondale RAM traffic moving south bound through right	East Service Rd./Avondate AM traffic moving south bound through right and left	None	Моне	Usuffician length can result in blockage of adjacent intersections
	 number of problem, movements at intersections during the AM and PM peak hour 	Yonge/Avandale AM north 19 bound Inft and through 16 moving traffic, and PM 17 rough bound right and east 18 bound right moving traffic 16	Yonge/Avendale AM north bound left and through involving traffic, and PM round right and east is bound right moving traffic	Yongo/Avendale AM north Poound left and through moving traffic, and PM south bound right and east bound right moving traffic	No movement problems	No movement problems	Problem movements at intresections will result in traffic congestion and delays
b. Roadway Design	 qualitative assessment of a driver's roadway design expectations 	The straight INS roadway alignment allows the East Service Road/Avondale intersection to cross in a perpendicular manner	The slightly skewed N/S condows alignment forces the East Service Road-Avondale intersection to cross at a 70 degree angle	The curvature of the NVS continue alignment creates a East Service Road/Avondate intersection design that is not typical of the area	The West Service Road Florence intersection is skewed at 70 degrees.	The West Service Road Florence intersection is perpendicules. However, the section further north contains a right reverse curve.	Access to and from the residential community may have to be re-routed to Yongo or Sheppard
Natural Environment a Vegetation	• number, type and condition of irees removed	hpprox 101, predominately silver maple trees showing signs of stress and strain.	approx. 57, predominasely silver maple trees showing signs of stress and strain.	approx. 57, predominately silver maple trees showing signs of stress and strain	approx. 41, predominately silver maple trees showing signs of strees and strain.	approx 41, pradominately silver maple trees showing signs of stress and strain.	Roadway construction may result in the removal of frees from existing urban landscapes
Socio-Economic Environment n Noise Impact	 number of sensitive land uses with a significant change in noise 	Noticeable change in ambient noise between Sheppard and Ayondale.	Noticeable change in ambient noise between Shegpard and Avondale.	Noticeable change in ambient noise between Sheppard and Avondale.	Noticeable change in ambient noise between Sheppard and Franklin,	Noticeable change in ambient noise between Sheppard and Franklin.	More traffic in combination with new or widend roads will move the noise source (auto traffic) closer to the sensitive receivers (i.e. houses)
b. Air Quality Impact Desidential Declaration	qualitative assessment of air quality impact to sensitive receivers runmber and two of residential premetrize recurring total acquisition	Does not exceed MOEE air quality standards.	Does not exceed MOEB air quality standards. 25. single family	Does not exceed MOEE air quality standards. 26. single family	<u> </u>	Does not exceed MOEE air quality standards. 46. sinele family	More traffic in combination with new or widened roads may lower local air quality below provincial standards. Will require anniestion of recidental property.
	- number, type and area of residential properties partially impacted	200 sm	gie family, 100 sm, and floor, apartment ing, 20 sm	gle family, 50 sm floor, apartment ing, 20 sm	1, single family, 20 sm	2, single family, 80 sm	Will require sequisition of sesidential property
e Separation Distance	 distance of the stable residential development from the service road curb at the closest point 	21m	64m	67m	20m	20ш	Need to establish buffer area that will minimize impacts to stable residential area
E. Consistency of Blocks	 qualitative assessment of consistency of street and block pattern to urban design principles contained in the South Downtown Secondary Plan. 	Limited possibilities to accommodate extension of street and flock pattern south of Avondate Avenue. Rating Moderate	Creates some smaller and conceites some inegular remaint particle that are not consistent with the street and block pattern. Limited possibilities to accommodate extension of second block pattern south of Avvandale Avenue Rating: Low	Accommodates extension of sneet and block pattern south of Avondale Avenue. Rating: Good	Road alignment swings easterly to meet Beecroft Road earter creating more regular staped blocks. Rating: Good	Road alignment swings further west before meeting state of the desirating smaller, more irregular shaped blocks. Rating: Moderate to Good	Proposed roadway should create blocks that are consistent with the surrounding area

IMPACTS ARE THE SAME THEREFORE THE EVALUATION FACTOR IS NOT DECISION RELEVANT

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L			Eas	East Service Road Alternatives	ives	West Service Ruad Alternatives	ad Alternatives	
Š	EVALUATION FACTOR	INDICATOR	Alternative #1	Alternative #3	Alternative #3	Alternative #1	Allemative #2	RATIONALE
			Tradewind Alignment	Combination Alignment	Midblock Abgament			
DQ	Pedestrim and Vehicular Connections	 qualitative assessment of connections to North York City Centre and surrounding stable residential areas. 	Toes not alfoid connection of Bales Avenue into huge development parcel south of Avondale Avenue (Westnor). Rating: Moderate	Does not afford connection (S Bales Avenue into Jago development aparel south of Avondate Avenue. (Westnot). Rating: Moderate	Afforts connection of Bales Avenue into large development parcel south Avondale Avenue. Affords major predestriantvehicular intege via the East Service Rowei into Westnor. Rahmg. Good	Affords pedestrian and vehicular connections vehicular connections vehing: Good	Affords pedestnan and vehicular connections Rating: Good	Sufficient space must be available to establish public open spaces that form continuous system throughout the South Downtown
<u> </u>	Open Space Provision	 qualitative assessment of size, configuration, location, access and linkage potential for open space in the axea. 	Foor allothent of open spac due to small parcel size and access constraints	Poor allotment of open space Good allotment of open space due to small parcel size and given the relatively large access constraints parcel size, afficient shape and easy access potential	Good allotment of open space given the telahvely lurge parcel size, efficient shape and easy access potential	Good allotment of open space because it provides convenient pedestrian linkage through south downlown	Good allotment of open space because it provides convenient pedestrian linkage drough south downtown	
	Busingses Displaced	number and type of business property requising total acquisition		0	0	Three including: Petro Canada, Naulits and Video Oralet	Three including: Petro Carada, Naudis and Video Outlet	Construction of a new or widened toadway will require acquisition of commercial or institutonal property
	•	· number of employees affected			0		7.0	
	Businesses Disrupted	. number, type and size of business property impacted	1 (Marathon), 7 and 9 floor office buildings, 1850 sm (impact on the east side displaces access and parking spaces)	1 (Marathon), 7 and 9 floor office buildings, 3000 sm (impact on the west side displaces parking spaces and landscaped open space)	i (Marathon), 7 sud 9 floor office buildings, 2300 sm (impact on the west side displaces parking spaces and landscaped open space)			Construction of a new or widened madway will require acquisition of commercial or institutional property
		• disruption during construction	relocation ing	Marathon access relocation will disrupt parking activity		Highway 401's lengthy (amp construction period will eliminate Yonge St. pedestrian access to Warrer I B.roy.	Lighway 401's lengthy iranp construction period will eliminate Youge St pedestrian access to Warner Bros.	Discuption during construction including noise, dust, vibration and goldution may impact existing businesses
ند	Institutions Displaced	 number and type of institutional property requiring total acquisition number of employees affected 	0.0	0	۵ ئ	0 0	0	Construction of a new or widened roadway will require acquisition of institutional property
-	Institutions Disrupted	number, type and size of institutional property impacted disruption during construction	Catholic School 100 sm	1 (Seneca College), 1410 sm Minimal	1 (Seneca College), 1200 sm Minimal	0	0	Construction of new or widened road may impact existing institutional uses
É	Future Development	length of development block exposure to service road number of unreasonably constrained development blocks	1070 m I (area between the alignment and Bonnington)	.1220m o	1270m 0	720m 1 (area bounded by the abignment, Yonge St. and Chrneron Ave.)	790m. I (area bounded by the alignment, Yonge St. and Cameton Ave.)	Development of sites should not be unreasonably constrained by coadway location
ď	Traffic Infiltration	 qualitative assessment of infiltration of outside traffic into stable residential areas 	Запс	Same	Same	Same	Same	Fiallic that will accompany this fevel of development may infiltrate the stable residential areas that abut the

The City of North York SOUTH DOWNTOWN SECONDARY PLAN REVIEW Environmental Assessment Study Service Road Analysis/Evaluation

		East	East Service Road Alternatives	ves	West Service Ro	West Service Road Alternatives	
EVALUATION FACTOR	INDICATOR	Alternative #1 Tradewind Alignment	Atteniative #2 Combination Alignment	Alternative #3 Midbloch Alignment	Allemative#L	Alternative #2	RATIONALE
Cultural Environment a. Heritage Features Displaced	number and type of heriage feature requiring total acquisition	l (Elhu Pesse House), 0 designated undet by-law 31251			(F. Camichael Houri) not designated	1 (E. Carmichael Houer, librarical description)	(fo Carnickasi House); 14.(E. Carnickasi House). Heninge features are an important part of any community obligacions.
b. Hettinge Features Disrupted	Heringe Features Disrupted • number, type and size of heritage feature partially impacted	9		0	0		Heritage features are an important part of any community
Cost a Total Cost	 present day cost to acquire necessary property, construct roadway and provide mingation 	\$18,500,000 (\$14,6M + \$2.8M + \$1.1M)	\$16,500,000 \$16,000,000 \$14,6M + \$2,8M + \$1,1M) (\$11,6M + \$2,3M + \$2,2M) (\$11.9M + \$1.9M + \$2,2M)	(\$11.9M + \$1.9M + \$2.2M)	524 3.00 bed (3.2 764 * \$1.15.ft)	\$\$4.200,600 (\$\$2.700 + \$4 15);	Roadway construction will require acqueition of property Cost of construction of infrastructure works

During the evaluation process, each of the service road alternatives are considered against the various evaluation criteria. The decision irrelevant criteria are highlighted as these are factors that are common to each alternative and therefore do not aid in the decision making process. The next step would be to create a concise table showing only those decision relevant factors that will aid in the decision making process. The results of this evaluation process can be seen in Exhibits 6.4, 6.5 and 6.6. Relevant background data used to complete these evaluation matrices are held on file.

6.6 DECISION MAKING PROCESS

The next step in the evaluation process would be to assess the final table, make tradeoffs and recommend a preferred alternative. This step was not completed at the time of writing. The alternatives developed and the evaluation method to be used was presented to the Steering Committee, however no formal recommendation has been carried forward to Council or the public.

7.0 PROPOSED PROJECT DESIGN

At the time of the preparing this report, no decision was made on the selection of the preferred service road alignments. This section of the report will serve as a forum for discussing and displaying engineering work that is complete to date.

MTO has given approval in principle to the engineering and construction staging and will require specific endorsement of the appropriate ESR as well as at construction design and implementation stage.

7.1 ROADWAY

7.1.1 Cross-Section

Typical cross-sections were developed for most of the major components of the roadway network. The proposed cross-section for the east and west service road is typical through-out the project with the exception of taper and turning lane widenings. This can be seen in Exhibit 7.1

Exhibit 7.2 displays the existing and future typical cross-sections for Yonge Street between Highway 401 and Avondale Avenue. The details of the construction staging required on Yonge Street can be seen in Section 7.2 of this report.

Typical ramp sections were developed for all of the proposed ramps based on OPSD standards and MTO Geometric Design standards. These can be seen in Exhibits 7.3, 7.4 and 7.5, referring to one lane, two lane and three lane ramps respectively.

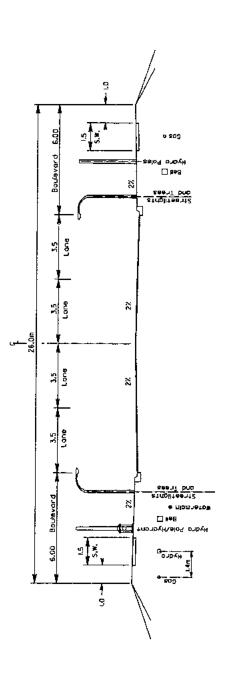
Structural sections for the N-E flyover ramp and the Hogg's Hollow Bridge are referred to in Section 7.3.

7.1.2 Horizontal Alignment

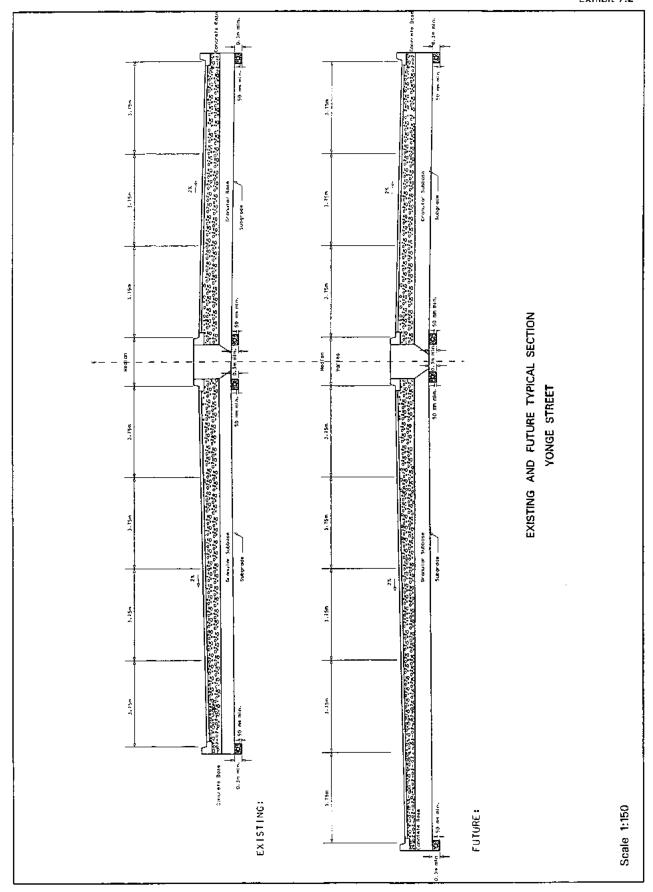
The details of the horizontal alignment, including all ramp and roadway geometrics at 1:1000 scale have been prepared. Final Exhibits of the project have not been prepared at this time.

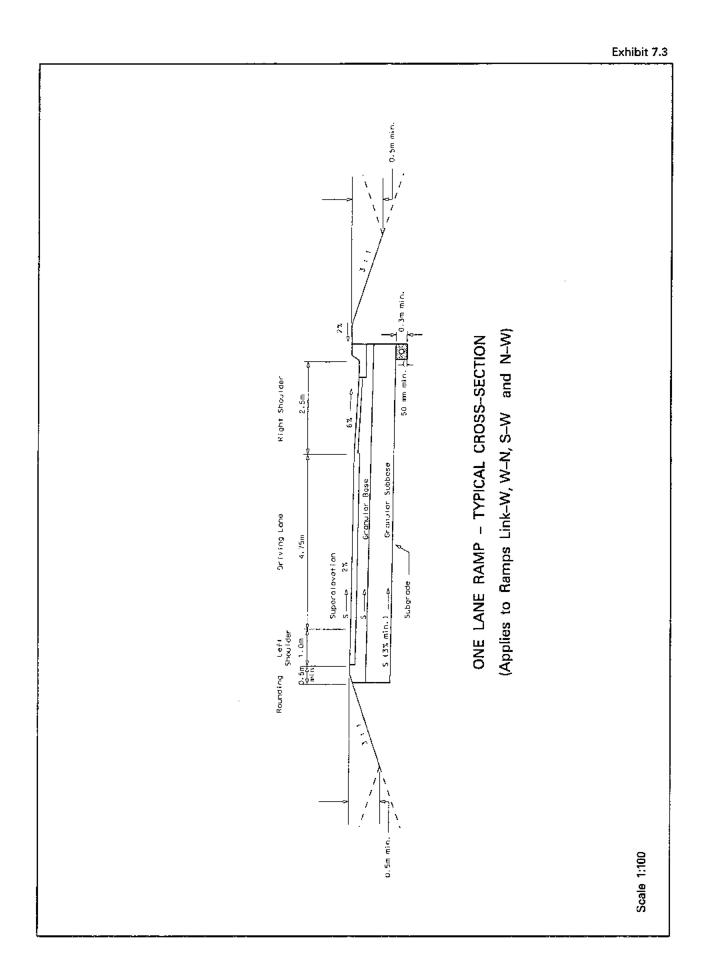
7.1.3 Vertical Alignment

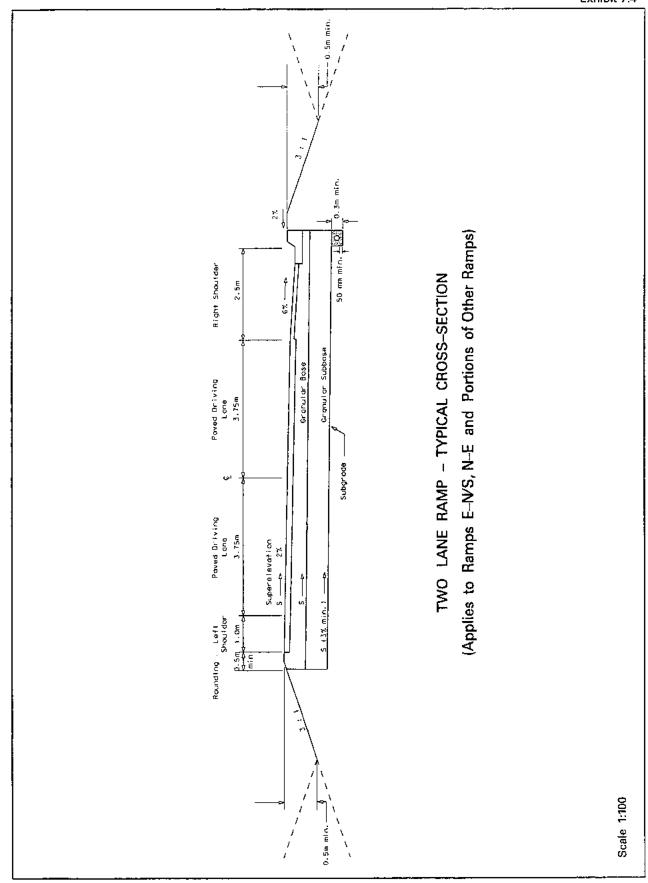
Profiles of all ramps and roads within the proposed network have been prepared on roll section paper. Formal Exhibits of the vertical alignment have not been prepared at this time.

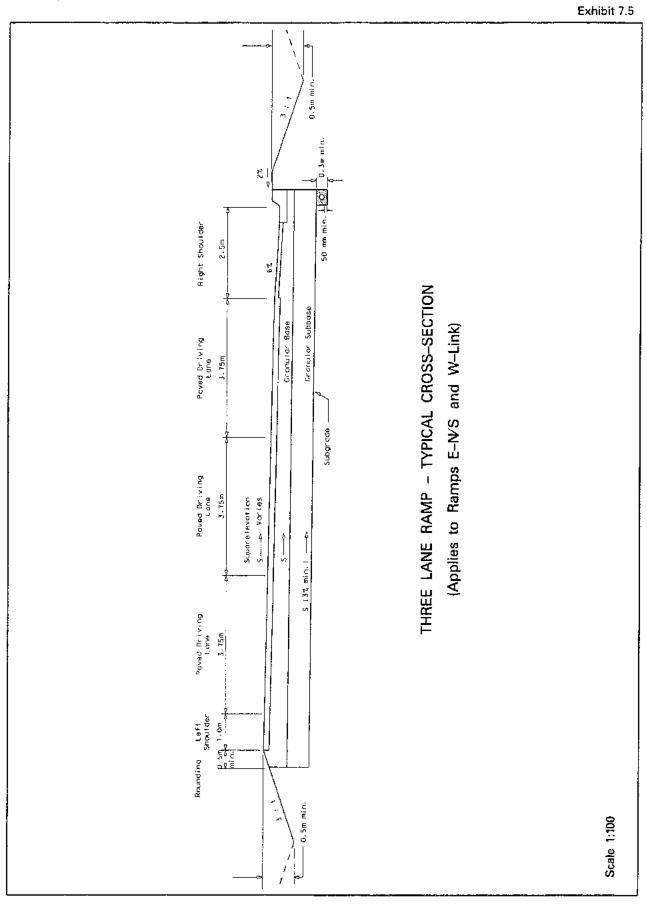


SERVICE ROAD TYPICAL SECTION (26.0m RIGHT-0F-WAY)









7.2 STAGING AND DETOURS

Construction staging has been considered on two major levels. The first is the overall long term staging for the entire roadway network and the second is the details of the staging and detours necessary to construct various portions of the network while maintaining safe and efficient traffic flow.

The former of the above two levels is shown on Exhibit 7.6 and explained in detail below:

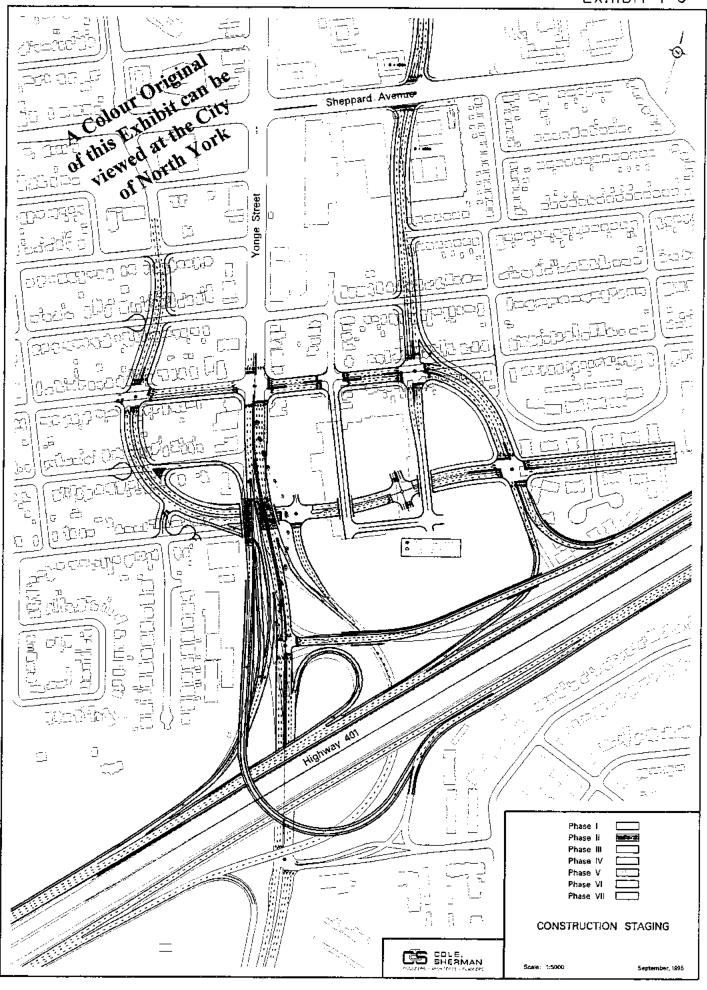
Phase I

- Construct ramp 401 east to Yonge Street, ramp 401 east to Service Road and entire East Service Road (and Avondale Avenue), including a new structure over future ramp Service Road to 401 west and widening of existing structure over ramp 401 west to Yonge Street north
- Existing traffic on existing roads and ramps, stage construct the widening of the existing structure over ramp 401 west to Yonge Street north with a temporary connection to the existing Yonge Street for the south movement
- At completion of construction, traffic from 401 east going to areas north of the 401 forced to use ramp 401 east to Service Road and Service Road system to Yonge Street and Sheppard Avenue. Traffic going to areas south of the 401 would use new ramp 401 east to Yonge Street south
- This would relieve some of the traffic at the intersection of Yonge Street and Franklin Avenue

Phase II

- Detour Yonge Street or stage construct Structures at Yonge Street and Franklin Avenue
- Traffic the same as Phase I except complete temporary connection to ramp Yonge Street north to 401 west
- Stage construction of theses structures is possible while keeping all existing lanes open. A detour would quicken construction of the structures, allow Yonge Street traffic to flow smoothly and clear existing Yonge Street through this area for the Yonge Street re-alignment

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Phase III

- Construct flyover ramp Yonge Street north to 401 east complete with tie to existing ramp Yonge Street north/south to 401 east
- Traffic using Phase I infrastructure (ramps/East Service Road), detoured Yonge Street and existing ramps
- Open new flyover ramp to traffic, the section of Yonge Street between Florence Avenue and the 401 has been relieved of most of the traffic flow to or from Highway 401
- Short time closure at ramp connection Yonge Street south to 401 west would likely be required

Phase IV

- Stage construct the re-alignment of Yonge Street including the widening of the existing Highway 401 westbound collector structures over Yonge Street and ramp 401 west to Yonge Street north and connection to ramp 401 west to Yonge Street north
- Traffic on newly constructed ramps and stage constructed Yonge Street remaining open at peak traffic periods
- Temporary connections to existing ramps Yonge Street south to 401 west and Yonge Street north to 401 west
- Some work may be required on ramp 401 west to Yonge Street north for structure clearances

Phase V

- Construct the widening of the Hogg's Hollow structure (401 westbound collector)
 and ramp Yonge Street north to 401 west
- · Ramp to remain open at all times

Phase VI

- Construct ramps Service Road to 401 west and Yonge Street south to 401 west
- Short time closure likely required for ramp Yonge Street south to 401 west construction

Phase VII

- Complete construction of West Service Road, east-west link (Lower Service Road)
 and ramp connections 401 west to Service Road and Service Road to 401 west
- Service Roads and connection from ramp 401 west to Yonge Street north could be constructed after Phase IV with the connection to ramp Yonge Street north to 401 west being constructed after Phase V

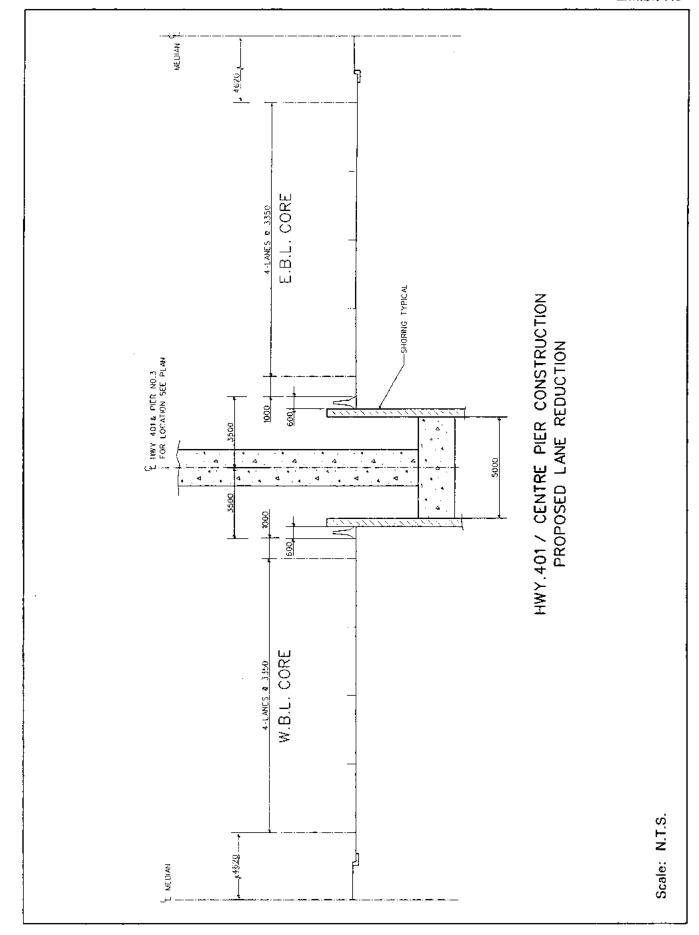
There were four major areas of concern regarding the staging and constructability of the proposed works: i) Yonge Street overpass at Franklin, ii) Yonge Street south of Franklin, iii) N-E flyover (impact to Highway 401 operations) and iv) N-E flyover (impact to Yonge Street at pier). Each one of these concerns was addressed in detail as can be seen in the recommended staging sections, Exhibits 7.7 to 7.10 respectively.

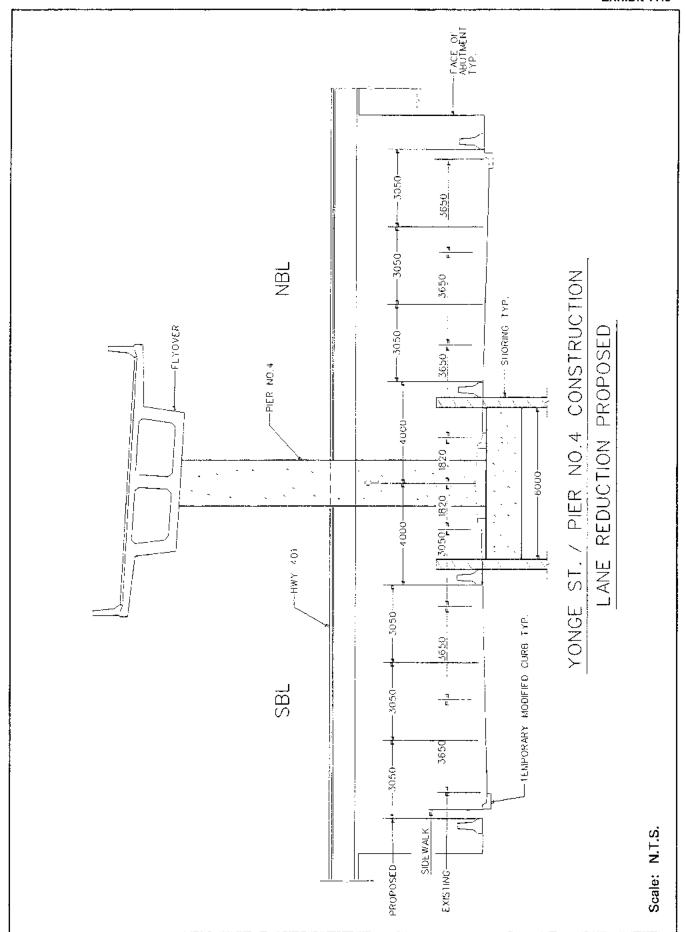
7.3 STRUCTURES

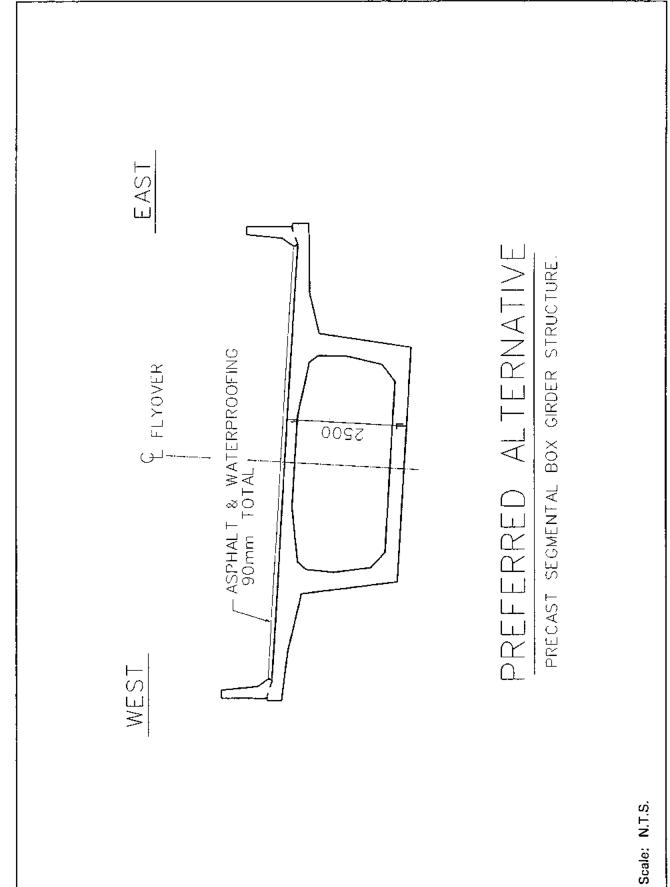
A preliminary assessment was made of all structural issues during course of this study. These included the following; i) Highway 401 bridge widenings, ii) new structure ramp E-N/S, iii) ramp N-E (flyover), iv) Yonge Street structure at Franklin Avenue and v) Hogg's Hollow bridge widening. All of these structural works are considered feasible at this time. Items iii) and v) were considered to be the most critical to the success of the network improvements and therefore received the greatest attention.

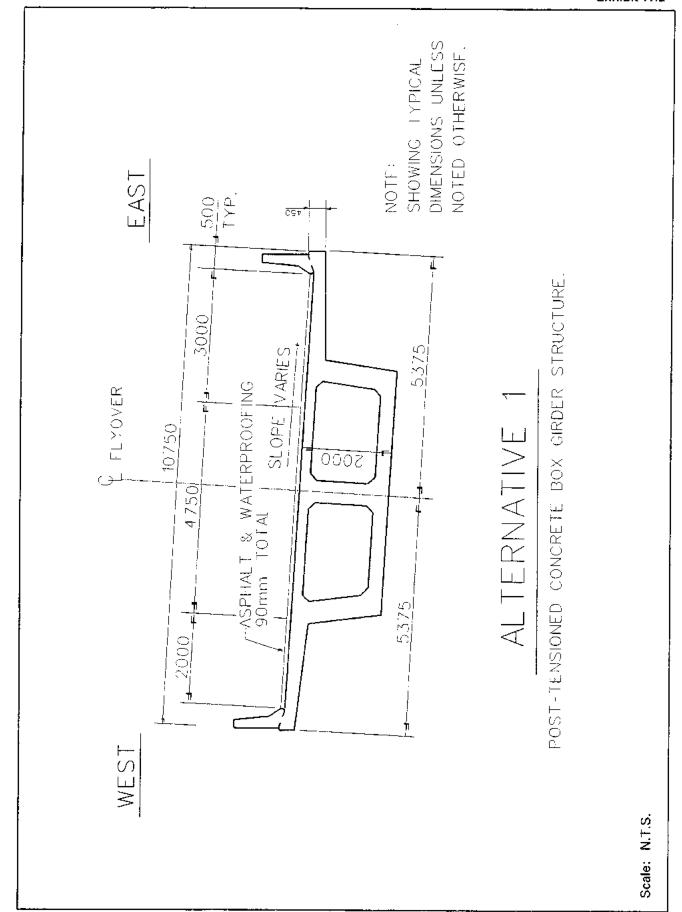
Although many alignments for the N-E flyover were considered, only one met the geometric constraints of the existing conditions. The location of this structure can be seen in Exhibits 6.1, 6.2 and 6.3. Three alternative structure types were considered for the flyover as seen in Exhibits 7.11, 7.12 and 7.13. At the time of writing, the precast segmental box girder (Exhibit 7.11) was favored due to its ease of construction.

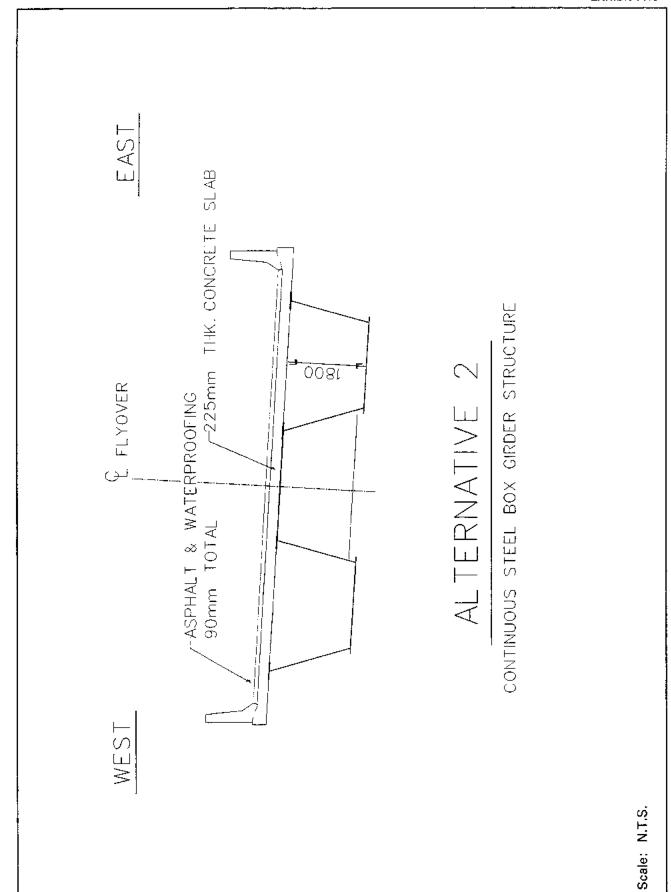
Exhibit 7.14 shows the lane reconfiguration considered for the additional westbound collector lane over the Hogg's Hollow bridge. It was determined that the substandard lane and shoulder widths would not be acceptable and this alternative was dropped. Exhibits 7.15 and 7.16 show the two widening alternatives considered for the widening of the bridge. As can be seen in Exhibit 7.15, the applied moment would be increased by the cantilever and it was determined that the bridge would fail. The only feasible alternative for the widening of the Hogg's Hollow bridge is shown in Exhibit 7.16. This construction would require additional piers down to the valley floor.

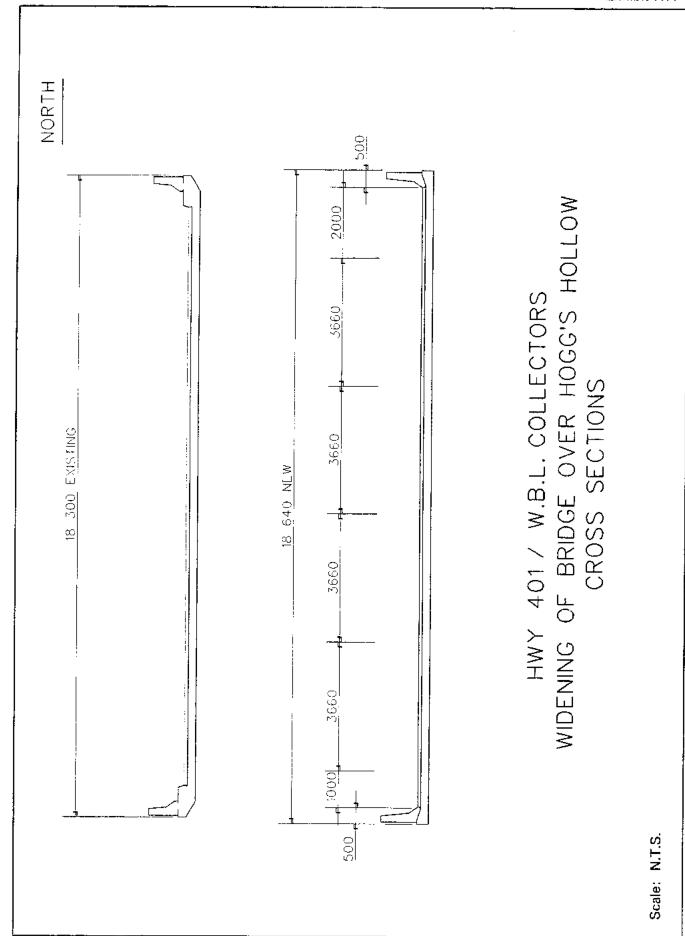


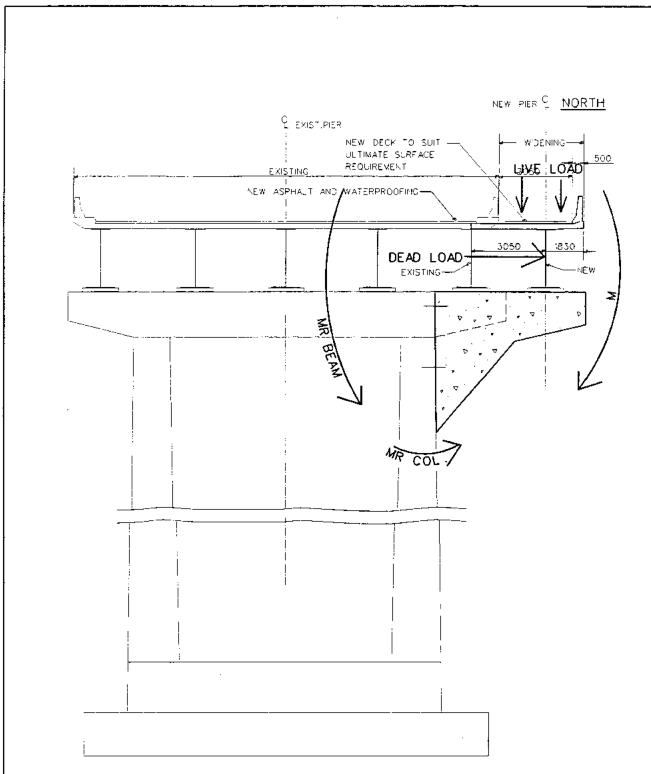






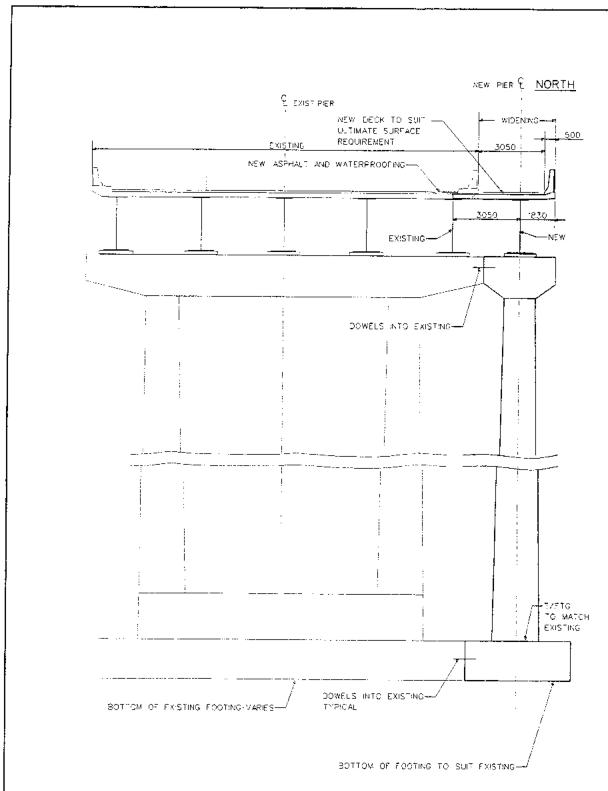






HWY 401 / W.B.L. COLLECTORS
WIDENING OF BRIDGE OVER HOGG'S HOLLOW
PIER CAPPING BEAM EXTENSION

Scale: N.T.S.



HWY 401 / W.B.L. COLLECTORS
WIDENING OF BRIDGE OVER HOGG'S HOLLOW
CROSS SECTION

Scale: N.T.S.

7.4 CONSTRUCTION COST ESTIMATES

Preliminary quantities and construction costs were developed at the alternative evaluation stage of this project. These included costs (in 1995 dollars) for every component of the infrastructure improvements as summarized below:

Eas	st Service Road	
•	Alternative #1 (Tradewind)	\$3,920,000
•	Alternative #2 (Combination)	\$4,514,000
•	Alternative #3 (Midblock)	\$4,121,000
W	est Service Road	
•	Alternative #1	\$1,473,000
•	Alternative #2	\$1,492,000
Eas	st-West Link (Lower Service Road)	
•	Preferred Alignment	\$ 853,000
Yo	nge Street Reconstruction	
•	Preferred Alignment with detour	\$5 <i>,</i> 788,000
Int	terchange	
•	Ramp 401 East to Service Road	\$2,162,000
•	Ramp 401 East to Yonge North & South	\$1,641,000
•	Ramp 401 West to Yonge North & Service Road	\$ 591,000
•	Ramp Service Road to 401 West	\$1,503,000
٠	Ramp Yonge South to 401 West	\$ 691,000
•	Ramp Yonge North to 401 East	\$9,528,000
•	Ramp Yonge North to 401 West	\$10,215,000
To	tal Construction Cost	
•	Based on Average Cost of Alternatives	\$38,640,000
•	10% Contingency	\$ 3,860,000
•	10% Engineering	\$ 3,860,000
	TOTAL COST	\$46,400,000

Details of the quantities, unit costs and totals for each item and each component of the above summary can be seen in Appendix B.

8.0 TASKS TO COMPLETE THE STUDY

8.1 Introduction

As discussed earlier, this is a "Background Report". This chapter will suggest the outstanding work required to complete a Class 'C' "Environmental Assessment for Municipal Roads" for the transportation infrastructure required for development levels associated with "Vision" development. The tasks are broken down into three main sections i) engineering, ii) public consultation and iii) the final report. Section 8.5 of this chapter outlines the additional information available through Cole, Sherman that is not included in this report.

8.2 ENGINEERING

The evaluation of the east and west service road alternatives is now complete. The next step will be to complete the decision making process and identify the preferred alternatives.

When the preferred alternatives are selected, Cole, Sherman will continue with the preliminary design of the recommended infrastructure improvements. This process is partially complete for the interchange portion of the project and will continue as outlined in section "5.0 Preliminary Design" of our original study design. Preliminary design of the service roads has not begun.

It should be noted that the Hogg's Hollow bridge widening will require an additional study. The structural investigation into various widening techniques identified additional piers to the valley floor as the only feasible solution. These piers introduce a new set of environmental and geotechnical concerns that must be identified and engineered. MTRCA is fully responsible for the terrestrial and aquatic impacts caused by the bridge widening and have not yet been contacted. The following is a preliminary list of concerns at the West Don River Tributary:

- Fish Habitat warmwater tributary of Type II significance (i.e., warrants mitigation or compensation if impacted). Pier and footing construction will force the relocation of the West Don River tributary.
- Flood and Fill pier and footing placement will fall within MTRCA's flood and fill regulation lines.
- Vegetation plant life potentially impacted falls within the following categories: manicured, meadow, and successional forest.

- Wetlands/ANSIs/ESAs none.
- Surficial Geology the area immediately below the Hogg's Hollow bridge closest to the river bed consists of sand, silt, clay and muck including Pleistocene Alluvium. Surrounding the flood zone, the earth consists of Undifferentiated Glacial and Interglacial Deposits.
- Recreation the area under Hogg's Hollow bridge links the north and south portions of the Don Valley Golf Course (a public course owned by the municipality).

The final step in the original study design was "6.0 Construction Staging and Scheduling". During the course of this study construction staging sections, detours and schemes have been completed to ensure constructability. The level of detail in these areas is sufficient for a Class EA. It has been determined through the traffic study that the entire infrastructure improvement scheme must be in place to support further development in the North York South Downtown. For this reason, it is not recommended that reduced schemes be considered to support reduced development levels. Therefore, the construction schedule (timing) is a product of development levels and funding and is beyond the scope of this study.

8.3 Public Consultation

The public consultation process for this undertaking has been extensive and open. A second Public Information Centre was scheduled for March of 1995, however, was suspended pending direction from Council. This PIC must be held to present the preferred alternative once it is identified during the above-mentioned decision making process. Public input from this PIC will be gathered, summarized and weighed against the decision that is presented. All of this input will be detailed further in the completed (final) ESR.

8.4 FINAL ENVIRONMENTAL STUDY REPORT (ESR)

Given that this is simply an interim status report, the final ESR will be required to satisfy the Class EA process. The ESR will be in a similar format as this report however, will detail the preferred alternative and complete the public consultation component. Additional background information will be provided along with further exhibits and support material. The ESR document will be placed on public record for examination purposes and will ultimately become the governing work to guide the undertaking.

APPENDIX

A

TRAFFIC STUDY

SECONDARY PLAN REVIEW

ZNVRONMENTAL Assessment Study

> SERVILS REPORT

NORTH YORK SOUTH DOWNTOWN E.A.

TRAFFIC DOCUMENTATION

The following report documents the information and the results of the traffic analysis undertaken in support of the Environmental Assessment for the transportation infrastructure for the North York South Downtown Secondary Plan. The report consists of the following parts:

- Need and Justification Background Information
- Arterial Road Traffic Operations
- Highway 401 Traffic Operations

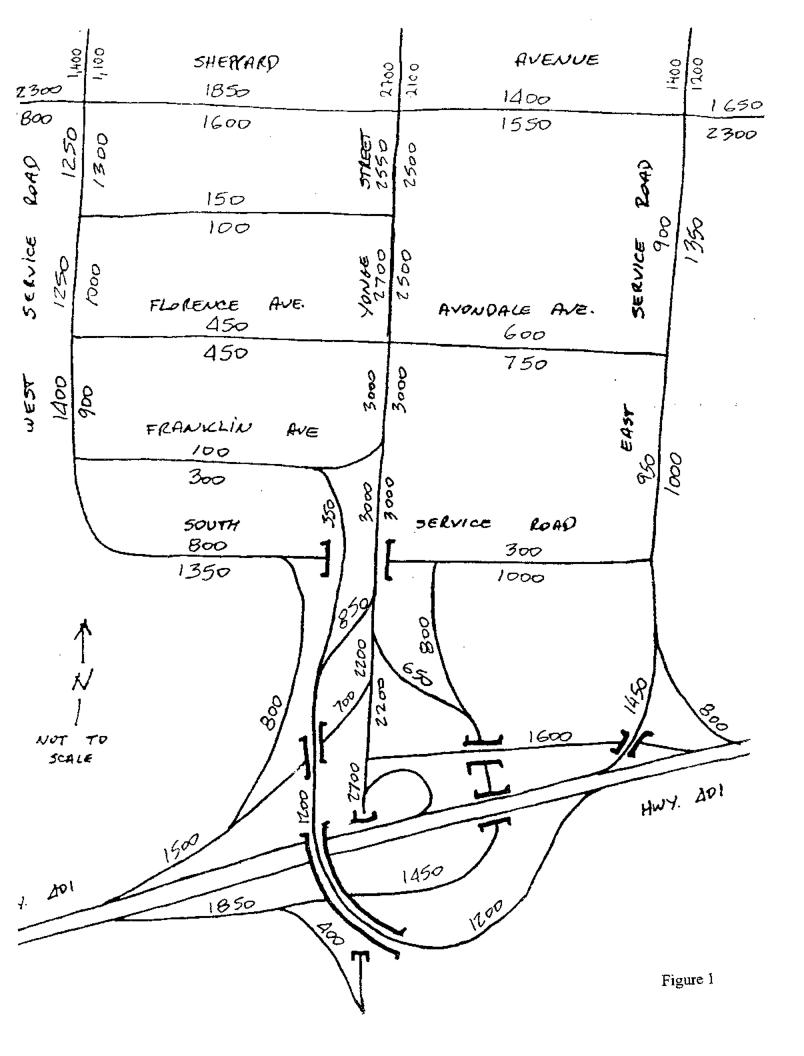
A NEED AND JUSTIFICATION BACKGROUND INFORMATION

The City of North York Transportation Department provided the following background information for the need and justification for the transportation improvements proposed for the south downtown under the VISION-2 scenario:

- 1. initial estimates of overall network capacity versus development potential
- 2. assessment of road link capacities (v/c) for initial land use scenarios (report #3)
- 3. comparison of uptown, downtown and south downtown development intensities
- 4. detailed link assignment (at 60% modal split) for four land use scenarios which lead to "the vision"
- 5. detailed link assignment (at 60% modal split) for "the vision"
- 6. some of the background data used in link assignments
- 7. comparative assessment of two alignments of Service Road (Doris) south of Avondale Avenue
- 8. Phase 1 Analysis BA Group
- 9. Phase 1 Analysis City of North York Transportation

The above information is contained in a binder available from the City of North York Transportation Department. Appendix A of this report includes exhibits of link volumes and links operating over capacity in the south downtown in the future PM peak hour under various land use alternatives.

Link volumes for the proposed development and transportation infrastructure improvements under the VISION-2 scenario are shown in Figure 1.



The land use and trip generation assumptions for this scenario are as follows:

1. Development

Westnor Site

	Floor .	Area			
	sq.m.	%	residents	res. units*	employees**
residential	249,205	65%	4,019	2,233	
non-res.	134,187	35%			4,473
TOTAL	383,392	100%	4,019	2,233	4,473

South Downtown (incl. Westnor)

	sq.m.	%	residents	res. units*	employees**
residential	787,190	62%	12,697	7,054	
non-res.	487,856	38%			16,262
TOTAL	1,275,046	100%	12,697	7,054	16,262

^{* 1.8} residents/unit

2. Trip Generation Rates (O.P.A. 343)

peak hour factor	45%
Car occupancy	1.2 persons/vehicle
absenteeism rate (emp.)	10%
walk/other	10%
transit modal split	60%

PM peak hour trip rates:

employment: 0.34 autos/100 sq. m outbound

off-peak direction (inbound) is 20% of peak

residential: 0.16 autos/res. unit inbound

off-peak direction (outbound) is 50% of peak

3. Parking Requirement

usual parking requirement rates

1 - 1.5 spaces /res. unit

1 - 2 spaces/ 1,000 sq. ft. of office/non-res. development

^{** 30} sq.m./employee

```
assuming 1.3 spaces/unit (per north York By-law for R.M. density 2,233 res. units will require approximately 2,900 parking spaces available for non-residential development (134, 187 sq.m. or 1,491,000 sq. ft.)
for a total of

1.100 (or 0.74 spaces/1,000 sq. ft.)
4,000 parking spaces

2,233 units will require approximately avail. for non-res. development
for a total of

1.800 spaces (1.2 spaces/1,000 sq. ft.)
4,000 parking spaces
```

More details about the land use assumptions for the various sites in south downtown are provided in Appendix B.

Trip Generation Rates

The following is a discussion of the sensitivity of trip generation factors and how rates used by the City of North York compare to trip generation rates calculated using data from the 1991 and 1986 Transportation Tomorrow Survey (TTS). This discussion deals primarily with the sensitivity of trip generation rates to factors such as modal split and attendance factor.

As shown in the attached table, the City of North York Transportation Department has calculated a future trip generation rate of 0.34 inbound vehicle trips per 100 sq.m. of development for the AM peak hour. This value was obtained using the following factors:

```
30 sq.m. per employee (i.e. 3.33 employees/100 sq.m.);
```

0.9 attendance factor (i.e. 90% of employees will go to work in the AM peak period);

0.3 auto modal split (i.e. 60% transit and 10% walk/cycle);

1.2 persons per vehicle;

0.45 peak hour factor (i.e. 45% of the peak period trips arrive within the peak hour).

Using information from the TTS, the trip generation rate can be calculated as the product of:

```
the number of employees per 100 m<sup>2</sup>, percent of daily trips per employee, percent of work trips in the peak period, modal split, no. of passengers per vehicle and the peak hour factor.
```

It should be noted that the product of 'percent of daily trips per employee' and 'percent of work trips in the peak period' is approximately equivalent to the attendance factor used in the trip generation rate calculations by North York. Trip generation rates were calculated for Planning District 11 and Planning District 1 of Metropolitan. Toronto using data obtained in the 1986 and 1991 TTS. Planning District 11 is the area of North York bounded by Dufferin Street, the Don River, Highway 401 and Steeles Avenue. This area includes the North York City Centre, as well as, established residential neighbourhoods. Planning District 1 in the City of Toronto, is bounded by Bathurst Street, the Don Valley Parkway, the lakeshore and Bloor Street. The detailed calculations for these trip generations are outlined in Tables 1 and 2.

A trip generation rate of 0.50 was calculated for Planning District 11 using the following 1986 TTS values:

- 0.77 daily work trips/worker;
- 0.75 work trips in peak period;
- 0.69 auto modal split.

A trip generation rate of 0.51 was calculated using the following 1991 TTS values:

- 0.78 daily work trips/worker;
- 0.71 work trips in peak period;
- 0.74 auto modal split.

The trip generation rate for 1991 is slightly higher than the rate for 1986 because the auto modal split increased. This is primarily a result of the decrease in the transit modal split which is consistent with the decreases experienced throughout Metropolitan Toronto.

A trip generation rate of 0.28 was obtained for Planning District 1 using the following 1986 TTS values:

- 0.76 daily work trips /worker;
- 0.79 work trips in peak period;
- 0.36 auto modal split.

A trip generation rate of 0.28 was obtained for Planning District I using the following 1991 TTS values:

- 0.8 daily work trips /worker;
- 0.77 work trips in peak period;
- 0.36 auto modal split.

The North York City Centre is expected to become a high density fully developed urban area, therefore, it is reasonable to assume that this area will produce a future trip generation rate similar to that which currently exists in downtown Toronto (Planning District 1). With the high density development, surface transit and rapid transit improvements that are expected for this area, it is

reasonable to assume a transit modal split of 60% in the future. The high density and mix of development that is expected for the area will also be able to support a 10% walk/cycle mode. Surveys show that in various areas in Metropolitan Toronto the walk/cycle mode represents 6% to 28% of the work based trips.

As noted above, the attendance factor was calculated as the product of the daily work trips/worker and the work trips made in the peak period. The attendance factor calculated from the 1991 TTS Data is 0.55 and the attendance factor calculated based on the 1986 TTS data is 0.58. North York has assumed a peak period attendance factor of 0.90 which is consistent with the absenteeism rate of 10% reported by the City of North York Human Resources Department, the building vacancy rate in the North York City Centre and the absenteeism rates used by Metropolitan Toronto and the City of Toronto. The assumed attendance factor of 0.90 implies a much higher participation of the work force in the morning peak hour trip making than the trip making participation indicated by the TTS data.

The assumed peak hour factor of 0.45 is representative of current patterns of work trip made by auto in the morning peak period. Assuming higher levels of congestion in the future and, possibly, peak period spreading, this factor could in theory go much lower than 0.40.

Tables 3 and 4 show combinations of modal split and attendance factor that may result in a trip generation rate of 0.34. Figure 2 is a sensitivity analysis to demonstrate the impact that changes in the absenteeism factor, the modal split and the peak hour factor have on the trip generation rate. Copies of TTS data summaries for Planning Districts 1 and 11 are also attached.

Trip Generation Rate

Trip Generation Rate calculated by the City of North York

		auto		Peak	Trip
# empl. per	AM peak period	modal	# empl.	Hour	Generation
100 sq.m.	attendance	split	per veh.	Factor	Rate
3.33	0.9	0.3	1.2	0.45	0.34

Table 1 - 1991 TTS Values

		k period dance					
	daily trips work trips		auto		Peak	Тпір	
# empi. per	per in peak		modal	# empl.	Hour	Generation:	
100 sq.m.	employee period		split	per veh.	Factor	Rate	Comments
3.33	0.8 0.77		0.36	1.2	0.45	0.28	PD1
3.33	0.78	0.71	0.74	1.2	0.45	0.51	PD11

Table 2 - 1986 TTS Values

		k period dance					
	daily trips work trips		auto		Peak	Trip	
# empl. per	per in peak		modal	# empl.	Hour	Generation	
100 sq.m.	employee	period	split	per veh.	Factor	Rate	Comments
3.33	0.78	0.79	0.36	1.2	0.45	0.28	PD1
3.33	0.77	0.75	0.69	1.2	0.45		PD11

Table 3 - Adjusting Modal Split Value

	daily trips	work trips	auto		Peak	Trîp	
# empl. per	per	in peak	modal	# empl.	Hour	Generation	
100 sq.m.	employee	period	split	per veh.	Factor	Rate	Comments
3.33	0.78	0.71	0.3	1.2	0.45	0.21	1991 PD11 TTS values - 30% modal split
3.33	0.78	0.71	0.5	1.2	0.45	0.34	1991 PD11 TTS values - 50% modal split

Table 4 - Adjusting Attendance

		auto		Peak	Trip	
# empl. per	AM peak period	modal	# empl.	Hour	Generation	
100 sq.m.	attendance	split	per veh.	Factor	Rate	Comments
3.33	0.8	0.3	1.2	0.45	0.30	NY values with attendance=80%
3.33	0.7	0.3	1.2	0.45	0.26	NY values with attendance=70%

Figure 2

Sensitivity Analysis of Trip Generation Rates

Attendance = 0.9

		auto modal split												
PHF	0.3	0.35	0.4	0.45	0.5	0.55	0.6	0.65	0.7					
0.35	0.26	0.31	0.35	0.39	0.44	0.48	0.52	0.57	0.61					
0.4	0.30	0.35	0.40	0.45	0.50	0.55	0.60	0.65	0.70					
0.45	0.34	0.39	0.45	0.51	0.56	0.62	0.67	0.73	0.79					

Attendance = 0.8

		auto modal split												
PHF	0.3	0.35	0.4	0.45	0.5	0.55	0.6	0.65	0.7					
0.35	0.23	0.27	0.31	0.35	0.39	0.43	0.47	0.51	0.54					
0,4	0.27	0.31	0.36	0.40	0.44	0.49	0.53	0.58	0.62					
0.45	0.30	0.35	0.40	0.45	0.50	0.55	0.60	0.65	0.70					

Attendance = 0.7

	auto modal split								
PHF	0.3	0.35	0.4	0.45	0.5	0.55	0.6	0.65	0.7
0.35	0.20	0.24	680):00:00:00:00:00:00:00:00:00:00:00:00:0	0.31	0.34	0.37	0.41	0.44	0.48
0.4	0.23	0.27	0.31	0.35	0.39	0.43	0.47	0.51	0.54
0.45	0.26	0.31	0.35	0.39	0.44	0.48	0.52	0.57	0.61

Attendance = 0.6

	auto modal splít								
PHF	0.3	0.35	0.4	0.45	0.5	0.55	0.6	0.65	0.7
0.35	0.17	0.20	0.23	0.26	0.29	0.32	0.35	0.38	0.41
0.4	0.20	0.23	0.27	0.30	0.33	0.37	0.40	0.43	0.47
0.45	0.22	0.26	0.30	0.34	0.37	0.41	0.45	0.49	0.52

PLANNING DISTRICT 1 MUNICIPALITY OF METHOPOLITAN TORONTO

12 O.6 4.0 Deliv Most Person face 11.1 0.8
--

24 hours 278,000 20,4 75% 14% 8% 24 hours 278,500 42% 175% 32% 28% 28% 190 117% 28% 24 hours 87% 50% 24 hours 85% 24 hours 56% 24 hours

Ima Period 6 · 9 a.m.

1408 337,000 316,400 811,500

24 hours

Tripa Made to Plenning Dietrici 1

% of 24 hr. 20.4 23.0

14ps 57,000 54 300

<u>Ilma Perlod</u> 6 - 9 a.m.

Trips Made by Residents of Planning District 1

TRIP PURPOSE

1981 TTS

144-301

PLANNING DISTRICT 11 MUNICIPALITY OF METROPOLITAN TORONTO

TOTAL NUMBER OF HOUSE: 54,400 TOTAL POPULATION; 132,000 Employment Shatus Employment Shatus Employment Shatus Employment Shatus Employment Shatus Espaiglia Espaiglia Employment Shatus Employment Shatus	TOTAL POPULATION: 122,000 133,000	Sundonii 1900
Ferral 2 3 4 5+ Male Papuleilon Licenced Full Peril Work at Peril Peril Work at Peril Peril Work at Peril Peril	House: 54% Other 46%	Sludeni 19%
Size 1 2 3 4 5+ Mailo Bizono 77% 45% 1% 1% 14% 6% 1% 14% 6% 1% 14% 6% 1% 1% 1% 1% 1% 1% 1	Licenced Butto Deal.	Sludenu S. Carte C
16% 49% 30% 4% 1% Age 38.4 11% 4% 14% 33% 19% Persons Workers Drivers Vehicles Trios/Dax 2.4 1.2 1.6 1.3 5.2 Dally trips/Person (age 11+) 2.4 Dally work trips/Worker: C	1 2 3 4 5+ Mate B2.000 77% 45% 1% 1/0 1/10 1/0 1/0 1/0 1/0 1/0 1/0 1/0 1/	、一般の一般は現代は、一般の一般に対して、 できれば、 で
Persons Workers Drivers Vehicles Trios/Day 2.4 1.2 1.6 1.3 5.2 Daily work trips/Worker:	0 1 2 3 4+ 4% 1% Moden Q-10 11-15 16-25 28-45 48-64	
	Workers Drivers Vehicles Trios/Day 1.2 1.6 1.3 5.2 Dally trips/Person (age 11+) 2.4 Dally work trips/Worker:	2000

		×		FileLos	University of forents University of forents Show the property of the propert
位 如 如 立			LEGEND 1991 TTS		RANSPORTATION TOMORROW SING
	MODE OF TRAVEL	Trips Made by Residents of Planning District (1	ocel GO Walk 905tl Trein & Cycle OI 24% 5%	Mean Trip Length: 7.2 5.7 9.8 (kilometres)	Trips Made to Planning Dierrict 11 Ilms Petical Trips Auto Auto Local GO Walk 6 - 9 a.m. 68,500 59% 15% 19% 0% 5% 2% 24 hours 310,500 65% 16% 15% 19% 0% 3% 11%
	TAIP FURPOSE		Time Parlog Tips % of 24 hr, HB-W HB-S HB-O N-HB 0 - 9 a.m. 00.000 21.2 55% 18% 19% 9% 24 hours 284,000 31% 31% 10% 44% 18% 2	within district: 6-9 a.m. × 31% 24 hours = 35%	Trips Made to Planning District 11 Trips Made to Planning District 11 Trips Period Trips % of 24 hr. Work School Home Other Trips 5.9 a.m. 68.500 22.1 55.9 21.4 57.5 24.5 57

B ARTERIAL ROAD TRAFFIC OPERATIONS

Existing Turning Movements

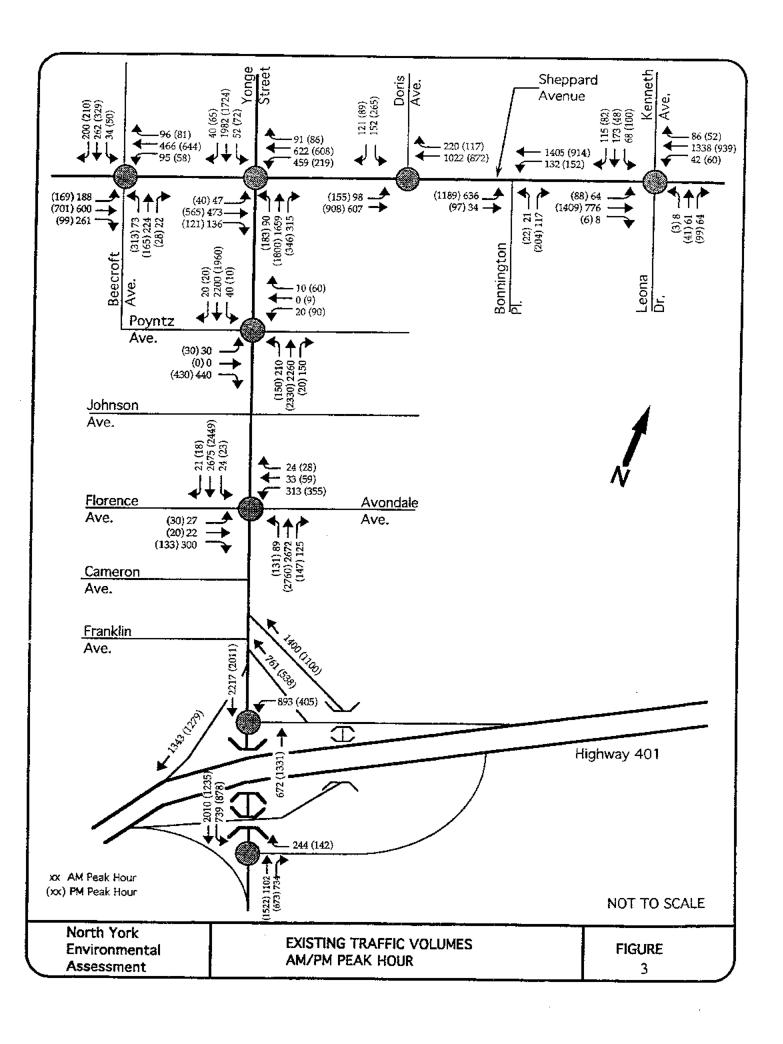
All existing turning movements, except the westbound Highway 401 to northbound Yonge Street ramp, were obtained from Metro counts. The west-north off ramp volume was obtained from the existing volumes used by the BA Group in their traffic impact study of the Westnor Development Project. The existing turning volumes are provided in Figure 3. The traffic volumes provided by the BA Group are contained in Appendix C. Included with these traffic volumes is a figure which outlines the Current/Committed Lane Configurations and Area Road System.

Future Turning Movements

Four designs were considered to account for various alignments of the service roads under future conditions. Traffic analyses were conducted for two of the four designs, these are design 1 "Tradewind Allignment" and design 3 "Midblock Allignment". Design 2 "Combination" produces the same traffic volumes as design 1 and design 4 "Modified Mid-block" produces the same traffic volumes as design 3.

The following table summarizes the sources from which the future turning movements were taken:

Intersection	AM Peak	PM Peak
Existing Intersections	Balanced future AM background traffic volumes provided by BA Group with the future link volumes provided by City of North York.	Balanced future PM background traffic volumes provided by BA Group with the future link volumes provided by City of North York.
Proposed Intersections	Reversed PM volumes and made minor adjustments to ensure volumes coming out of one intersection and going into the following intersection are equal.	BA Group
Existing Ramps	Reversed the PM volumes.	BA Group PM background volumes
Proposed Ramps	City of North York future ramp volumes	City of North York future ramp volumes



The future turning movements for design 1 are outlined in Figure 4 and the future turning movements for design 3 are outlined in Figure 5.

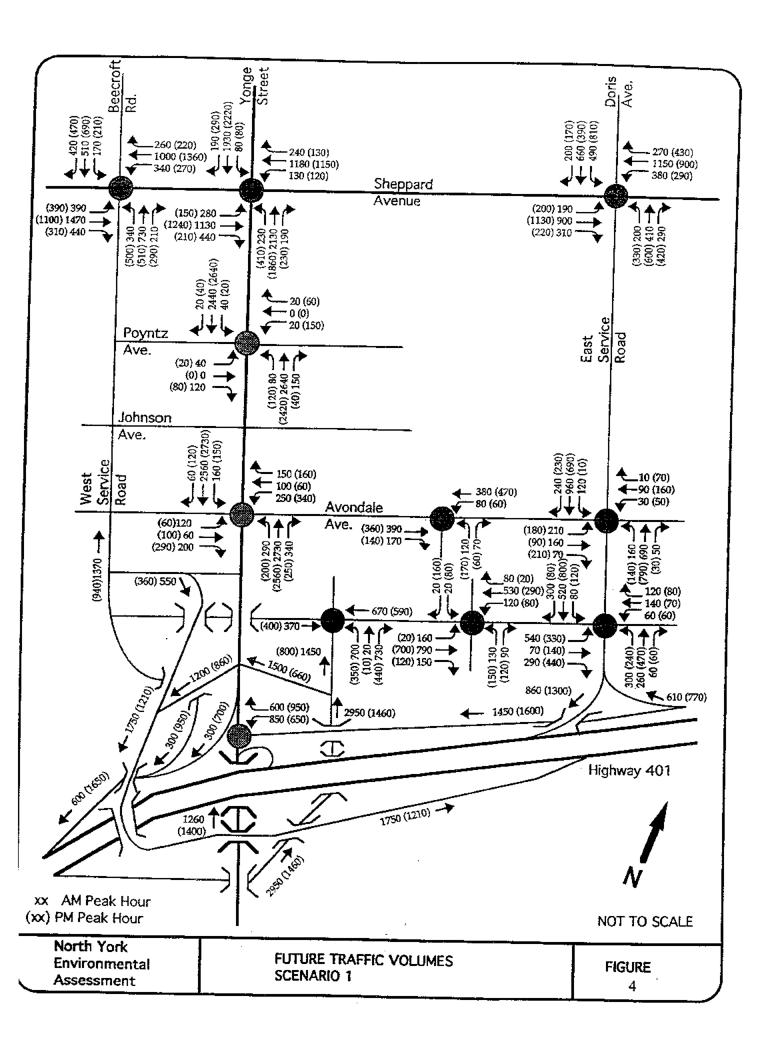
Capacity Analysis

The Highway Capacity Software was used to conduct the capacity analyses.

Under existing conditions capacity analysis was conducted for the AM and PM peak hours at all signalized intersections along Yonge Street between Sheppard Avenue and Highway 401, as well as the intersections of Sheppard Avenue with Beecroft Road and Doris Avenue. The existing volumes and existing traffic signal timing were used in the analysis, however some signal timing adjustments were required to keep the v/c ratio below 1.2. Since the traffic signals on Yonge Street are under SCOOT Control it is acceptable to adjust the signal timing for the existing conditions. At all intersections, except Yonge Street and Avondale Avenue, adjustments were made to the phase times but the cycle length remained the same. A saturation flow of 1800 vph and a peak hour factor of 0.95 were used in the analyses. For the analysis of the Avondale Avenue and Yonge Street intersection a saturation flow of 1900 vph and a peak hour factor of 0.98 were assumed due to the saturated conditions experienced at that intersection. The critical movements at these intersections are outlined in Table 5.

Capacity analyses were conducted for the future AM and PM peak hours at all existing and proposed signalized intersections in the study area. A saturation flow of 1800 vph and a peak hour factor of 0.95 were used in the analyses. The critical movements at the existing intersections along Yonge Street and Sheppard Avenue are outlined in Table 6 and the critical movements at the proposed intersections are outlined in Table 7. The level of service at these intersections are shown in Figures 6, 7 and 8 for designs 1 and 3.

The South Service Road and Westnor access intersection and the Avondale and Bales Avenue intersection were analyzed as both signalized and unsignalized intersections. The analysis of the South Service Road/Westnor access intersection indicates that traffic signals are not required for the movements on the main road, however traffic signals are required to serve the traffic exiting the access roads. Storage length requirements for the South Service Road intersections have been checked and it appears that the signalization of this intersection will not have adverse effects on the intersections of South Service Road/East Service Road and South Service Road/401 off ramp. The intersection of Avondale Avenue and Bales Avenue does not require traffic signals.



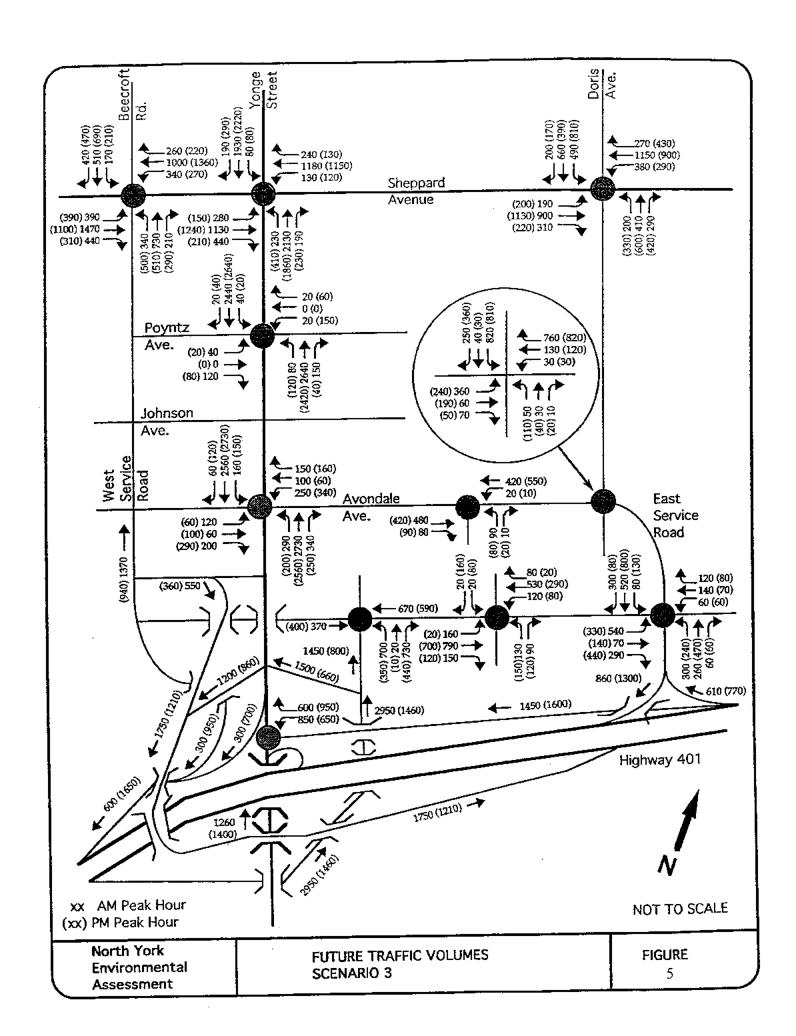


Table 5
Intersection Analysis - Existing Conditions

Intersection	Period	lr.	itersectio	ก	Cri	tical Mov	ement	
	1	v/c	delay	LOS	Movement	v/c	delay	LOS
Beecroft/Sheppard	AM Peak	0.711	13.3	В		Ī	<u> </u>	
Beecroft/Sheppard	PM Peak	1.013	36	D	EBLTR	1.05	55. 9	Е
	-				WBTR	0.92	28.4	Ď
	1				NBL	0.98	50.2	E
Yonge/Sheppard	AM Peak	0.961	27.9	D	WBL	1.02	61.5	F
	İ				NB L	1.19	202.4	F
	}				NBTR	0.9	23.2	C
					SBTR	0.9	23.2	С
Yonge/Sheppard	PM Peak	0.829	31.4	D	NBTR	0.97	25.7	D
					SB L	0.94	78	F
					SB TR	1.04	46.5	E
Doris/Sheppard	AM Peak	0.555	9.6	В				
Doris/Sheppard	PM Peak	0.756	10	В				
Kenneth/Sheppard	AM Peak	0.731	12	B				
Kenneth/Sheppard	PM Peak	0.607	10.8	В				
Yonge/Poyntz	AM Peak	0.876	23.3	¢	SB TR	0.96	27.6	D
-					NBTR	0.87	16.1	C
Yonge/Poyntz	PM Peak	0.859	16.9	С				
Yonge/Avodale	AM Peak	1.1	85.9	F	WB LTR	1.12	113.3	F
				ł	NBTR	1.08	64.3	F
					SB TR	1.17	115	F
Yonge/Avondale	PM Peak	1.165	98.4	F	WBLTR	1.15	118.9	F
					NBTR	1.18	111.6	F
					SB TR	1.14	89.7	F
Yonge/401 N	AM Peak	1.028	39.7	D	WB L	1.13	105.4	F
-					SB T	0.99	24.9	С
Yonge/401 N	PM Peak	0.848	10.5	В	SBT	0.88	10.3	В
Yonge/401 S	AM Peak	0.838	10.3	В	NB TR	0.88	20.1	С
Yonge/401 S	PM Peak	0.951	23.5	C	NB TR	1	33.2	D
_					SB L	1.02	33	D

critical if LOS = E or F

or if v/c >= 0.85 for through, v/c >= 1.00 for left or right

Table 6
Intersection Analysis - Future Conditions

Intersection	Period	İn	tersectio	n .	Crit	tical Mov	ement	<u>-</u> .
		v/c	delay	LOS	Movement	v/c	delay	LOS
Beecroft/Sheppard	AM Peak	1.017	75.5	F	EBTR	1.15	108.8	F
[WBL	1.13	125.7	F
					WBTR	0.94	41	E
					NBL	1.13	124.7	F
					NBTR	1.03	65.8	F
					SBR	1.04	79.6	F
Beecroft/Sheppard	PM Peak	1.023	76.2	F	EBL	1.03	71.9	F
	!				EBTR	1.12	98.1	F
	:				WBT	1.05	65. 6	F
					NBL	1.16	130	F
•					NBTR	1.16	124.7	F
					SBT	0.94	49.8	E
Yonge/Sheppard	AM Peak	0.998	63.4	F	EBL	1.13	126.1	F
					EBTR	1.12	93.3	F
					WBTR	1	49. 4	E
•		ļ		·	NBL	1.11	123.3	F
					NBTR	1.03	46.1	E
	:				SBL	0.99	113	F
					SBT	1.06	60.7	F
Yonge/Sheppard	PM Peak	1.059	101	F	EBL	1.04	119.6	F
					£8TR	1.18	130	F
		l			WBTR	1.03	62	F
		İ			NBL	1.14	120.3	F
		ı			NBTR	1.13	93.4	F
					SBT	1.18	122.6	F
Doris/Sheppard	AM Peak	1.055	71	F	EBTR	0.88	35.8	D
					WBL,	1.16	135.4	F
		i			WBTR	1.03	57.1	Е
		1			NBTR	1.16	129.7	F
					SBLTR	1.12	99. 9	F
Doris/Sheppard	PM Peak	1.092	95.9	F	EBTR	1.1	87.9	F
					WBL	1.13	131.2	F
					WBTR	1.11	93.6	F
					NBTR	1.16	122.8	F
					SBL.	0.91	48.7	E
					SBLTR	1.16	124.5	F
Yonge/Poyntz	AM Peak	0.729	15.1	С	· - · ·			
Yonge/Poyntz	PM Peak	0.782	17.9	C			-	
Yonge/401 North	AM Peak	0.83	16.5	С		0.04	10.4	
Yonge/401 North	PM Peak	0.863	15.4	υí	SBT	0.91	16.4	C
Yonge/Lord Seaton	AM Peak	0.732	13.7	В	NBTR	0.98	29.9	D
Yonge/Lord Seaton	PM Peak	0.76	9.8	В	NBTR	0.93	18.4	С

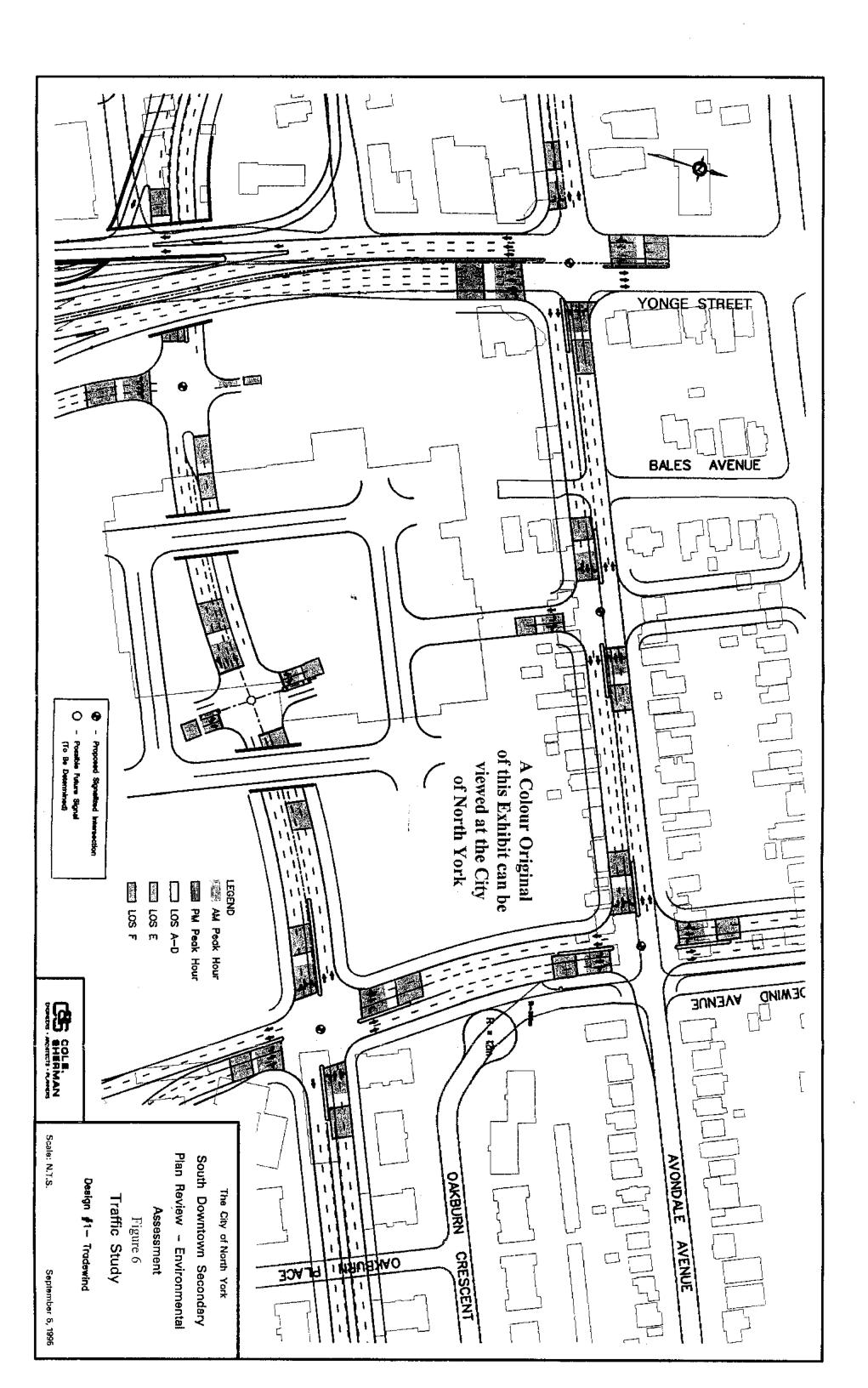
critical if LOS = E or F

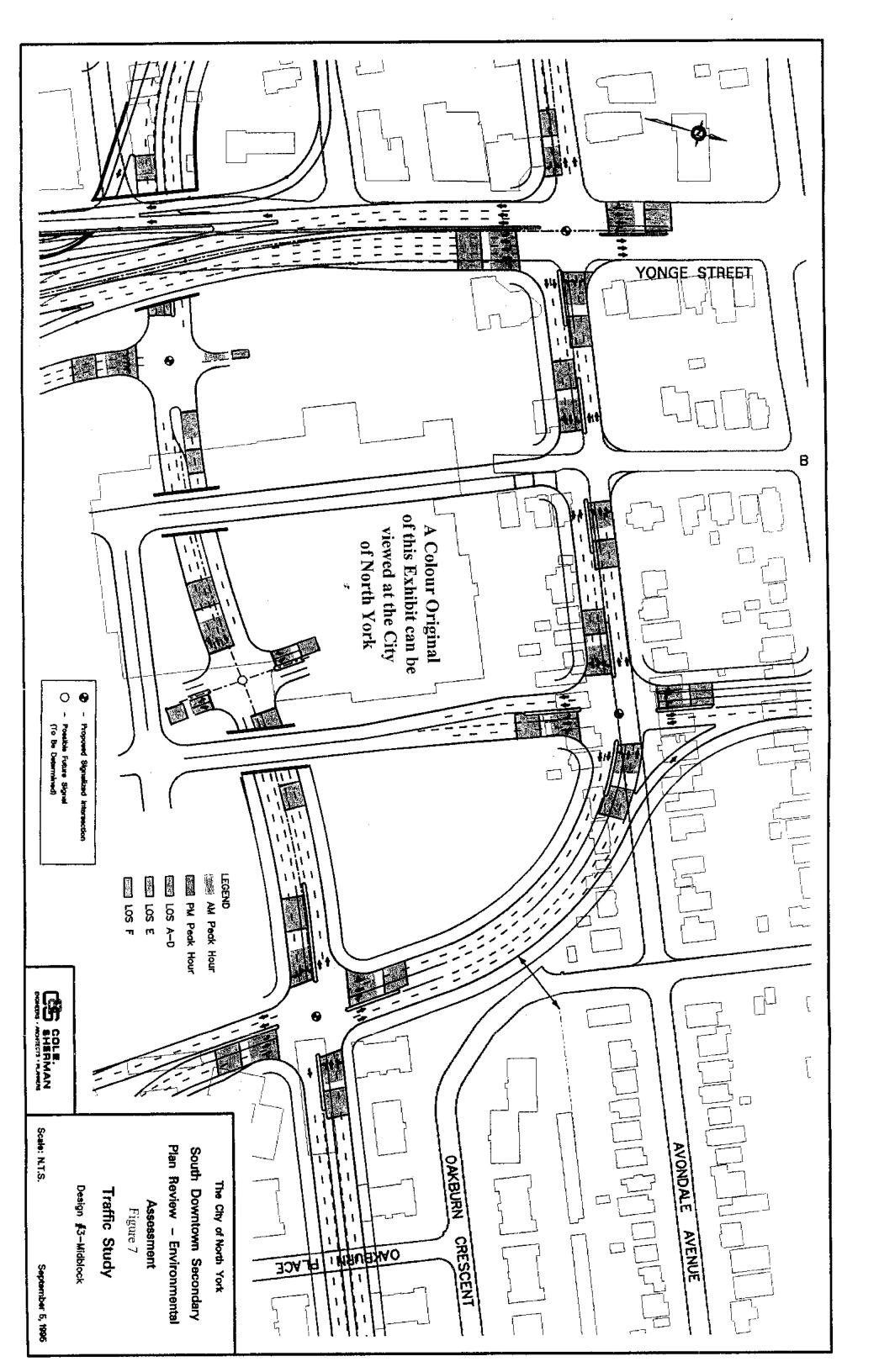
or if v/c >= 0.85 for through, v/c >= 1.00 for left or right

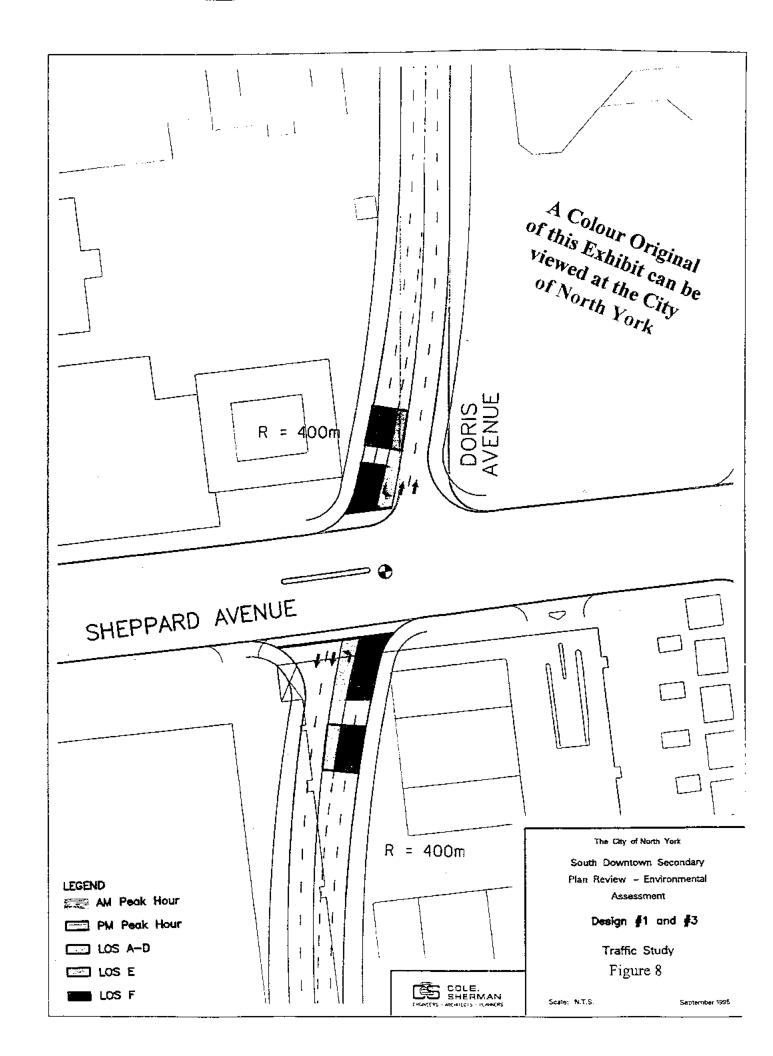
Table 7
Intersection Analysis - Future Conditions

Intersection	Period	lr Ir	tersection			tical Mov	rement	
		v/c	delay	LOS	Movement	v/c	delay	LOS
South Service Road/	AM Peak	0.726	14.9	В				
401 off ramp							l	l
South Service Road/	PM Peak	0.497	8.6	В		Ţ	1	<u> </u>
401 off ramp		<u> </u>]	L	<u></u>			
South Service Road/	AM Peak	0.466	9.9	В		I		
Wesnor Access						<u> </u>	L	
South Service Road/	PM Peak	0.465	8.8	В			T	
Wesnor Access			<u> </u>			l	<u>l</u> .	
East Service Road/	AM Peak	0.891	23.5	ņ	EBTR	0.85	25.7	Đ
South Service Road			<u> </u>		NBTR	0.87	35.1	D
		}	[:		SBTR	0.94	28,4	D
East Service Road/	PM Peak	0.855	24	C .	SBTR	0.85	23.6	C
South Service Road		1	ļ			-		
Avondale Avenue/	AM Peak	0.614	12	В			i	
East Service Road		1						
Design #1	1							
Avondale Avenue/	PM Peak	0.634	11.9	В	,		† · · · · · · · · · · · · · · · · · · ·	
East Service Road	1			_				
Design #1		}						
Avandale Avenue/	AM Peak	0.598	11.4	В.	··· ··· -· ··-			
East Service Road	1 /	1 0.555		_ [
Design #2								
Avondale Avenue/	PM Peak	0.577	10.7	В			 	
East Service Road	FIVITEAN	0.377	10.7					
	Ì							
Design #2 Avondale Avenue/	AM Peak	0.853	37.6	D	WBR	1.03	53.4	E
	Alvi reak	0.003	37.6	ا ت	AA DU	1.03	53.4	
East Service Road							•	
Design #3	D14 D1	0.000	24.0		ED)	0.00	44.0	
Avondale Avenue/	PM Peak	0.899	34.9	D	EBL	0.89	44.6	E
East Service Road				1	WBR	1.05	55.2	E
Design #3		2 24 5	22.2		NBL	0.82	40.8	E
Avondale Avenue/	AM Peak	0.615	22.2	Ç			!	
East Service Road		1						
Design #4	<u> </u>	1					<u> </u>	
Avondale Avenue/	PM Peak	0.697	22.9	С	·		į	
East Service Road		1 1	ł		1		!!	
Design #4	<u> </u>							
Avondale Avenue/	AM Peak	0.321	8.1	В	i		! !	
Proposed Road								
Design #1,2								
Avondale Avenue/	PM Peak	0.335	8	В				
Proposed Road]	ı			}	
Design #1,2	i		1		i			
Avondale Avenue/	AM Peak	0.294	8.1	В				
Proposed Road	1			1				
Design #3,4]			- 1			1	
Avondale Avenue/	PM Peak	0.278	8.2	В				
Proposed Road	1	}		[
Design #3,4]	, 1	l	ŀ				
Avondate Avenue/	AM Peak	0.9	49.9	E	NBL	1.11	107.4	F
Yonge Street		0		_ [NBT	1.08	61.3	F
, ongo dabet	1]		j	SBTR	1.04	44.8	E
Avondale Avenue/	PM Peak	1.042	48.2	E	EBR	1.17	157.4	F
	F INTERN	1	40,2	٠ ا	_ D1.1	1.13	[107,44	
Yonge Street	į.	1	l l	E	NBT	1.07	58.9	Ε

critical if LOS = E or F or if v/c >= 0.85 for through, v/c >= 1.00 for left or right







Storage Length Analysis

The storage length requirements were calculated for all four designs. The vehicle arrival rates were calculated for each movement at the intersections. The arrival rates for the left turn movements are based on a probability that 95% of the time vehicles will clear the intersection in one cycle. Using the Vehicle Arrival Rate Table provided in the Ministry of Transportation Geometric Design Standards the number of vehicles that will be stopped per cycle was determined. This number was multiplied by 7.5 metres, the average length of a vehicle, to determine the required storage. This adjustment for 95% probability of clearance results in an increase in storage length requirement of about 80% - 120% over the non-adjusted storage length requirement (depending on the arrival rate, this increase may range from about 45% to over 200%). The arrival rate for through and right turn movements was increased by 50% and rounded to determine the number of vehicles stopped per cycle, and was multiplied by 7.5 meters to determine the required storage.

At most intersections sufficient storage was provided, however there were a few critical intersections where storage length requirements could not be met, or where the lane configuration had to be adjusted to meet the storage length requirements. The storage length problems are primarily due to the close proximity of the proposed intersections.

The intersection of East Service Road and South Service Road could operate with only one eastbound left turn lane, however, there was a storage length problem in all the designs. A double left turn lane was provided at this intersection to meet the storage length requirement. Summarized below are storage length problems by design option.

Design #1 (Tradewind)

Intersection	Movement	Distance btwn Intersections (m)	Required Storage (m)	# of Lanes	Total Storage Provided (m)
Avondale/	SBTR	100	100	1	70
East Service	SBTR	100	130	1	70
		(Avondale - Glendo	ra)		
South Service	E/EBTR	150	130	1	120
East Service		(East Service - Wes	tnor access)		
Avondale/	WBL	100	150	2	125
Yonge Street	WBTR	100	100	1	70
Ü		(Yonge - Bales)			

Design #2 (Combination)

Intersection	Movement	Distance btwn	Required	# of	Total Storage
		Intersections (m)	Storage (m)	Lanes	Provided (m)
Avondale/	SBTR	100	100	1	70
East Service	SBTR	100	130	1	70
		(Avondale - Glendor	ra)		

South Service East Service	/EBTR	150 (East Service -	130 Westnor access)	1	120
Avondale/	WBL	100	150	2	135
Yonge Street	WBTR	100	100	1	75
-		(Yonge - Bales	3)		

Design #3 (Mid-block)

Intersection	Movement	Distance btwn Intersections (m)	Required Storage (m)	# of Lanes	Total Storage Provided (m)
Avondale/	SBTR	100	100	1	70
East Service	SBTR	100	130	1	70
		(Avondale - Glendo	ora)		
	EBL	110	115	1	65
		(East Service - Prop	osed Rd)		
	WBR	220	210	1	160
		(East Service - Sout	h Service)		
South Service	:/EBTR	150	130	1	120
East Service		(East Service - Wes	tnor access)		
Avondale/	WBL	100	150	2	135
Yonge Street	WBTR	100	100	1	75
		(Yonge - Bales)			

Design #4 (Modified Mid-block)

Intersection	Movement	Distance btwn Intersections (m)	Required Storage (m)	# of Lanes	Total Storage Provided (m)
Avondale/	SBTR	100	100	1	70
East Service	SBTR	100	130	1	70
		(Avondale - Glendor	ra)		
	EBL	110	115	1	65
		(East Service - Prope	osed Rd)		
South Service	e/EBTR	150	130	1	120
East Service		(East Service - West	nor access)		
Avondale/	WBL	100	150	2	135
Yonge Street		100	100	1	75
5		(Yonge - Bales)			

The storage length problems for designs 1 and 2 could be eliminated by:

- closing Glendora Avenue at the East Service Road to eliminate the southbound storage length problems at the Avondale/East Service Road intersection;
- providing an exclusive right turn lane for the eastbound movement at the South Service/East Service intersection;
- eliminating through movements at the Avondale/Yonge intersection so that the WBTR lane could be designated an exclusive right lane;

Providing these adjustments would eliminate all storage length problems except for the westbound left turn movement at Yonge and Avondale. Two left turn lanes are provided for this movement with the left most lane being 60m long and the adjacent left turn lane being 75m long. The left most lane is shorter because a 15m eastbound left turn lane is provided at the Avondale/Bales intersection west of Yonge St. With this design, the westbound left turn movement at Yonge and Avondale would operate with a 90% probability that the left turn vehicles will not back up into the upstream intersection (Avondale/Bales). However, a capacity analysis for the intersection of Avondale and Bales has shown that an exclusive lane for eastbound left turns into Bales is not needed. Therefore, if the left turn lane into Bales is not provided, the westbound double left turn lane at Avondale/Yonge would provide sufficient storage length (150m) for left turning vehicles.

These same solutions could be provided for designs 3 and 4, however there would still be storage problems at the intersection of Avondale Avenue and East Service Road. Designs 3 and 4 have a storage problem for the eastbound left turn movement and design 3 also has a storage length deficiency for the westbound right movement.

Storage length requirements for the unsignalized intersections, at the South Service Road/Westnor access and Avondale Avenue/Bales Avenue, was conducted for AM and PM peak hours. The Ministry of Transportation Geometric Design Standards was used to determine the storage length requirements. A left turn storage lane is required in both the eastbound and westbound directions at the South Service Road and Westnor access intersection and a left turn storage lane is required for the westbound movement at the Avondale Avenue and Bales Avenue intersection.

Progression Along the Corridor

Progression analysis was conducted along the corridor using PASSER II-90 and TRANSYT-7F. The analysis indicates that it may not be attainable to provide progression long the East and South Service Roads because there is a lot of side friction which makes it very difficult to have progression, however this analysis was used to establish offsets between intersections.

An assessment of opportunities for coordination of traffic signals was undertaken using PASSER II-90 and TRANSYT-7F. The analysis indicates that it may be difficult to provide good progression along the East Service Road and especially along the South Service Road because there are high volumes of turning traffic which are not conducive to the coordination of signals. However, the analysis showed that offsets in the order of 4 - 10 seconds would allow the intersections to operate without queuing problems. More detailed analysis should be undertaken once the improvements have been implemented and actual traffic counts have been taken.

C HIGHWAY 401 TRAFFIC OPERATIONS

- Analysis of Hwy 401 operations was undertaken using MTO's INTEGRATION model.
 This model is set up separately by direction of travel and period of travel (am peak & p.m. peak) i.e. four sub-models
- Loading of the network is based on a 1986 simulated matrix of trip flows between pairs of on and off ramps. (this matrix has been adjusted to 1991/92 ramp volumes)
- Only the eastbound, a.m. peak period has been calibrated by the developers of the program.
- For purposes of the North York study, CSA has:
 - combined the two directions into one network
 - added ramp detail at the Yonge St. interchange
 - trimmed the network to include Hwy 401 between Hwy 404 and 400

This was done in order to reduce simulation run time and capture the effects of ramp and arterial road operations onto freeway operations.

In addition, CSA has enhanced the coding of the network by providing UTM coordinates for the nodes. This way, the graphical representation of the network on the screen is more realistic with respect to the network's actual geographic location.

- Calibration of CSA's enhanced network (including saturation flow and congested speed adjustments) is based on volume and speed information provided by MTO-FTMS for October 11-13, 1994 and November 23, 1994.
- Because of the discrepancies between observed traffic counts and the trip tables provided by MTO, some modifications were made to these trip tables. Volumes on Yonge Street ramps, were adjusted to reflect observed peak hour traffic counts, using the same origin-destination ratios as was found in the base table. Also trip tables provided by MTO reflected volumes that were only 20-30% of observed traffic counts for eastbound p.m. peak period traffic. The trip tables were factored up to match observed counts.

An additional modification to the network was necessitated by the need to analyze weaving problems between the westbound core-collector diversion and the Avenue Road off-ramps. To handle this analysis, lanes were divided between weaving lanes and non-weaving lanes for this section, and saturation flows were reduced for the weaving lanes to reflect the friction caused by weaving vehicles.

- Some discrepancies in the coding of number of lanes were found in the networks provided by MTO. The number of lanes on all links were verified against the Highway 401 lane continuity diagram and the following changes were made.
 - One westbound collector lane added from Highway 404 to Yonge Street off-ramp

- One westbound collector lane added between Avenue Road on-ramps
- One westbound core lane removed between Leslie St and collector-core diversion
- One eastbound collector lane removed between core-collector diversion and Leslie Street off-ramp
- The future network was modified to include the assumed future changes at the Yonge Street ramps:
 - add one additional lane to westbound collector lanes from the first Yonge Street onramp to the first Avenue Road on-ramp
 - extend E-NS ramp and provide off-ramp connection to new Service Road
 - add a new off-ramp connection from W-N ramp to new Service Road
 - prohibit left turn from Southbound Yonge to Lord Seaton Drive (current N-E movement)
 - add new flyover for N-E ramp movement
 - add new lane to NS-E on-ramp merge lane
 - add new N-W ramp connection from new Service Road
 - a new centroid was added to represent trips in and out of the new Service Road and its freeway ramp connections.
- The following scenarios were considered for analysis of traffic operations on Highway 401:
 - Existing Conditions
 - Future Do Nothing
 - VISION

The analysis was undertaken for both AM and PM peak periods. For the Do Nothing scenario (exisiting interchange configuration), mainline volumes for Highway 401 were obtained from the Ministry of Transportation EMME/2 model. The ramp volumes were rationalized on the basis of the future development in the North York City Centre excluding the South Downtown. The rationalization and the ramp volumes are provided in Tables 8 and 9. For the VISION scenario, trip linkages were growth factored to total the future study area ramp volumes as obtained from the North York Transportation Department traffic assignments.

Table 10 summarizes the travel time outputs of the INTEGRATION model for the sections of Highway 401 between Avenue Road and Bayview Avenue, and between Highway 400 and Highway 404 by direction of travel, time of operation and analysis scenario. Figures 9-14 display the simulated travel speeds on the section of Highway 401 between Avenue Road and Bayview Avenue for the scenarios considered in this analysis.

Table 8

Rationalization of "Do Nothing" Ramp Volumes **NORTH YORK - VISION 2**

Devel	Development (sq.m.)			Traffic (vph)	
Foliation	South Downtown	Total"		AM Peak Hour	PM Peak Hour
retail/office	57,600	637,000	to Hwy. 401	2,080	2,160
residential	. 006,89	626,000 1.263.000	from Hwy. 401	2,160	1,640
Future Do Nothing					. •
retail/office	58,000	1,948,000	to Hwy. 401	2,640	3,160
residential	000'69	2,304,500	from Hwy. 401	3,160	2,410
Vision					
retail/office		2,378,000	to Hwy. 401	3,210	4,160
residential	787,000	3,022,500 5,400,500	from Hwy. 401	4,160	3,180
		,			

^{*} traffic on all ramps from/to the north
** includes Uptown, Downtown and South Downtown

Table 9
HIGHWAY 401 RAMP VOLUMES @ YONGE STREET INTERCHANGE

	EXISTING	DO NOTHING	VISION
AM PEAK HOUR			
WESTBOUND OFF	1,400	1,800	2,100
ON	2,000	2,100	2,200
EASTBOUND OFF	2,100	2,550	2,950
ON	1,350	1,900	2,500
PM PEAK HOUR			
WESTBOUND OFF	850	1,250	1,600
ON	1,950	2,450	2,950
EASTBOUND OFF	1,650	1,850	2,000
ON	1,600	1,750	1,900

TRAVEL TIME (minutes)

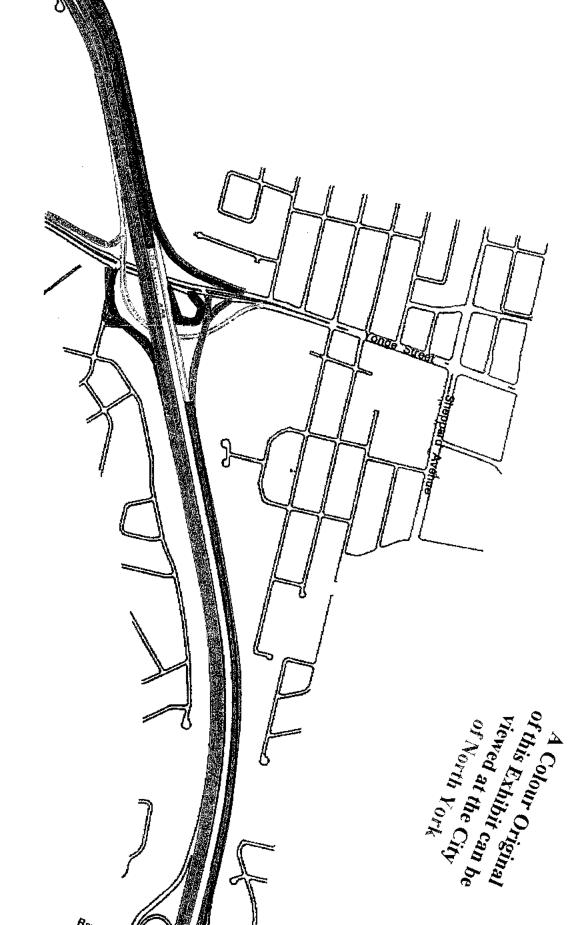
			Free Flow	Existing	Do Nothing	Viston
				•	with Background Growth	nd Growth
AM PEAK HOUR	AVENUE RD	AVENUE RD BAYVIEW AVE.			X	
	Westbound	collector core	2.51	9	11	5 8
٠	Eastbound	collector core	- ରାଷ	ღღ	മഹ	~ ~
	HIGHWAY 400	HIGHWAY 400 - HIGHWAY 404				
	Westbound	collector	88	20 15	31	30 16.
	Eastbound	collector	ဆဆ	41 0	23 16	21 16
PM PEAK HOUR	AVENUE RD	AVENUE RD BAYVIEW AVE.				
	Westbound	collector core	2 2	33	8 7	9 8
	Eastbound	collector core	00	7	10	7 13
	HIGHWAY 400	HIGHWAY 400 - HIGHWAY 404				
	Westbound	collector core	& &	9	18	19
	Eastbound	collector core	& &	27	23	35 27

Avenue Road - Bayview Avenue

3	Core	
ယ	Collector	EB
7	Core	
မ	Collector	WB

Highway
400 - I
⊀ighway
404

10	Core	
14	Collector	E8
15	Core	
20	Collector	ВW



PEAK HOUR AVERAGE OPERATING SPEED

80 kph and above

60-80 kph

40-60 kph

below 40 kph

BHERMAN MONICITY - NAMEDS

Scale: N.T.S.

South Downtown Secondary The City of North York

Plan Review - Environmental Assessment Figure 9

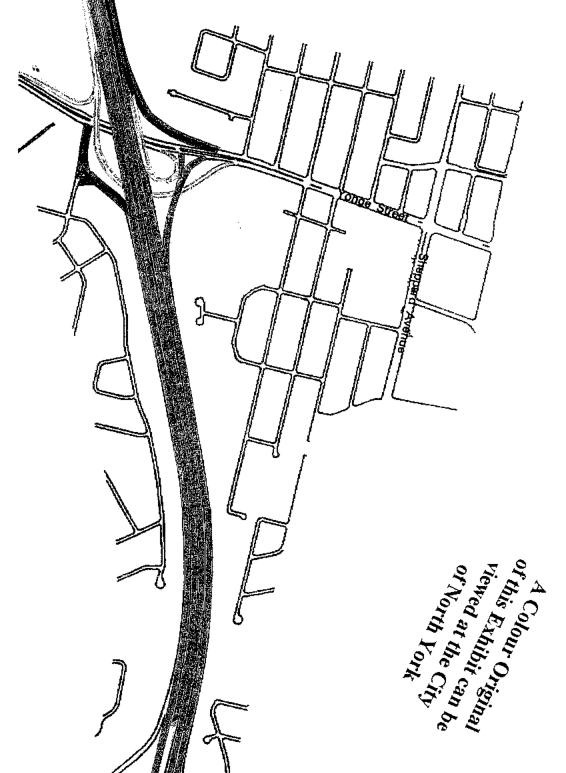
(Integration Software) Existing Conditions Highway 401

Avenue Road - Bayview Avenue

i	E		WB
Core	Collector	Core	Collector
7	7	ω	ယ

Highway 400 - Highway 404

	EB		WB
Core	Collector	Core	Collector
- - 200	27	9	<u>"</u>



PEAK HOUR AVERAGE OPERATING SPEED



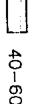
60-80 kph

Plan Review - Environmental South Downtown Secondary

The City of North York

Bayyin

80 kph and above



40-60 kph



below 40 kph



Scale: N.T.S.

September 1996

(Integration Software)

Highway 401

Existing Conditions

Figure 10 Assessment

TRAVEL TIME (minutes)

Avenue Road - Bayview Avenue

Core	EB Collector	Core	WB Collector
5	&	7	<u> </u>

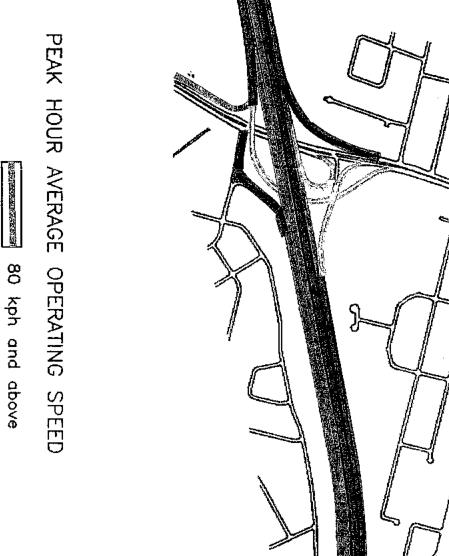
Highway 400 - Highway 404

16	Core	
23	Collector	B
17	Core	
31	Collector	₩B

HUM	AM - I (with I
	AM - FUTURE DO NOTHING (with background growth only)
) NOTHING growth only)

viewed at the City

of this Exhibit can be



60-80 kph

40-60 kph

below 40 kph



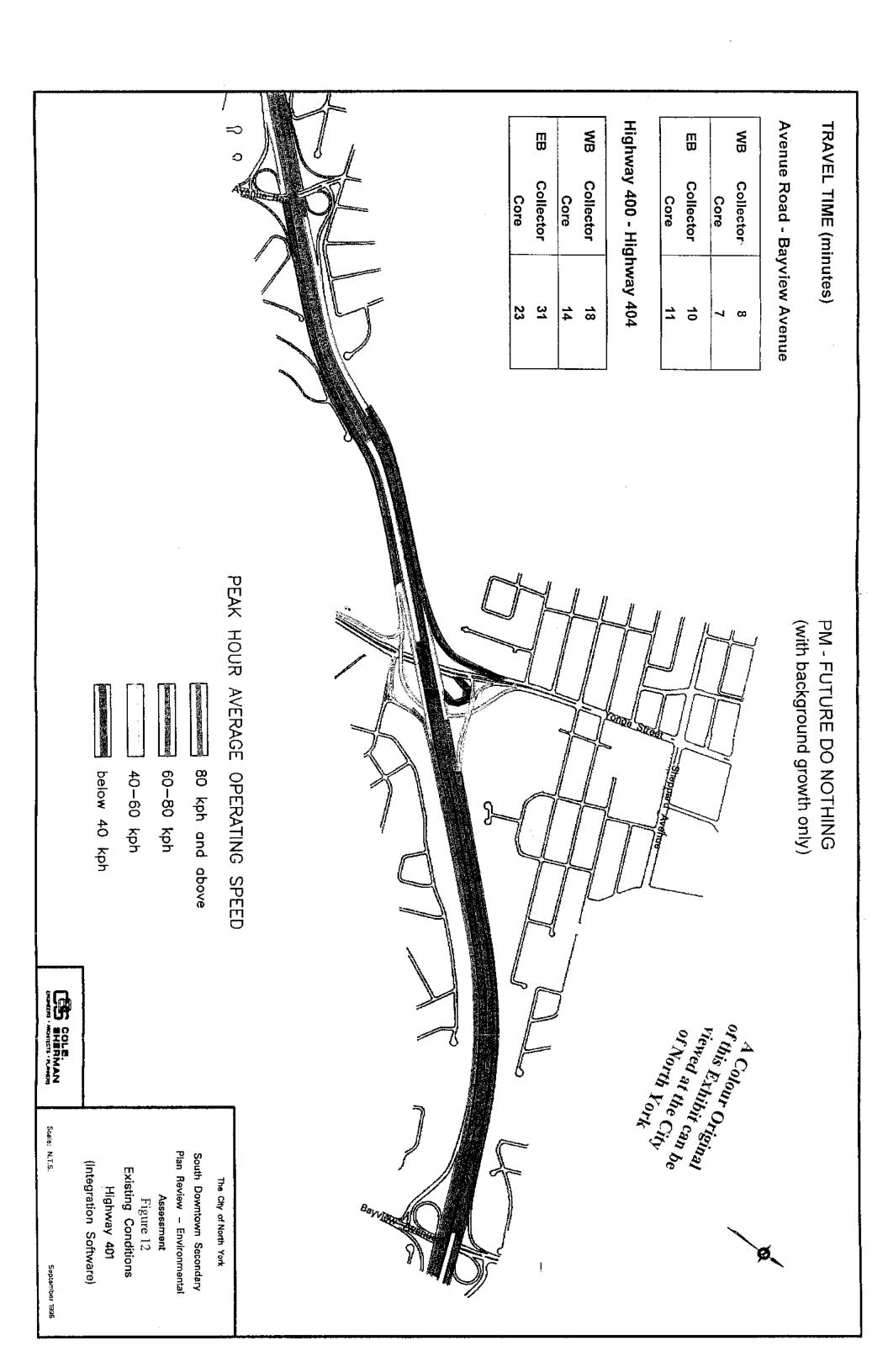
The City of North York

Plan Review - Environmental South Downtown Secondary Assessment Figure 11

(Integration Software) **Existing Conditions** Highway 401

Scale: N.T.S.

Saptember 1995



TRAVEL TIME (minutes)

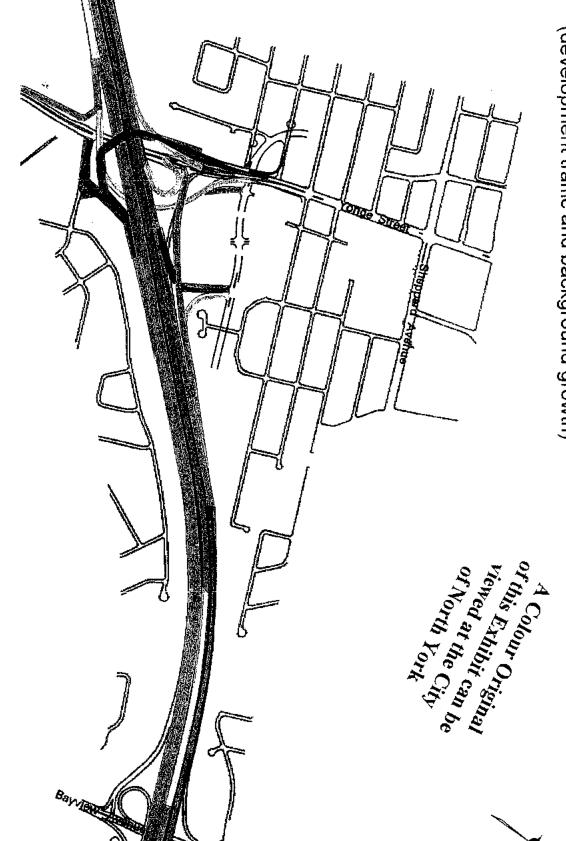
Avenue Road - Bayview Avenue

	EB		WB
Core	Collector	Core	Collector
7	7	8	(J)

Highway 400 - Highway 404

	EB		WB
Core	Collector	Соге	Collector
16	21	16	30

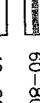
(development traffic and background growth) AM - FUTURE WITH IMPROVEMENTS



PEAK HOUR AVERAGE OPERATING SPEED



80 kph and above



60-80 kph







The City of North York

Plan Review - Environmental South Downtown Secondary Assessment

Figure 13
Future Conditions Highway 401

(Integration Software)

September 1995

Scale: N.T.S.

TRAVEL TIME (minutes)

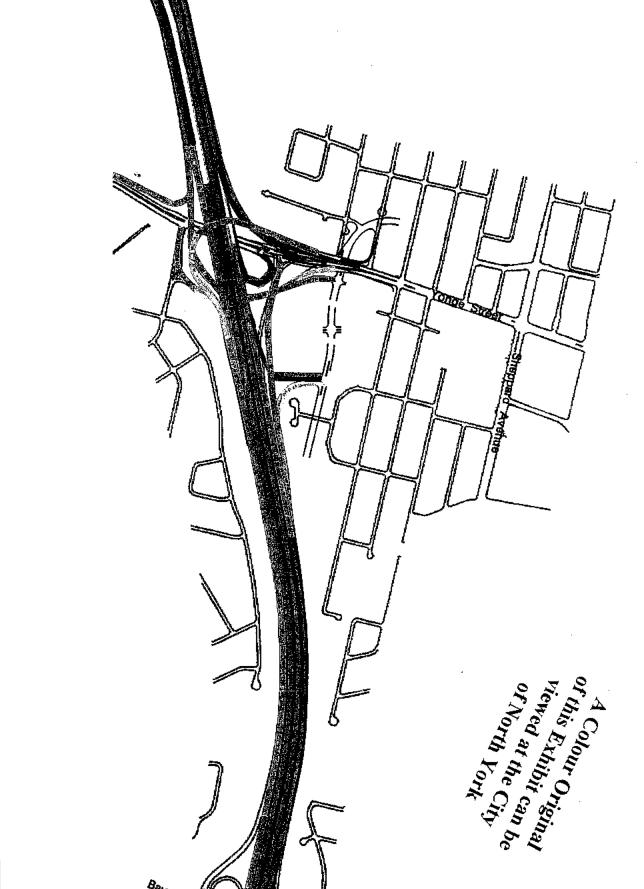
Avenue Road - Bayview Avenue

	8		₩B
Core	Collector	Core	Collector
13	7	8	ത

Highway 400 - Highway 404

Core	EB Collector	Core	WB Collector
27	35	15	19

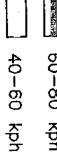
(development traffic and background growth) PM - FUTURE WITH IMPROVEMENTS



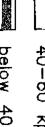
PEAK HOUR AVERAGE OPERATING SPEED



80 kph and above



60-80 kph



below 40 kph



The City of North York

Plan Review - Environmental South Downtown Secondary

Assessment

Future Conditions Highway 401 Figure 14

(Integration Software)

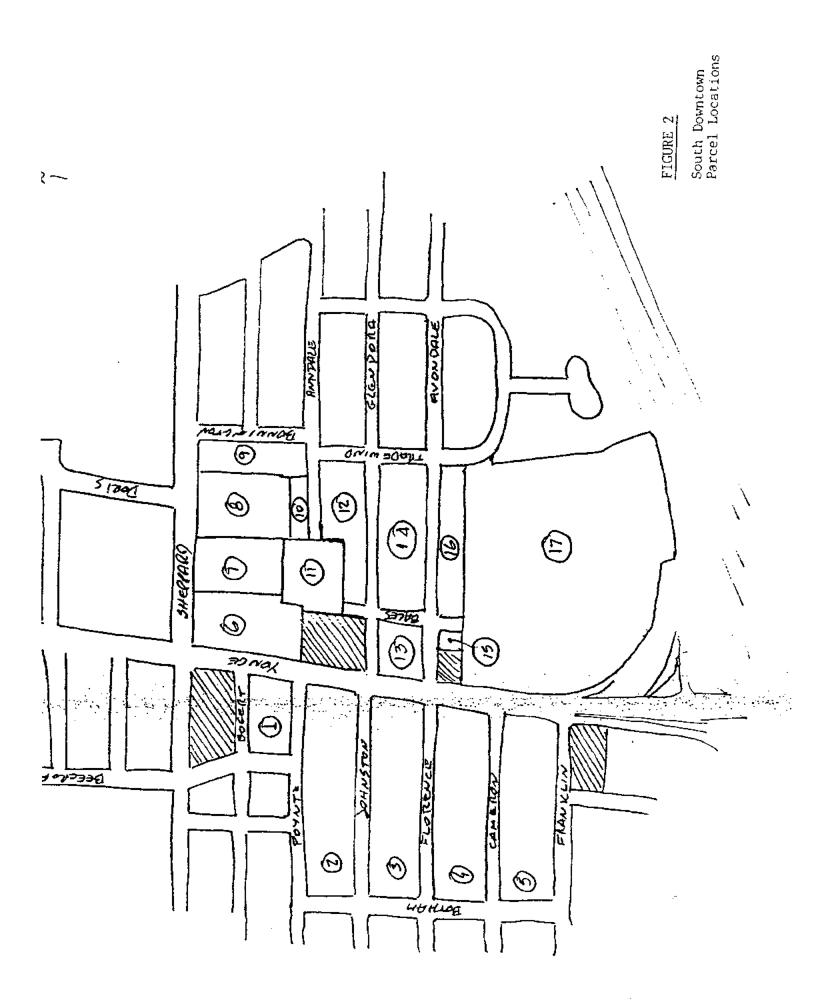
Scale: N.T.S.

D Conclusions

- Arterial roads and certain intersections in the study area (e.g. Yonge/Sheppard, Yonge/Avondale)
 are presently near or at capacity. Also, most sections of Highway 401 and its ramps within the
 study operate at or near capacity.
- Yonge Street and the existing ramps to/from Highway 401 do not provide sufficient access capacity for the proposed redevelopment of the South Downtown.
- The proposed system of service roads and new freeway ramps would provide the necessary capacity, as well as better balance of traffic flows, and enhanced and flexible circulation of traffic in the South Downtown area.
- All signalized and select unsignalized intersections of the proposed system of arterial roads, service
 roads and ramps were analyzed in terms of levels of service, storage length requirements and
 progression considerations for two alternative alignments. Intersection configuration adjustments
 and other design refinements were undertaken (as necessary) to ensure that the road system would
 operate without undue delays or queue spill overs.
- Analysis of future conditions on Highway 401 indicates that, with the proposed ramps and the
 additional westbound collector lane from Yonge Street to Avenue Road, the proposed
 redevelopment of the South Downtown would not have any adverse impacts on Highway 401
 operations when compared with the conditions expected to prevail on Highway 401 under a future
 "Do Nothing" situation.

	·	

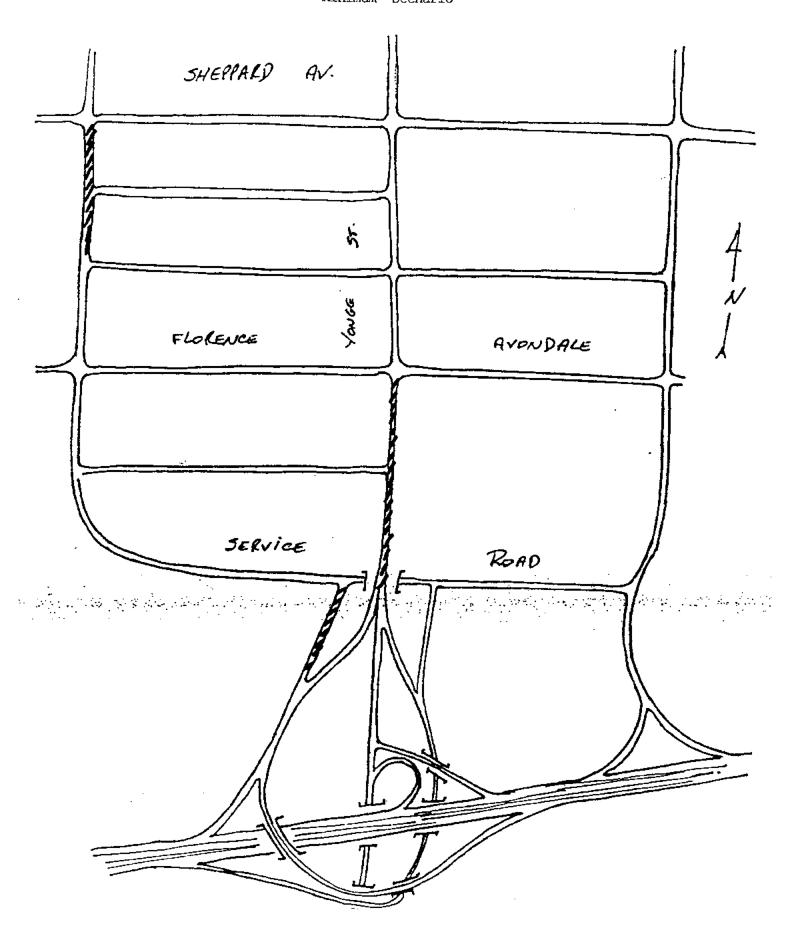
APPENDIX A



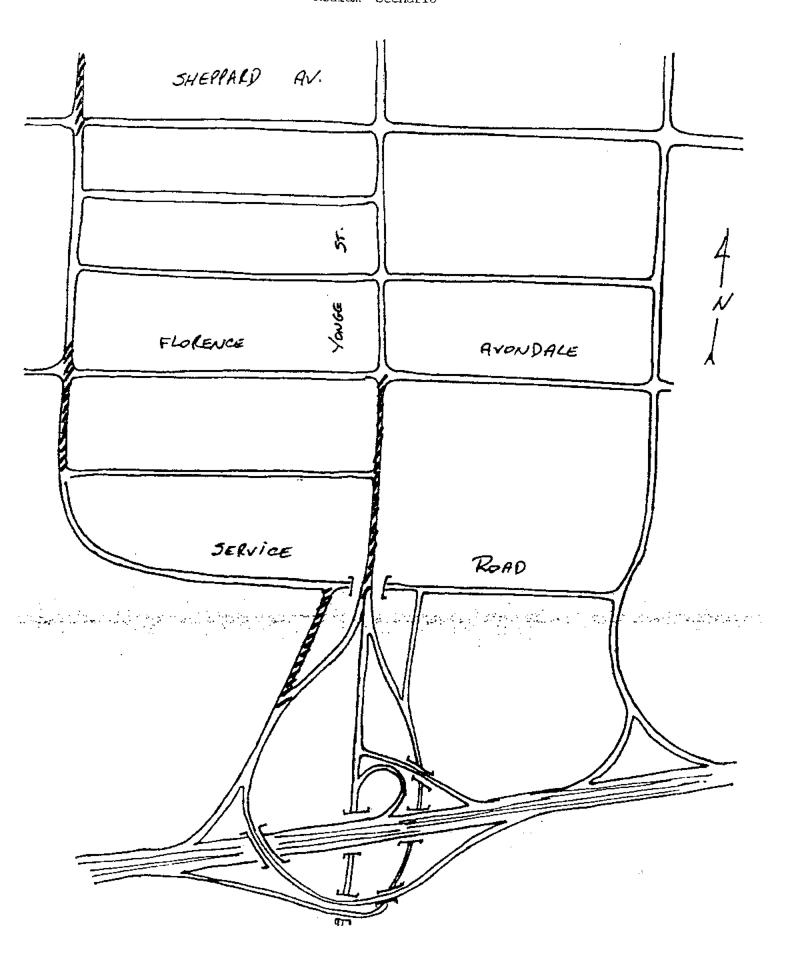
Land Use
Densities and Areas
(Sq. M.)

MAXIMUM SCEN.	4 50 32878 08		۲	-		4.50 92538,66	4.50 112095,26	4.50 43971.07					4:50 41805.00	4.50 46600.08	4.50 24812.18)	4.50	4.50 33400.14	4	1320194.46
MEDIUM SCEN.	4.50 32676.06	4.00 86829.28	·				_			2.00 11271.07	2.00 5538,79	_			3.50 19298,36	2.00 29480.38	1.50 1321.04	•	1.50 11133,38	1.50 144840.00	703448,43
MINIMUM SCEN.	4.50 32676.06	1.50 32560.98	1.50 33609.81	1.50 32229.54		•	-		-	~		2.00 18580.00	1.50 15533.38	4 60 00101		N	1.50 1321.04	1.50 11122.39	•	1.50 144840.00	580791,53
"EXISTING" SCEN.	4.50 32676.06		_		1.50 30846,22	4.50 112095.26					5.00 0.00 0.00 0.00		1.50	50 8270 73				.50 0.00	50 144840 pp		496624.63
PAR. PARCEL NO. (SQ. MT.)		_ `	_ '	•	20564.15	24910.06	7 9771.35 4	12101.96	5635.54	2769.40		4 00.00	10305.57	5513.82	14740.19	880.70	7400.70	7422.25	17 96560.00 1	•	TOT. 293376,55

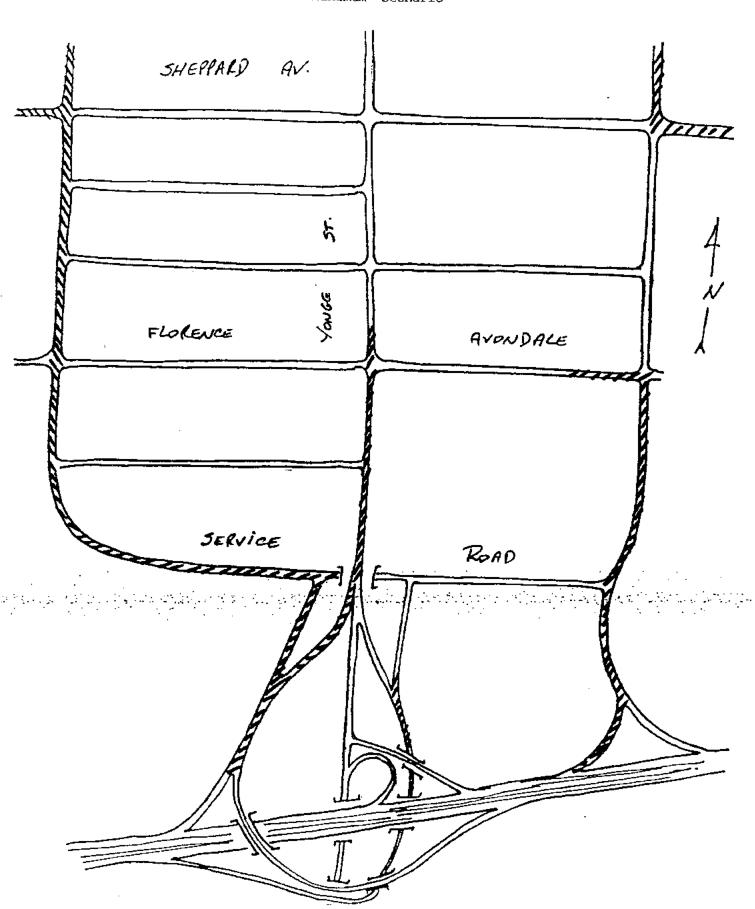
FIGURE 8
Links Over Capacity
"Minimum" Scenario



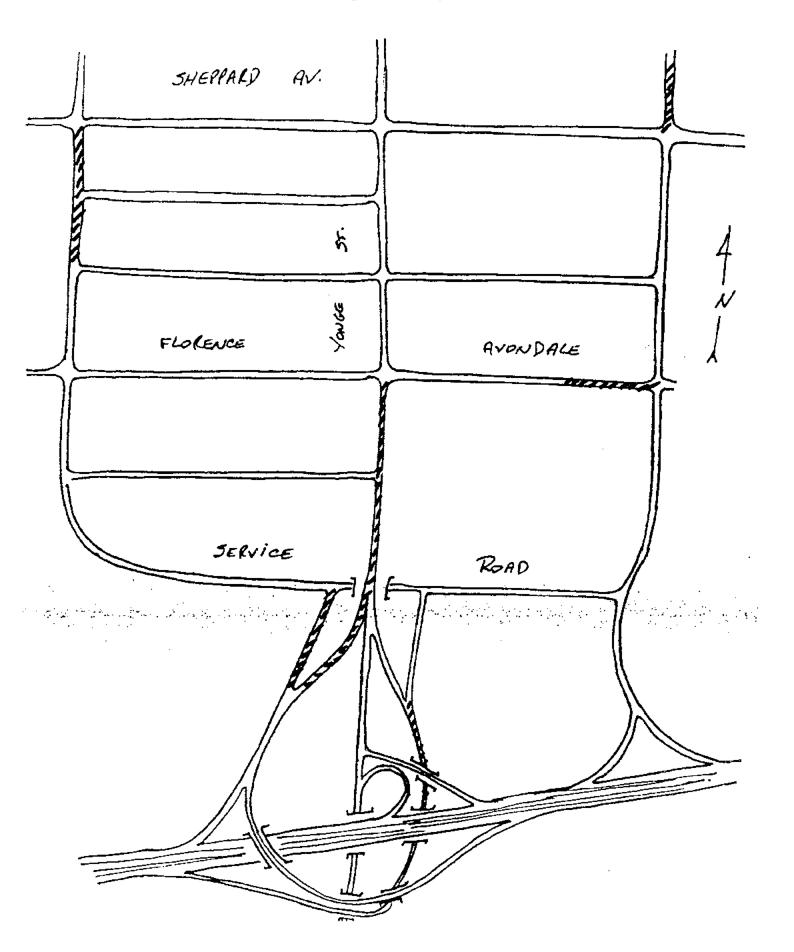
"Medium" Scenario



"Maximum" Scenario



"Average" Scenario



DETAILED LINK ASSIGNMENT (AT 60% MODAL SPLIT) FOR FOUR LAND USE SCENARIOS WHICH LEAD TO "THE VISION"

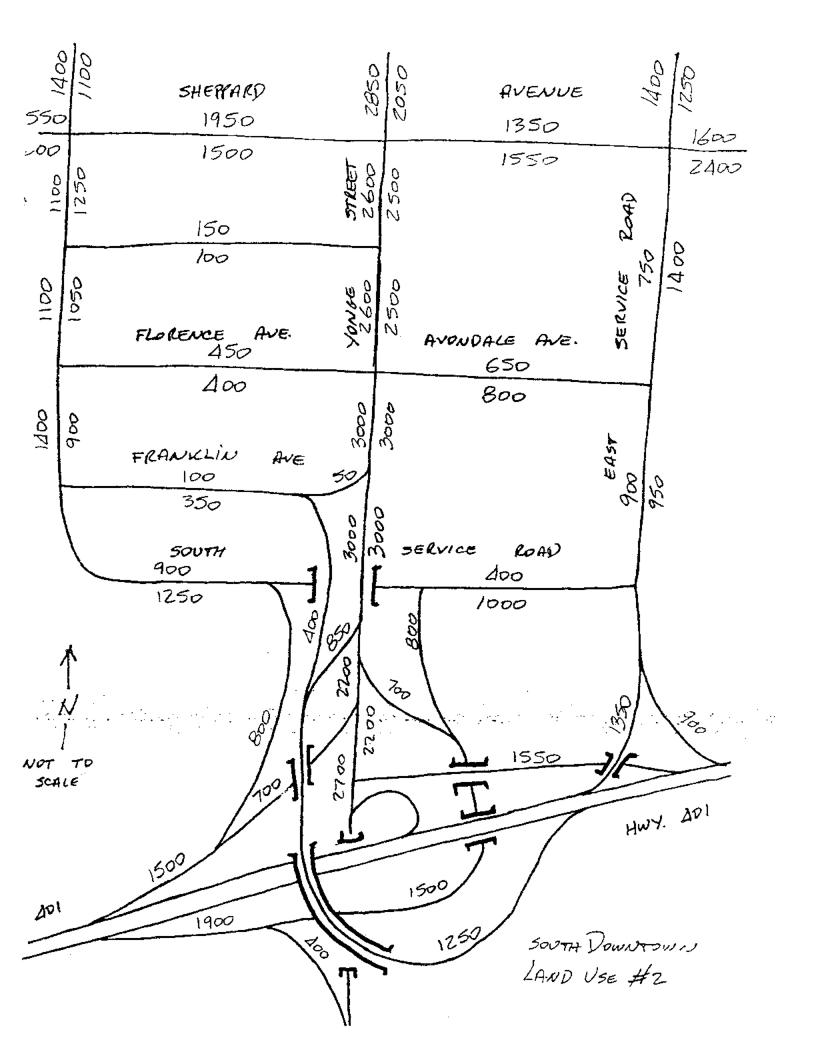
11399	13275	12911	13637
TOTAL TRIPS IN OUT 2277 2452 1623 5040 3900 7492	TOTAL TRIPS IN OUT 2277 2452 1265 3932 1561 1848	TOTAL TRIPS IN OUT 2277 2452 1265 3932 880 2105 4422 8489	TOTAL TRIPS IN OUT 2277 2452 1265 3932 1673 2038 5215 8422
TOTAL 43,842 71,937	TOTAL 43,842 58,349 28,383 130,574	TOTAL 43,842 58,349 25,749 127,940	TOTAL 43,842 58,349 31,123 133,914
POPULATION EES RESIDENTS ,075 25,767 ,992 13,945 067 39,712	POPULATION EES RESIDENTS ,075 25,767 ,595 11,754 ,182 15,201 ,852 52,722	POPULATION ES RESIDENTS .075 25,767 .595 11,754 .924 6,825 .594 44,346	POPULATION EES RESIDENTS .075 25,767 .595 11,754 .252 16,871
EMPLOYI 18 57 57	POP EMPLOYEES 18,075 46,595 13,182 77,852	POPL EMPLOYEES 18,075 46,595 18,924 83,594	POPU EMPLOYEES 18,075 46,595 14,252
TOTAL 2,139,825 2,641,611 4,781,436	707AL 2,139,825 2,185,843 1,337,943 5,663,611	TOTAL 2,139,825 2,185,843 990,869 5,316,537	707AL 2,139,825 2,185,843 1,473,564 5,799,232
GROSS FLOOR AREA ICIAL RESIDENTIAL 12,259 1,597,566 8,647 802,964 0,906 2,400,530	GROSS FLOOR AREA CIAL RESIDENTIAL 2,259 1,597,566 0,840 695,003 5,470 942,473 3,569 3,235,042	GROSS FLOOR AREA ICIAL RESIDENTIAL 12,259 1,597,566 10,840 695,003 17,729 423,140 0,828 2,715,709	GROSS FLOOR AREA ICIAL RESIDENTIAL 12,259 1,597,566 0,840 695,003 77,573 1,045,991 0,672 3,338,560
GROS 4 COMMERCIAL 542,259 1,838,647 2,380,906	GROSS FLOOR A COMMERCIAL RESIDENT 542,259 1,597 1,490,840 695 395,470 942 2,428,569 3,235	GROSS FLOOR A GROSS FLOOR A 542,259 1,597 1,490,840 695 567,729 423 23,600,828 2715	GROS COMMERCIAL 542,259 1,490,840 427,573
CHOSS FLOOR COMMERCIAL RESIDENT COMMER	LANDUSE OPTION 1 UPTOWN DOWNTOWN SOUTH DOWNTOWN TOTAL	LANDUSE OPTION 2 UPTOWN DOWNTOWN SOUTH DOWNTOWN TOTAL	LANDUSE OPTION 3 UPTOWN DOWNTOWN SOUTH DOWNTOWN

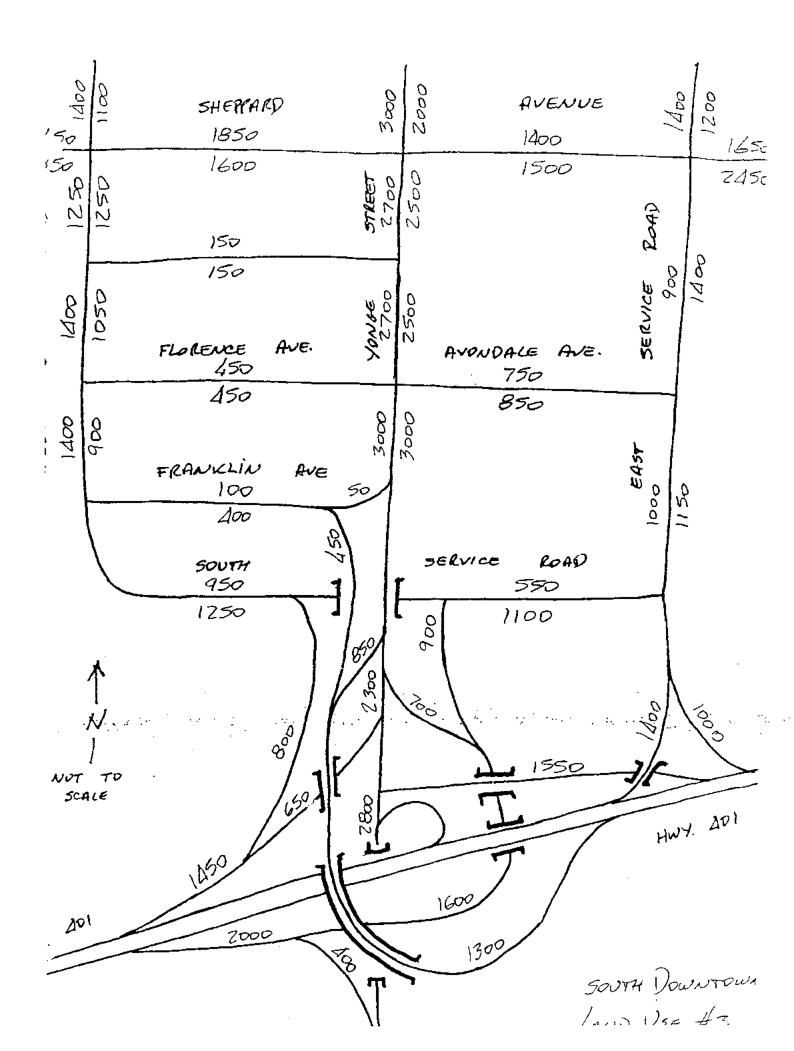
13778 2452 3932 2822 9206 TOTAL TRIPS 2277 1265 1030 4572 43,842 58,349 32,369 134,560 TOTAL L EMPLOYEES RESIDENTS
18,075 25,767
46,595 11,754
8 25,464 6,905 11,754 6,905 44,426 25,767 **POPULATION** 90,134 TOTAL 2,185,843 2,139,825 2,720,669 5,517,686 COMMERCIAL RESIDENTIAL 542,259 1,597,566 1,490,840 695,003 763,918 428,100 GROSS FLOOR AREA 763,918 2,797,017 LANDUSE OPTION 4 SOUTH DOWNTOWN DOWNTOWN TOTAL

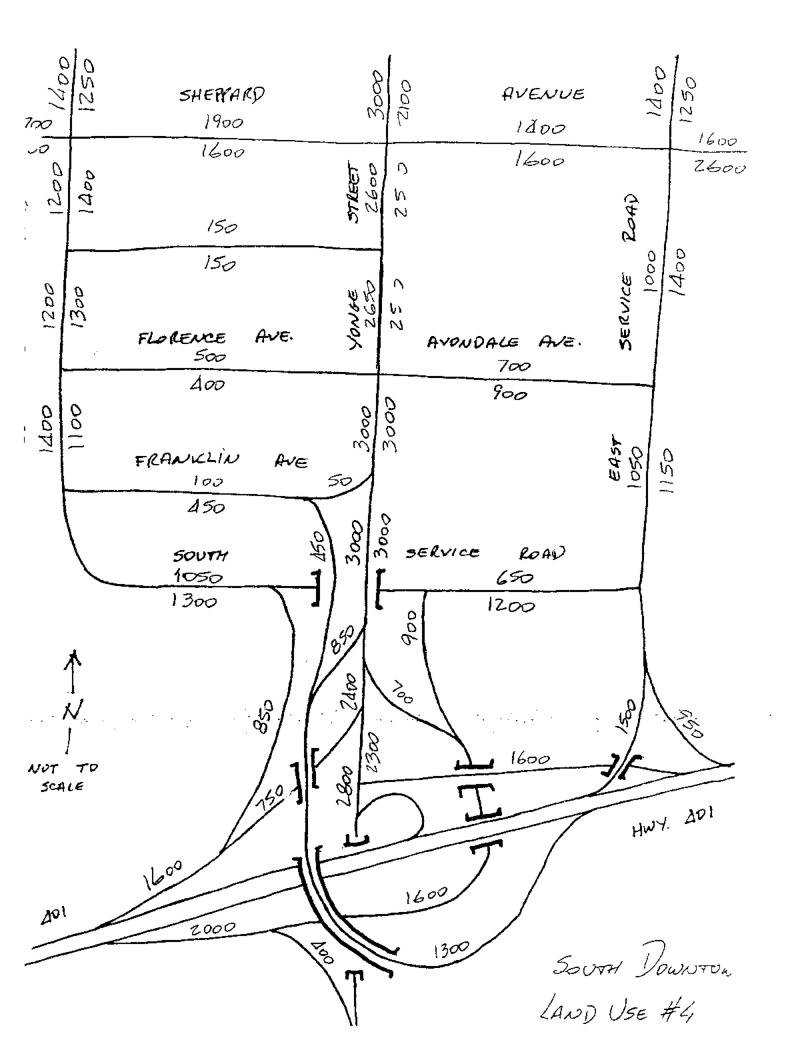
LANDUSE OPTIONS 1 THRU 4 TAKEN FROM PLANNING FILES "TRADE1.WK1" , "TRADE2.WK1"... (PREPARED BY VS) ABOVE OPTIONS WERE RUN IN CONJUNCTION WITH DOWNTOWN/UPTOWN AS SET OUT IN PLANNING FILES "DOWNCALO.WK! (QUADRANTS N/O SHEPPARD ONLY) AND UPTOWN FILE "EXPLORE6.WK1"

1400	SHERFARD 1750	3000	AVENUE 1350	1400
1400 OSE1	1600	37/ee7 2650 2500	1500	25.2
Service 1300	P FLORENCE AVE. 100	0552.2 0082 2082 2082 4	NOALE AVE. 600	SERVICE 950 1250
WEST 1400	FRANKLIN AVE	501	750	950 950
\	300 500TH 950	JOS SERVI	500 900	
) 100		2200 820		32
NOT SCAI	100 1 1500	20027	1600 T	HWY. At
WY. 401		1500	500TI LANT	H Dawntowa Vse #1

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APPENDIX B

SOUTH DOWNTOWN BLOCKS - POSSIBLE VISION DENSITIES

(Revised August 25, 1994)

AUGUST

1994

Alternatives for Remaining Undeveloped Land are based on no S.D.I. Integrated with Existing and committed projects per YCD, Jan. 1993.*

	1988 Pop
1.80	
62.00	30.00
Resident	Office
	Area
į	Floor
- 1	Area
	Area
	Block

1994	Net Change Emps. Res. Block	11 0 Plaza Seneca	--	--------------------------------------	--
1.80	1986 Pop. Emps. Res	5.5 S88 S88 S88 S88 S88 S88 S88 S88 S88 S8			
Worker 30.00 Resident 62.00	5	2,334 0 15 1,464 0 0 107 0 107 55 0 2,00 11 1,027 0 11 1,027 0 11 0 2,00 11 1,027 0 0 11 0 1,027 0 0 11 0 1,027 11 1,027 0 145 0 422 234 0 422 234 0 422 234 0 422 234 1,473 4,019 2,233 2,652 1,459 0 1,025 5,679 10,894 10,223 5,679			
	% Total F,S.1, (res.)	0.00% 70,034 4,50 0.00% 43,929 4,50 0.00% 43,929 4,50 0.00% 6614 1,150 0.00% 6614 1,150 0.00% 30,822 4,22 90,00% 32,715 3.50 100,00% 4,946 1,50 100,00% 4,946 1,50 100,00% 1,998 3,00 100,00% 1,998 3,00 100,00% 26,169 3,00 100,00% 26,169 3,00 100,00% 1,908 4,00 100,00% 1,908 3,00 100,00% 1,50 95,00% 1,50 95,00% 1,50 95,00% 1,50 95,00% 1,50 95,00% 1,50 95,00% 1,50 95,00% 1,50 95,00% 1,50 95,00% 1,50 95,00% 1,50 95,00% 1,50 95,00% 1,50			
S.D.I. 993.*	Floor Area % (non) Resident	100.00%			
and committed projects per YCD, Jan. 1993.	Area Area (Acres) (Sq.m.) Non-Res	304 15563 70,034 241 8762 43,929 249 12,100 25,410 1.09 4,409 0.30 1,227 0.69 2,769 0.40 2,769 0.81 3,297 0.81 3,297 0.81 3,297 0.81 3,297 0.81 3,297 0.81 3,297 0.81 6,606 0.74 3,007 0.81 3,297 0.81 8,597 0.81 8,598 0.81 8,598 0.81 8,598 0.81 8,598 0.81 8,598 0.82 8,572 0.83 8,572 0.84 8,698 0.85 8,572 0.85 8,572 0.85 8,572 0.86 0.72 2,913 0.86 0.72 2,913 0.86 0.72 2,913 0.72,84 8,985			
Integrated with Existing and committed projects per YCD, Jan. 1993.*	Block	EAST SIDE OF YONGE, SOUTH BB.1 Plaza 70.2 Seneca 26.3 North York Square 26.4 Bonnington (Res.) 26.4 Bonnington (Com) 26.5 Proctor & Gambie 26.5 Proctor & Gambie 26.5 Froctor & Gambie 26.5 Seneciner 26.7 N. side Anndale 26.9 S. side Anndale 26.9 S. side Anndale 26.10 N side Glendora B 26.11 Bales, N. end 26.12 Yonge/Glen./Avon. 26.13 Bales, N. end 26.14 Bales/Avon/Glen A 26.15 Westhor 26.15 Westhor 3.16 Salde, end 3.17 S side Avondale B 3.16 Salde., end 3.17 S side Avondale B 3.18 Oaldburn Apls. 3.19 N.Y. Bd. of Ed. 3.19 N.Y. Bd. of Ed. 3.19 N.Y. Bd. of Ed.			

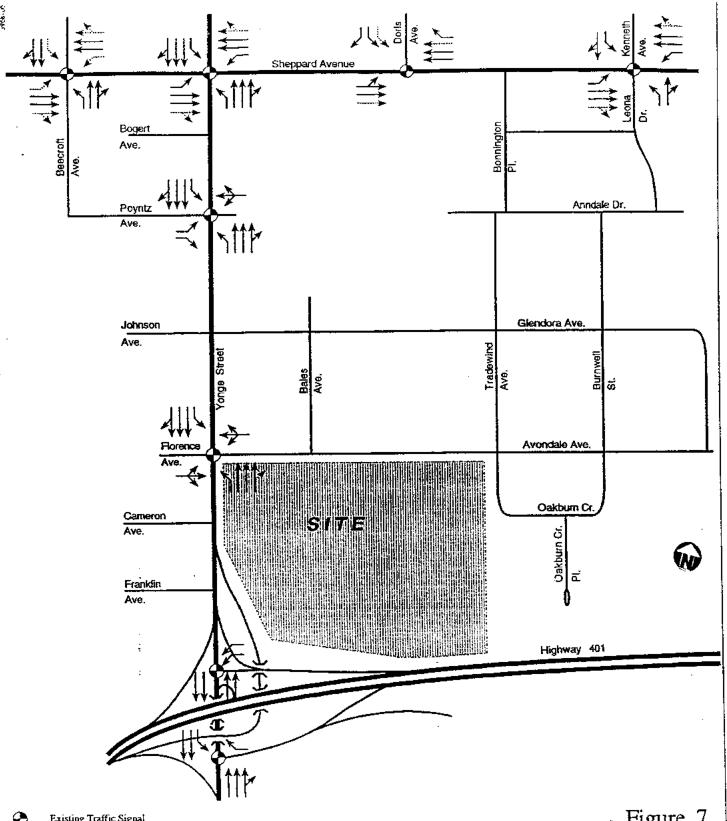
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	0 30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	O O O O O Beecroft N	4 0 1110 0 H&R Really	18 1148 - 1 Marathon	0 0 0 Boger	0 409 0 Church	75 75 75	23 1030 🐣 🚉	D	47 37 205 251 Povntz/John B	0	50 = 22 206 473 Flo./John B		77 27 223 × 554 Cam,/Flo, B	0 24 0 Prank./Cam A	23 10 193 1 408 Frank /Cam. B	0	0 302 % O Warner Brothers	278 220 5,090 1,885 SW-TOTAL
	0 0 0 0	0	1,114	1,166	0 0	409	264 0 0		135	489	135		73		126 70	216418232	0 24 13	À	5,368 2,474 1,374 2
61	0	0		5,53	'		7,916	.,,		37,782	D96'9	38,392	4,542	45,016		n '	0000 1,400 X	300,000	70,1070 014,408 30.43
-	0 0.00%	33.407 100.00%			2.279 100.000					2000	20.00			2 %000	30000	0.00%	:	153	
빞	0.79 3,191	4			_	_	1.79	1.38	9.448	5.573		3,028	11,254			977	0.70 2,800	22.80 92,271 161	
WEST SIDE OF YONGE,	25.2 Beecroft N.	25.3 H & R Really*	25.4 Marathon*	25.5 Bogert	25,6 Church	25.7 Beecroft S.	25.8 Yonge/Poyntz/Bogert	25.10 Poyntz/John. A	25.10 Poyntz/John, B	25.12 Flo./John, A	25.12 Flo./John, B	25.14 Cam./Flo. A	25.14 Cam./Flo. B	25.16 Frank./Cam. A	25.16 Frank/Cam, B	25.17 Frank,/Un.	25.18 Warner Brothers*	SW-TOTAL	

OTAL - EAST AND WEST S	EST SIDES OF YONGE	YONGE			j			I]	
i		1.00		Floor	Area		***				
Block	Area	Area	_	æ		***	Total				
	(Acres)	(Sq.m.)	Von Res	(Non)	Resident		3		In Salta se folding	<u> </u>	Ē
TOTAL	95.04	384.574	487 856	SR ORW	707 400						
			222	20.00	1061-100	01:74%	1,275,047 3.	 징	16,262 12,697 7,0	54	1,9
]	Į

988 Pop. Net Change imps. Res. Emps. 'Hes. 1,920 1,131 14,437 11,217		Block	TOTAL
988 Pop. Imps. Res. 1,920 1,111	Net Change	Emps. Res.	14,437 11,217
<u>- W) </u>	1988 Pop.	Emps. Res.	1,920 1,131

APPENDIX C



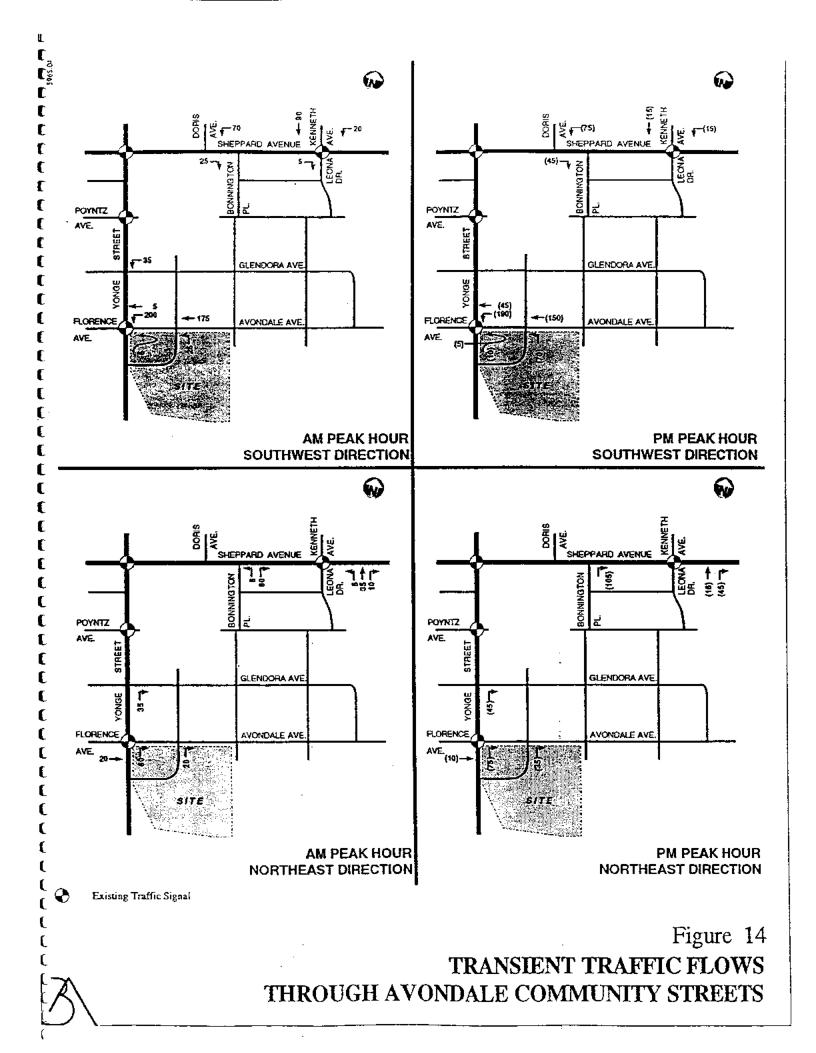
Existing Traffic Signal

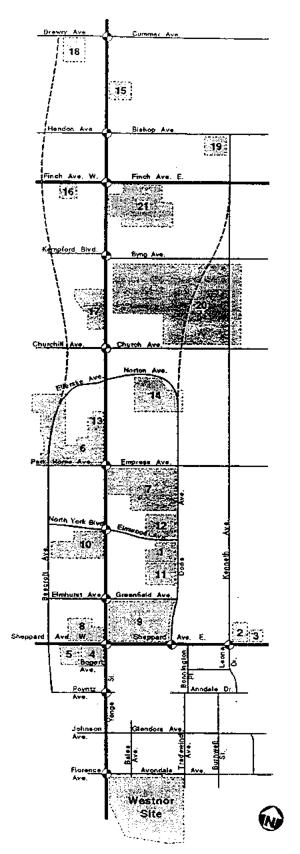
Widening of Sheppard Avenue

Schematic Only - Not to Scale

Figure 7
CURRENT/COMMITTED
LANE CONFIGURATIONS
AND AREA ROAD SYSTEM

3





- 1. Cam-nest (Hollywood II Res.)
- 2. Creditel (110 Sheppard Ave. E.)
- 3. Kenneth/Sheppard
- 4. Marathon (4800 Yonge)
- 5. Southwest Sheppard (25 Sheppard)
- 6. Penta Stolp (Gibson Square)
- 7. Menkes (Empress Plaza)
- 8. Canderel (Yonge/Sheppard)
- 9. Counsel Prop. (Sheppard Ctr. II)
- 10. Ontario Hydro (5000 Yonge)
- 11. Bramalea (Spring Garden 1,2A)
- 12. Bramalea (Eimwood)
- 13. Sam-Sor (5182-5200 Yonge)
- 14. Centara/Inland (Yonge-Norton)
- 15. Zaraska (5791-3 Yonge)
- 16. Mizrahi (Finch/Lorraine)
- 17. Ullscrest (Yonge/Horsham)
- 18. Crestine (Drewry)
- 19. Arendsquare (Pemberton I)
- 20. Eminent (Northtown I)
- 21. Yonge/Finch (N. Amer. Life)

Existing Traffic Signal

Proposed Road

"Chematic: Not to Scale

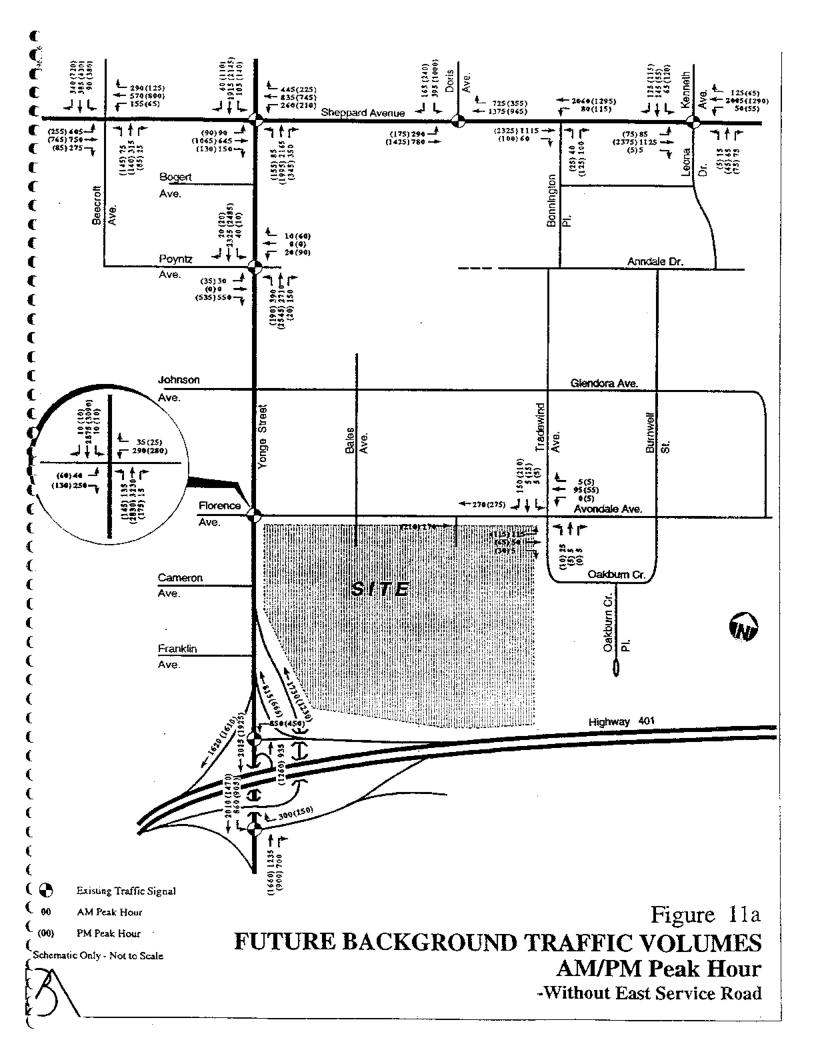
Figure 10

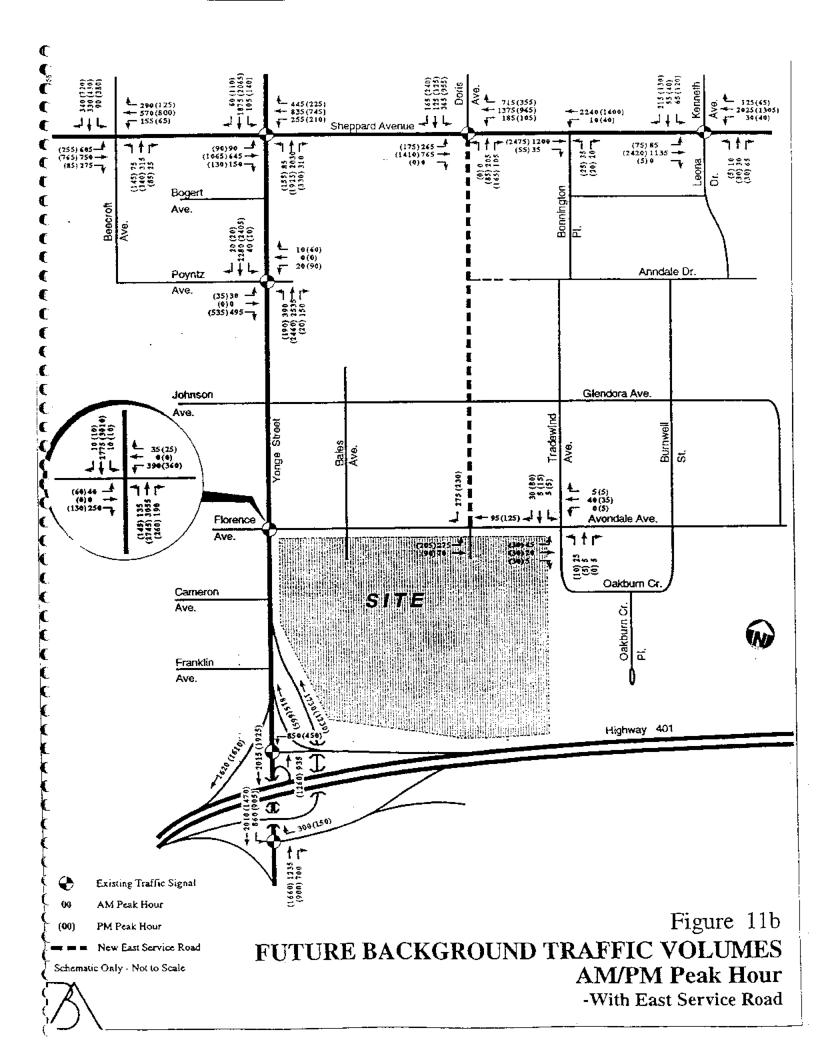
OTHER CITY CENTRE DEVELOPMENTS



TABLE 3 OTHER DEVELOPMENT - Traffic Generation

	TRIP GENER	ENERATION RATES			AM PEAK HOUR	CHOUR	PM PEA	PM PEAK HOUR
		Other	Residentia Commercial (Office: Hace) Assisted Housing	iai treh tulih tel treh fulih el treh foomi ng treh enti	DN 2008	Off 0.16 0.19 0.19 0.13	IN 0.16 0.09 0.15 0.15	0.07 0.08 0.45 0.20 0.20 0.08
PROJECT		LAND ÜSES	ÜSFS		PEAK	PEAK HOUR TRAFFIC	IC GENERATION	NOIL
DOWNTOWN	Residential (units)	Office (m² GFA)	Retail (m² GFA)	Other (htl rms)				
1. Cam-nest (Hollywood II Res) 2. Creditel (110 Sheppard Ave. E.)	150	14317			12	24 13	24 13	12 64
Under Construction:								•
5. Southwest Sheppard (25 Sheppard)		33407	1002		153	31	35	153
Approved:								
3. Kenneth/Sheppard 4. Marahon (48th Yange)	50	34993	3937		173	90 47	3.8	171
Forta Stop (Gibson Square)	303	103449	24108	300	596 596	145	145	\$05 160 119
8. Canderel (Yonge/Sheppard) 9. Counsel Prop. (Sheppard Ct. II)	250	46317	4714 10097		138	282	285	227
 Ontario Hydro (5000 Yonge) Bramalea (Spring Garden 1,2A) 	•	180750	17396 2361		883 252	171 50	177 50	883 252
12. Bramalea (Elmwood) 13. Sam-Sor (5182-5200 Yonge) 14. Centara/Inland (Yonge • Norton)	336	31345 2990	2068	347	248	8.08 8.08 8.08 8.08	4 % E	22 149 118
Subtotal	1359	617786	72883	647	3283	868	930	3315
UMTOWN	Residential	Office	Retail	Other				
Approved:	(minta)	((C. 5)	(geor, 119g)				
15. Zaraska (5791-3 Yonge) 16. Mizrahi (Finch/Lorraine)	, c	30859 4227	1145 669		143	29	29	143
17. Ullscrest (Yonge/Horsham) 18. Crestline (Drewry)	735			135	26	57	550	90,90
19. Arendsquare (Pemberton I) 20. Eminent (Northtown I)	1168				32 93	187	64 187	32
Proposed:	<u> </u>	41						
21. Yonge/Finch (N. Amer. Life)	350	24289	1758	216	131	77	77	131
Subtotal	2153	59375	3572		450	429	422	457
TOTAL CITY CENTRE	3512	677161	76455	863	3733	1326	1352	3772





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APPENDIX

B

SUPPORTING MATERIAL

SECONDARY PLAN REVIEW

ENVIRONMENTAL Assessment Stúdy

> Spans Stoor

PROPERTY AND ECONOMIC DEVELOPMENT DEPARTMENT

MEMORANDUM

To:

Paula Dill

Commissioner of Planning

From:

Jayne Domazet,

Director of Economic Development

Date:

February 17, 1995

SUBJECT:

South Downtown Service Road - Acquisition Cost Estimate Revision

Further to our cost estimate prepared January 1995, the land requirements have been revised to include all of the lands located between Cameron Avenue, Franklin Avenue, Yonge Street and the proposed service road. The cost estimate has been revised accordingly. The cost, as of May 1994, of acquiring the land for South Downtown Service Road, west of Yonge Street is summarized on the following table.

	COST ESTI	MATE	
ALTERNATE ROUTES	ACQUISITION COST	SALE OF SURPLUS	NET COST
	West of Yor	ge St.	
Route #1W	\$23,900,000	\$1,200,000	\$22,700,000
Route #2W	\$24,900,000	\$1,200,000	\$22,700,000

In addition it should be noted that this is an estimate only and is not based on appraised values.

Only the cost of the land is considered. Not included are any entitlements under the Expropriations Act for injurious affection, business loss, disturbance damage, relocation costs, good will, legal costs, survey costs or appraisal costs.

Jayne Domazet,

Director of Economic Development

PROMEMOSSDSR958.MEM

CC:

Joe Farag, Finance Department Colin Couper, Transportation Dept. Paul Hudspith, Cole Sherman

SOUTH DOWNTOWN SECONDARY PLAN REVIEW - ENVIRONMENTAL ASSESSMENT West Service Road

Alternative design #1

Property	Frontage	Depth	Area	Road Area	Residual
	(ft)	(ft)	(ft2)	(ft2)	(ft2)
4578 Yonge Street	67	130	8558	8653	
4630 Yonge Street	195.37	124.43	24310	5705	18605
4664 Yonge Street	79	124	9795	3122	6674
12 Franklin Avenue	31	130	4049	3337	713
14 Franklin Avenue	25	130	3248	2476	772
16 Franklin Avenue	25	130	3248	2583	665
20 Franklin Avenue	50		reneed no permitted	6028	468
22 Franklin Avenue	50	130	6496	4736	1760
24 Franklin Avenue	40	130	5200	2583	2617
30 Franklin Avenue	55	130	7146	646	6500
15 Cameron Avenue	77	130	9974	538	9436
21 Cameron Avenue	136	130	17647	3310	14337
27 Cameron Avenue	25	130	3240	2648	592
29 Cameron Avenue	45	130	5840	5840	0
33 Cameron Avenue	30		3879	3337	542
34 Cameron Avenue	25	130	3240	215	3024
35 Cameron Avenue	37	130	4774	2368	2406
36 Cameron Avenue	25	130	3240	2153	1087
38 Cameron Avenue	30	130	3879	3879	0
39 Cameron Avenue	37	130	4774	431	4343
40 Cameron Avenue	45	130	5840	5840	0
44 Cameron Avenue	49	130	6394	1399	4994
15 Florence Avenue	25	130	3240	377	2863
17 Florence Avenue	50	130	6479	807	5672
21 Florence Avenue	25	130	3240	377	2863
23 Florence Avenue	50	130	6479	807	5672
26 Florence Avenue	50	130.5	6525	1184	5341
27 Florence Avenue	40	130	5200	646	4554
31 Florence Avenue	35	130	4561	592	3969
32 Florence Avenue	70	130	9079	8396	683
33 Florence Avenue	5Q	130	6479	1292	5187
36 Florence Avenue	37	130	4774	4575	199
37 Florence Avenue	37	130	4859	3983	877
39 Florence Avenue	50	130	6479	6479	0
40 Florence Avenue	30	130	3879	1938	1941
44 Florence Avenue	50	130	6479	431	6048
47 Florence Avenue	50	130	6500	861	5639
26 Johnston Avenue	48	130	6181	2691	3490
27 Johnston Avenue	50	130	6479	1292	5187
28 Johnston Avenue	34	130	4433	4433	0
29 Johnston Avenue	52	130	6735	6243	492
32 Johnston Avenue	31	130	4007	3337	670
33 Johnston Avenue	45	130	5840	5059	781
34 Johnston Avenue	37	130	4774	4090	684
37 Johnston Avenue	31	130	4030	969	3061
39 Johnston Avenue	50	130	6500	22	6478
25 Poyntz Avenue	40	110	4399	2045	2354
27 Poyntz Avenue	35	110	3858	3858	o
31 Poyntz Avenue	50		5481	4521	960
(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	TOTAL:		298333	143128	155205

TOTAL: 298333 143128 155205

SOUTH DOWNTOWN SECONDARY PLAN REVIEW - ENVIRONMENTAL ASSESSMENT - West Service Road

Atternative design #2

		Donath) Asse	Bond Area	Residual
Property	Frontage	Depth	Area	Road Area (ft2)	(ft2)
	(ft) 67	(ft) 130	(ft2) 8653	8653	(112)
4578 Yonge Street	195.37	124.43	24310	5597	18713
4630 Yonge Street	195.37 79	124.43	9817	3122	8695
4664 Yonge Street			4049	3142	713
12 Franklin Avenue	31 25	130 130	3240	2476	764
14 Franklin Avenue	25 25	130	3240	2583	656
16 Franklin Avenue	50 50	130	5240 6479	2363 6028	451
20 Franklin Avenue	000000000000000000000000000000000000000	+30 130	6479	4736	1743
22 Franklin Avenue	50		5200	4736 2583	2617
24 Franklin Avenue	40	1 30 130	5260 7161	2363 646	6515
30 Franklin Avenue	55		9974	538	9436
15 Cameron Avenue	77	130			oleonos as as as as as as as as as as as as as
21 Cameroπ Avenue	136	130	17647	3310 2 648	14337 592
27 Cameron Avenue	25	130	3240	***********************	
29 Cameron Avenue	45	130	5840	5840 3337	542
33 Cameron Avenue	30 85	130	3879	***************************************	
34 Cameron Avenue	25	130	3240	215	3024
35 Cameron Avenue	37	130	4774	2368	2406 1087
36 Cameron Avenue	25	130	3240	2153	
38 Cameron Avenue	30	130	3879	3879	0
39 Cameron Avenue	37	130	4774	431	4343 Ū
40 Cameron Avenue	45	130	5840	5840	SCHOOL STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET,
44 Cameron Avenue	49	130	6394	1399	4994
15 Florence Avenue	25	130	3240	377	2863
17 Florence Avenue	50	130	6479	807	56 7 2
21 Florence Avenue	25	130	3240	377	2863
23 Florence Avenue	50	130	6479	807	5672
27 Florence Avenue	40	130	5200	646	4554
31 Florence Avenue	35	130	4561	592	3969
33 Florence Avenue	50	130	6479	***************	5833
36 Florence Avenue	37	130	4774	1830	2944
37 Florence Avenue	37	130	4859	3337	1522
39 Florence Avenue	50	130	6479	6479	0
40 Florence Avenue	30	***************************************			***************************************
44 Florence Avenue	50	130	6479	6479	0
46 Florence Avenue	50	130	6479	1507	4972
47 Florence Avenue	50	130	6479	1938	4542
26 Johnston Avenue	47.5	130	6175	54	6121
28 Johnston Avenue	34	130	4433	1830	2603
32 Johnston Avenue	31	130		3767	239
33 Johnston Avenue	45	130		4951	888
34 Johnston Averuse	37	130		4413	
36 Johnston Avenue	37	130		2260	2514
37 Johnston Avenue	34	130	400000000000000000000000000000000000000	2368	2065
38 Johnston Avenue	25	130		431	2809
39 Johnston Avenue	50			6479	
45 Johnston Avenue	40		4 ·	3229	1971
25 Poyntz Avenue	40				3538
27 Poyntz Avenue	35		<u> </u>	3444	414
31 Poyntz Avenue	50				
35 Poyntz Avenue	50	110		431	5050
	TOTAL:		295025	141318	153706

TOTAL: 295025 141318 153706

SOUTH DOWNTOWN SECONDARY PLAN REVIEW - ENVIRONMENTAL ASSESSMENT East Service Road

Alternative design #1

Property	Frontage (ft)	Depth (ft)	Area (ft2)	Road Area (ft2)	Residual (ft2)
4661 Yonge Street	114	120	13680		9030
4679 Yonge Street	118	120	14173	3272	10901
45/47 Sheppard Avenue East	298	N/A	N/A	10979	N/A
80 Sheppard Avenue East	77.49	N/A	N/A	6997	N/A
9 Bates Avenue	79	119	9403	1722	7681
19 Avondale Avenue	79	118	9300	2368	6932
25 Avandale Avenue	40	118	4728	2563	2144
33 Avondale Avenue	58	120	6934	1292	5642
34 Avondale Avenue	NIA	118	5274	546	4628
35 Avondale Avenue	30	114	3399	700	2699
36 Avendale Avenue	35	118	4148	431	3716
37 Avondale Avenue	35	114	description of the second section of the second	807	3189
38 Avondale Avenue	35	118	4146	431	3716
39 Avondale Avenue	25	114	2839	592	2247
40 Avondale Avenue	45	138	5309	592	4717
41 Avendale Avenue	25	114	2839	700	2139
44 Avondale Avenue	25	118	2945	323	2622
45 Avondale Avenue	50	114	5677	5677	0
46 Avondale Avenue	25	118		323	2622
48 Avondale Aven⊔e	40	118	4728	5381	4189
49 Avondale Avenue	50	114	5677	1399	4278
50 Avondale Avenue	40	118	4728	538	4189
51 Avondale Avenue	50	114	5677	1130	4547
55 Avondale Avenue	50	114	5677	1130	4547
56 Avondale Avenue	25	118	2945	323	2622
58 Avondale Avenue	45	118	5270	523 592	2022 4678
	45 50	114			
59 Avondale Avenue			5677	1130	4547
60 Avondale Avenue	50	118	5890	646	5244
63 Avondale Avenue	50	114	5677	1130	4547
64 Avondale Avenue	45	118	5270	592	4678
66 Avondale Avenue	45	118	5270	646	4624
67 Avondale Avenue	50	114	5677	1130	4547
68 Avondale Avenue	46	118	5386	3875	1511
73 Avondale Avenue	50	114	5677	3552	2125
77 Avondale Avenue	50	114	5677	431	5247
78 Avondale Avenue	50	114	5700	108	5592
69 Glendora Avenue	50	118			2015
70 Glendora Avenue	50	118	5890	2314	3576
73 Glendora Avenue	50	118	5900	54	5846
76 Glendora Avenue	50	118	5900	161	5739
14 Anndaie Drive	43	100	4300	54	42 46
17 Anndale Drive	35	110	3894	2153	1742
21 Anndale Drive	42.5	110	4675	269	4406
2 Bonnington Place	42	113	4740	2207	253 3
4 Bannington Place	42	113	4740	861	3878
6 Bonnington Place	42	113	4740	915	3825
8 Bonnington Place	42	113	4740	969	3771
10 Bonnington Place	42	113	4740	1023	3717
12 Bonnington Place	42	113	4740	1184	3556
14 Bonnington Place	42	113	4740	1238	3502
16 Bonnington Place	42	113	4740	1561	3179
18 Bonnington Place	42	113	4740	1938	2802
20 Bonnington Place	42	113	4740	2476	2264
22 Bonnington Place	42	113	4746	1615	3131
24 Bonnington Place	42	113	4748	1184	3562
26 Bonnington Place	35	112.95	3953	969	2984
	TOTAL:		289629	90992	216612

SOUTH DOWNTOWN SECONDARY PLAN REVIEW - ENVIRONMENTAL ASSESSMENT East Service Road

Alternative design #2

Property	Frontage	Depth	Агеа	Road Area	Residual
Floberty	(ft)	(ft)	(ft2)	(ft2)	(ft2)
4661 Yonge Street	114	120	13680		9030
4679 Yonge Street	40	120	4819	1722	3097
45/47 Sheppard Avenue East	298	22.22.22	N/A	22497	N/A
43 Sheppard Avenue East	249.83	N/A	N/A	15177	N/A
East Side of Bales Avenue	N/A	N/A	N/A	8073	N/A
2 Forest Laneway	N/A	N/A	N/A	2045	N/A
9 Baies Avenue	79	119	9403	1722	7681
19 Avondale Avenue	79	118	9300	2368	6932
25 Avondale Avenue	40	118	4728	2583	2144
33 Avondale Avenue	58	120	6934	1292	5642
34 Avondale Avenue	N/A	118	5274	646	4628
35 Avondale Avenue	30	114	3399	700:	2699
36 Avondale Avenue	35	118	4146	431	3716
37 Avondale Avenue	35	114	3997	807	3189
38 Avondale Avenue	35	118	4146	431	3716
39 Avondale Avenue	25	114	2839	592	2247
40 Avoridale Avenue	45	118	5309	592	4717
41 Avondale Avenue	25	114	2839	700	2139
44 Avondale Avenue	25	118	2945	323	2622
45 Avondale Avenue	50	114	5677	5677	0
**************************************	25	118	2945	323	2622
48 Avondale Avenue 48 Avondale Avenue	40	118	4728	538	4189
49 Avondale Averue	50	114	5677	1399	4278
50 Avondale Avenue	40	118	4728	538	4189
51 Avondale Avenue	50	114	5677		4547
55 Avondale Avenue	50	114	5677	1130	4547
56 Avondale Avenue	25	118	2945	323	2622
58 Avondale Avenue	45	118	5270	700	4570
59 Avondale Avenue	50		5677	1130	4547
60 Avondale Avenue	50	118	5890	5597	293
63 Avondale Avenue	50		5677	3337	2341
64 Avondale Avenue	45	118	5270	5059	211
56 Avondale Avenue	45				
67 Avondale Avenue	50	114	5677	5677	0
73 Avondaie Avenue	-	114	5877	1399	4278
46 Glendora Avenue	40	118	4720	75	4645
50 Glendora Avenue	35		4146	***************************************	1509
53 Glendora Avenue	25	118	2950	11	2939
	50	118	5890		Ð
54 Glendora Avenue 55 Glendora Avenue	50	118	5890	3498	2392
57 Glendora Avenue	30	118			n
58 Glendora Avenue	50	118	5890	• • • • • • • • • • • • • • • • • • • •	3845
61 Glendora Avenue	35			ALC: ALC: ALC: ALC: ALC: ALC: ALC: ALC:	О
63 Glendora Avenue	50		5677	1399	4278
1 Anndale Drive	35	<u> </u>	3894		127
2 Anndale Drive	43	1			339
3 Anndale Drive	42		01.00000000000000000000000000000000000	Company of the contract of the	256
4 Anndale Drive	42.6	100			4163
5 Anndale Drive	42.0	 			4383

SOUTH DOWNTOWN SECONDARY PLAN REVIEW - ENVIRONMENTAL ASSESSMENT East Service Road

Atternative design #3

Property	Frontage	Depth	Area	Road Area	Residual
	(ft)	(ft)	(ft2)	(ft2)	(ft2)
4661 Yonge Street	114	120	13680	4650	9030
4679 Yonge Street	40	120	4819	1722	3097
45/47 Sheppard: Avenue East	298	N/A	N/A	25295	N/A
43 Sheppard Avenue East	249.83	N/A	N/A	12917	N/A
East Side of Bales Avenue	N/A	N/A	N/A	16038	N/A
2 Forest Laneway	N/A	N/A	N/A	2260	N/A
9 Bales Avenue	79	119	9403	1722	7681
19 Avondale Avenue	79	118	9300	2368	6932
25 Avondale Avenue	40	118	4728	2583	2144
33 Avondale Avenue	58	120	6934	1292	5642
34 Avondale Avenue	N/A	118	5274	646	4628
35 Avondale Avenue	30	114	3399	700	2699
36 Avondale Avenue	35	118	4146	431	3716
37 Avondale Avenue	35	114	3997	807	3189
38 Avondale Avenue	35	118	4146	431	3716
39 Avondale Avenue	25	114	2839	592	2247
40 Avondale Avenue	45	118	5309	753	4558
41 Avondale Avenue	25	114	2839	969	1870
44 Avondale Avenue	25	118	2945	2945	0
45 Avondale Avenue	50	114	5677	5677	0
46 Avondale Avenue	25	146	2945	2945	0.
48 Avondale Avenue	40	118	4728	4728	0
49 Avendale Avenue	50	114	5677	5220	457
50 Avondale Avenue	40	118	4728	1292	3436
51 Avondale Avenue	50	114	5677	2476	3202
55 Avondale Avenue	50	114	5677	32 8 3	2394
59 Avondale Avenue	50	114	5677	4662	995
63 Avondale Avenue	50	114	5677	5328	349
67 Avondale Avenue	50	114	5700	2906	2794
73 Avondale Avenue	50	114	5700	377	5323
41 Glendora Avenue	50	118	5900	11	5889
42 Giendora Avenue	50	118	5900	86	5814
43 Glendora Avenue	35	118	4146	3767	379
44 Glendora Avenue	50	118	5890	44 67	1423
45 Glendora Avenue	50	118	(5890)	5890	0
46 Glendora Avenue	40	118	4728	4728	0
50 Gtendora Avenue	35	118	4146	861	3285
51 Glendora Avenue	40	118	4728	2325	2403
1 Anndale Drive	35	110	3894	3606	288
2 Anndale Drive	43	100	4268	3229	1039

TOTAL: 191111 147005 100616

THE CITY OF NORTH YORK SOUTH DOWNTOWN SECONDARY PLAN REVIEW ENVIRONMENTAL ASSESSMENT STUDY

SUMMARY OF CONSTRUCTION COSTS

East Service Road	
 Alternative #1 (Tradewind) 	\$3,920,000
 Alternative #2 (Combination) 	\$4,514,000
Alternative #3 (Midblock)	\$4,121,000
West Service Road	
Alternative #1	\$1,473,000
Alternative #2	\$1,492,000
East-West Link (Lower Service Road)	
Preferred Alignment	\$853,000
Yonge Street Reconstruction	
Preferred Alignment with detour	\$5,788,000
Interchange	
Ramp 401 East to Service Road	\$2,162,000
 Ramp 401 East to Yonge North & South 	\$1,641,000
 Ramp 401 West to Yonge North & Service Road 	\$591,000
 Ramp Service Road to 401 West 	\$1,503,000
 Ramp Yonge South to 401 West 	\$691,000
 Ramp Yonge North to 401 East 	\$9,528,000
 Ramp Yonge North to 401 West 	\$10,215,000
Total Construction Cost	
Based on Average Cost of Alternatives	\$38,640,000
10% Contingency	\$3,860,000

TOTAL COST

\$46,400,000



North York South Downtown Secondary Plan Review **Environmental Assessment Study**

Summary of Construction Costs For Service Road Alternatives

			Aftermative	# Cast	Atternative	#2 Edat	Alternative	#3 East	Alternative #1 (46st	#1 West	Atternative #2 Weet	#Z Week	East. West Link	er une
Description	Š	. Unit	* Tradewind Alignment Service Road Drily*		Combination Alignment Service Road Only	Allginment id Only	Midblock Alignment Service Road Only	lignment ad Only	Service Read Only	ad Only	Service Road Only	ANO PE	-(Lower Service Road	log Road
			Cuantity	Total	Quantition	-Lioue	Quantity	Total	Cuenthy	Total	Chiamity Total	Total	Quentity	Total
Removals Remova Curb and Gutter	E	\$30.00	1900	\$57,000	1550	\$46,500	780	\$23.400	810	\$24,300	082	\$23.700		90
Remove Concrete Sidewalk	E	\$40.00	2850	\$114,000	2330	\$93,200	11/0	\$46,800	1220	\$48,800	1180	\$47,200	0	\$0
Remove Asphalt	Ě	\$20.00	9200	\$184,000	9250	\$185,000	5150	\$103,000	4280	\$85,600	4050	\$81,000	0	30
Roadway Base (Granular 'A')	-	\$12.00	9150	\$109,800	9300	\$111,600	0068	\$106,800		\$79.200	6100	\$73.200	3600	843 200
Sub Base (Granular '8')	_	\$10,00	22800	\$228,000	23200	\$232,000	22200	\$222,000	16380	\$163,800	15200	\$152,000	0006	000.065
Asphall Base	_	\$42.00	3750	\$157,500	3800	\$159,600	3760	\$155,400	2700	\$113,400	2500	\$105,000	1500	\$63,000
Asphall Top	_	\$62.00	1900	008'86\$	1900	\$98,800	1800	\$83,600	1350	\$70,200	1250	\$65,000	750	000 66\$
Sub drain	Ē	\$12.00	2950	\$35,400	2050	\$24,600	1800	\$21,600	1550	\$18,600	1550	\$18,600	7007	\$8,400
Concrete Curb and Gutter	Έ	\$40.00	2950	\$118,000	2050	\$82,000	1700	\$68,000	1550	\$62,000	1550	\$62,000	700	\$28,000
Sewer & Watermain Storm sewer (incl., carobbasins and manholes)	Sav			\$350,000		\$240,000		\$206,000		\$130.000		\$165,000		000 085
Sanitary Sewer	Say			\$225,000		\$155,000		\$140,000		\$110,000		\$110,000		\$55,000
Watermaln	Say					\$145,000		\$128,000		\$100,000		\$105,000		\$50,000
Boulevard Treatment Sodding	, w	\$5.00	11500	\$57,500	8700	\$43,500	7700	\$38,500	5940	\$29,700	6120	\$30,600	2800	\$14,000
Trees and Landscaping	Say			\$24,000		\$27,000		\$23,000		\$18,000		\$20,000		\$9,000
Concrete Sidewalk	_ III j	\$40.00	3825	\$153,000	2900	\$116,000	2550	\$102,000	1980	\$79,200	2040	\$91,600	066	\$39,600
Light Standards	Each	\$6,000.00		\$318,000	39	\$234,000	34	\$204,000	30	\$180,000	32	\$192,000	4	\$84,000
Traffic Lights Traffic Signals	Each	\$80,000 co	Ŋ	\$400,000	4	\$320,000	3	\$240,000	7	\$160,000	2	\$160,000	69	\$240,000
Reconfiguration At Marathon Underground Parking	Say			\$1,100,000		\$1,400,000		\$1,400,000		N/A		N/A		N/A
Transformer Relocation	Say			Q\$		\$800,000		\$600,000		N/A		NA		NA
Total Construction Cost			•	\$3,920,000		\$4,513,800		\$4,121,100		\$1,472,800		\$1,491,900		\$853,200

Notes:

Property acquisition costs not included
 Cost of removing troos and residential homes not included
 Cost of driveway re-construction not included
 Cost of driveway re-construction not included

Cost of utility relocation not included
 Temporary construction lighting not included
 All costs are preliminary only and are to be confirmed.

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North York South Downtown Secondary Plan Review Environmental Assessment Study

Summary of Construction Costs For Yonge Street Reconstruction

Description	Unit	Unit Price	Yonge \$ Reconstr	
			Quantity	Total
Removals			Ī	
Remove Curb and Gutter	m	\$30.00	1,850	\$55,500
Remove Concrete Sidewalk	m²	\$40.00	2,800	\$112,000
Remove Asphalt	m²	\$20.00	10,700	\$214,000
Remove Concrete Base	m²	\$30.00	11,000	\$330,000
Roadway				
Concrete Base	m²	\$50.00	11,200	\$560,000
Asphalt Base	t	\$42.00	2,000	\$84,000
Asphalt Top	t	\$52.00	1,000	\$52,000
Sub drain	m	\$12.00	1,700	\$20,400
Concrete Curb and Gutter	m	\$40.00	1,700	\$68,000
Detour		j		
Base (Granular 'A')	t	\$12.00	3,000	\$36,000
Sub Base (Granular 'B')	t	\$10.00	14,400	\$144,000
Asphalt Base	t	\$42.00	2,450	\$102,900
Asphalt Top	t	\$52.00	1,000	\$52,000
Drainage	Say			\$35,000
Sewer & Watermain				
Storm sewer	cou			\$250,000
(incl., catchbasins and manholes)	Say Say			\$130,000
Sanitary Sewer Watermain	Say			\$125,000
	Jay		<u>.</u>	V125,555
Boulevard Treatment Sodding	m²	\$5.00	2,000	\$10,000
Trees and Landscaping	Say	\$0.00	2,000	\$5,000
Concrete Sidewalk	m ²	\$40.00	750	\$30,000
Light Standards	Each	\$6,000.00	32	\$192,000
Traffic Lights Traffic Signals	Each	\$80,000.00	1	\$80,000
Structures Yonge/Service Road/Ramp Structure	Say			\$3,100,000
Total Construction Cost	<u> </u>	· · · · · · · · · · · · · · · · · · ·		\$5,787,800

- 1. Property acquisition costs not included
- 2. Cost of driveway re-construction not included
- 3. Temporary construction lighting not included
- 4. Cost of utility relocation not included
- 5. All costs are preliminary only and are to be confirmed



North York South Downfown Secondary Plan Review **Environmental Assessment Study**

Summary of Construction Costs For Interchange Ramps and Structures

E. Daniton Structure (Management of the Control of		1 (A) (New 1980)		A STATE OF SALES		Charles Broken	No. of all the latest		A CONTRACTOR	A	1 1 1 1 1 1 1 1 1	11-20 E-2012 AND AND AND AND AND AND AND AND AND AND	#100 FEB 14 19 19 19 19 19 19 19 19 19 19 19 19 19	2012 - 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
Dascribuon	Ē	100	Ramp 401 East	G1 East	Rampa	10.	Ramp 401 Wes	1 Meas	Kamp Se	Ramp Service Road	Ci Camp Conge South	unos es	Ramp Yo	s ,	Ramp Yonge North	
			Service Road	Road	Yonge No	North/South	Yonge/Service Ro	Vice Rd	100	401 Wast	2 - 10 - 401 West	(ee)	401 EBIC		159M 10F	Mesti
			- Quamtity	Total	Agueno	Total	Guanativ	Total	_ Guanaty_	🖅 Total 👙 🖟 Culantive 📑 Itotal 🐄	Cuedany	. Total	Guanny	Total .	Quantity	* Totel
Removals Remove Curb and Guller	E	\$30.00		0\$	1545		340	\$10,200		99	510	\$15,300	670	\$20,100	906	\$27,150
Remove Asphalt	Ē	\$20.00		Q\$	5460		1800	\$32,000		90	2000	\$40,000	3200	\$64,000	4060	\$81,200
Roadway - Ramps Raca (Crander 'A')	-	\$12.00	875	\$10,500	2350		1000	\$12,000	1120	\$13,440	970	\$10,440	1630	\$19,560	1700	\$20,400
Sub Base (Granular 'B')	-	\$10.00	2190	\$21,900	9069	\$59,000	2500	\$25,000	2800	\$28,000	2160	\$21,600	4060	\$40,600		\$42,500
Asphalt Base	-	\$42.00	300	\$12,600	068	\$37,380	350	\$14,700	380	\$15,960	300	\$12,600	920	\$23,100		\$24,360
Asphalt Top	-	\$52.00	240	\$12,480	720	\$37,440	280	\$14,560	300	\$15,600	240	\$12,480	440	\$22,880		\$23,920
- Asphalt OFC	-	\$100.00	150	\$15,000	410	↔	175	\$17,500	195	\$19,500	150	\$15,000	280	\$28,000	295	\$29,500
Sub drain	٤	\$12.00	720	\$8,640	2009		420	\$5,040	520	\$6.240	450	\$5,400	980	\$11,760		\$9,240
Concrete Curb and Gutter	É	\$40,00	720	\$28,800	200	\$20,000	420	\$16,600	520	\$20,800	2009	\$20,000	1120	\$44,800	770	\$30,800
Highway 401 Highway Widening	Say			000'005\$		0\$		0\$		0\$		0\$		000'009\$		\$500,000
Retaining Walls Noise Barrier	Say			\$1,000,000		\$700,000 \$0		\$0		\$150,000		÷ 65		\$400,000		\$ Q
Drainage Storm sewer (incl., catchbasins and manholes)	Say			\$160,000		\$110,000		\$100.000		\$110,000		\$100,000		\$130,000		\$150,000
Stope Treatment	Ē	\$7.00	200	\$3.500	2700	\$18,900	1900	\$13,300	250	\$1,750	0069	\$13,300	1500	\$10,500	2000	\$14.000
Seeding and Mukhing	\$	\$20.00	 20	\$400	1001	:	99	\$1,200	10	\$200	8	\$1,200	160	\$3,200		\$1,200
Trees and Landscaping	Say			\$1,500		\$7.000		\$5,000		009\$		\$6,000		\$10,000		\$6,000
Illumination High Mast Poles	Each	\$50,000.00	-	000'0\$\$	-	\$50.000	-	\$50,000		0\$	-	\$50,000	2	\$100,000	-	\$50,000
Structures Bridges	Say			\$0		\$320,000		\$250,000		\$1,100,000		\$350,000		\$7,000,000		\$8,500,000
Relaining Walks	Say	:::		\$25,000		₽\$		O\$		0\$		D\$		\$700,000		\$675,000
Concrete Barrier	E	06\$	125	\$11,250	535	\$46,150	265	\$23,850	235	\$21,150	195	\$17,550	920	\$49,500	325	\$29,250
Total Construction Cost				\$2,161,570		\$1,640,620		\$591,150		\$1,503,140		\$690,870		\$9,528,000		\$10,214,520

Total Interchange Construction Cost \$26,329,870

1 Property acquisition costs not included Notes:

2 Cost of Utility resocation not included 3. Temporary construction lighting not included

Temporary construction barriers and signage not included
 All costs are pretininary only and are to be confirmed



APPENDIX B

TRAFFIC REPORT

NORTH YORK DOWNTOWN AREA SOUTH OF SHEPPARD AVENUE

TRAFFIC ANALYSIS DOCUMENTATION

The following documents the information and the results of the traffic analysis undertaken in support of the Environmental Assessment for the transportation infrastructure required to support OPA 393.

For this project, CSA conducted capacity analysis at signalized intersections within the study area using turning movement volumes provided by the City of North York Transportation Department. Land use and other traffic generation assumptions were also provided by the City of North York.

LAND USE

Westnor Site - Phase 1

	sq.m.	units
residential	94,758	900
commercial	48,773	
Oakburn Site - Phase 1		
	sq.m.	units

residential -- 532 retail 600 --

other relevant land use assumptions: 1.8 residents/unit 30 sq.m./employee

TRIP GENERATION (As Per OPA 343)

Base assumptions:

peak hour factor	45%
car occupancy	1.2 persons/vehicle
absenteeism rate (emp.)	10%
walk/other	10%
transit modal split	60%

PM peak hour trip rates:

employment: 0.34 autos/100 sq. m outbound

off-peak direction (inbound) is 20% of peak

residential: 0.16 autos/res. unit inbound

off-peak direction (outbound) is 50% of peak

AM peak hour trip rates: the reverse of PM peak hour.

ARTERIAL ROAD TRAFFIC OPERATIONS

The 1995 Highway Capacity Manual was used to conduct capacity analyses at signalized intersections under existing and future traffic conditions. Intersection capacity analysis worksheets are included at the back of this document. Intersection configuration adjustments and other design refinements (e.g. storage length for turn lanes) were undertaken as necessary to ensure that the road system would operate without undue delays or queue spillovers.

Existing Turning Movements

All existing turning movements, except the westbound Highway 401 to northbound Yonge Street ramp, were obtained from Metro counts. The west-north off ramp volume was obtained from the existing volumes used by the BA Group in their traffic impact study of the Westnor Development Project. The existing turning volumes are provided in Figure 1.

Under existing conditions capacity analysis was conducted for the AM and PM peak hours at all signalized intersections along Yonge Street between Sheppard Avenue and Avondale Avenue, as well as the intersections of Sheppard Avenue with Beecroft Road and Doris Avenue. The existing volumes and existing traffic signal timing were used in the analysis, however some signal timing adjustments were required to keep the v/c ratio below 1.2. Since the traffic signals on Yonge Street are under SCOOT Control it is acceptable to adjust the signal timing for the existing conditions. At all intersections, except Yonge Street and Avondale Avenue, adjustments were made to the phase times but the cycle length remained the same. A saturation flow of 1800 vph and a peak hour factor of 0.95 were used in the analyses. For the Avondale Avenue and Yonge Street intersection a saturation flow of 1900 vph and a peak hour factor of 0.98 were assumed due to the saturated conditions experienced at that intersection. The performance characteristics and critical movements of these intersections are summarized in Table 1.

Future Turning Movements

Future turning movement volumes for the proposed development and transportation infrastructure improvements proposed under OPA 393 were provided by the City of North York

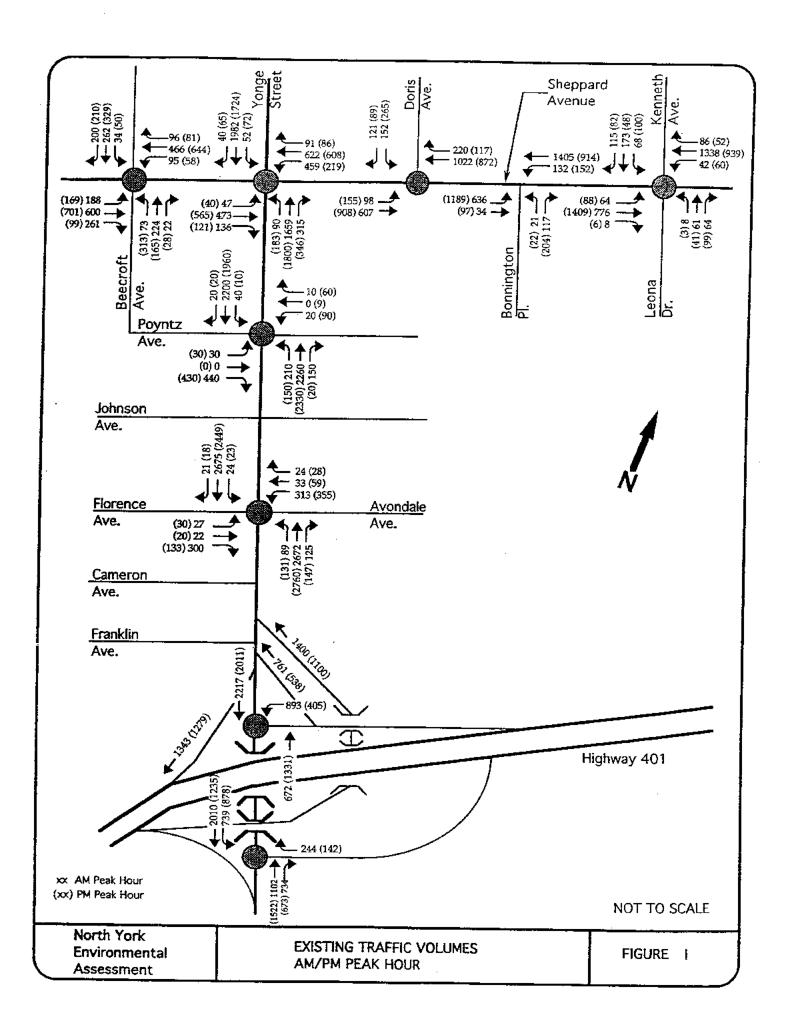


Table 1

Intersection Analysis - Existing Conditions

Intersection	Period	Ir	tersectio	n	Cri	tical Mov	ement	
		v/c	delay	LOS	Movement	v/c	delay	LOS
Beecroft/Sheppard	AM Peak	0.711	13.3	В				
Beecroft/Sheppard	PM Peak	1.013	36	D	EBLTR	1.05	55.9	E
					WBTR	0.92	28.4	D
					NBL	0.98	50.2	£
Yonge/Sheppard	AM Peak	0.961	27.9	D	WB L	1.02	61.5	F
					NB L	1.19	202.4	F
					NBTR	0.9	23.2	С
	j				SBTR	0.9	23.2	С
Yonge/Sheppard	PM Peak	0.829	31.4	D	NBTR	0.97	25.7	D
					SB L	0.94	78	F
					SB TR	1.04	46.5	E
Doris/Sheppard	AM Peak	0.555	9.6	В			,	
Doris/Sheppard	PM Peak	0.756	10	В		İ		
Yonge/Poyntz	AM Peak	0.876	23.3	С	SB TR	0.96	27.6	D
					NBTR	0.87	16.1	С
Yonge/Poyntz	PM Peak	0.859	16.9	С				
Yonge/Avondale	AM Peak	1.1	85.9	F	WB LTR	1.12	113.3	F
-				į	NBTR	1.08	64.3	F
					SB TR	1.17	115	F
Yonge/Avondale	PM Peak	1.165	98.4	F	WBLTR	1.15	118.9	F
-					NBTR	1.18	111.6	F
					SB TR	1.14	89.7	F

critical if LOS = E or F or if $v/c \ge 0.85$ for through, $v/c \ge 1.00$ for left or right

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Transportation Department. These are shown in Figures 2 and 3 for the AM and PM peak hours respectively.

Capacity analyses were conducted for the future AM and PM peak hours at all existing and proposed signalized intersections in the study area. A saturation flow of 1900 vph and peak hour factors of 0.95-0.98 were used in the analyses. The performance characteristics and critical movements of the existing and proposed signalized intersections in the study area are summarized in Table 2.

The storage length requirements were calculated for all exclusive left and right turn lanes. The vehicle arrival rates were calculated for each movement at the intersections. The arrival rates for the left turn movements are based on a probability that 95% of the time vehicles will clear the intersection in one cycle. Using the Vehicle Arrival Rate Table provided in the Ministry of Transportation Geometric Design Standards the number of vehicles that will be stopped per cycle was determined. This number was multiplied by 7.5 metres, the average length of a vehicle, to determine the required storage. This adjustment for 95% probability of clearance results in an increase in storage length requirement of about 80% - 120% over the non-adjusted storage length requirement (depending on the arrival rate, this increase may range from about 45% to over 200%).

The queue length analysis and storage length requirements for all exclusive left and right turn lanes are shown in the attached capacity analysis outputs. These storage lengths are also reflected in the preliminary design drawings prepared for the proposed road improvements.

CONCLUSIONS

- Arterial roads and certain intersections in the study area (e.g. Yonge/Sheppard, Yonge/Avondale) are presently near or at capacity.
- The proposed east service road and the widening of Avondale Avenue would provide the
 necessary capacity, provide for balanced traffic flows, and provide enhanced and flexible
 circulation of traffic as generated by the development outlined in OPA 393.

-	2480	Sheppard Avenu		FIGURE 2	2	Avondale	Avenue not to scale
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818 Beecroft Road 3551	1390 JUL (= 355	1910 ₁₃₁₀ = 0	267 268	Poyntz Avenue		325	225 MID-BLOCK ALIGNMENT

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Avondale	Avenue	0
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225	325	MID-BLOCK ALIGNMENT
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Table 2
Intersection Analysis - Future Conditions

Intersection	Period	Intersection		Critical Movement				
		v/c	delay	LOS	Movement	v/c	delay	LOS
Beecroft/Sheppard	AM Peak	0.82	25	С	WBT	0.87	32	D
Beecroft/Sheppard	PM Peak	0.94	39	D	EBL	1.07	76	F
					WBT	0.97	42	E
					SBT	1.04	55	E
Yonge/Sheppard	AM Peak	0.91	30	D	WBL.	1.08	79	F
	!				WBT	0.97	32	D
					NBT	0.92	34	D
					SBT	0.97	30	Ď
Yonge/Sheppard	PM Peak	0.94	32	D	EBT	0.97	37	D
	,				WBL	1.00	67	F
					NBL	1.01	59	E
<u> </u>					NBT	0.94	36	D
					SBT	1.01	38	D
Doris/Sheppard	AM Peak	1.01	39	D	WBTR	1.06	50	Ε
					NBTR	1.03	58	E
					SBL	1.04	75	F
Doris/Sheppard	PM Peak	1.02	44	Ε	EBT	0.97	45	E
	•				WBL	1.05	69	F
					WBTR	1.01	41	Ė
	•				NBTR	0.98	49	E
ļ					SBL	1.00	84	F
Yonge/Poyntz	AM Peak	1.06	26	D	NBL	1.18	125	F
					SBT	1.01	29	D
Yonge/Poyntz_	PM Peak	0.96	22	C	SBTR	1.04	38_	D
Yonge/Avondale	AM Peak	0.94	40	D	NBL	1.04	62	F
					NBT	1.07	53	Ε
					SBT	1.01	35	D
	PM Peak	0.99	37	D	WBL	1.06	76	Ή.
			i		NBT	0.92	20	C
					SBT	1.07	54	Ė
Avondale / ESR	AM Peak	0.42	10	В				
Avondale / ESR	PM Peak	0.5	10	В				

critical if LOS = E or F or if v/c >= 0.85 for through, v/c >= 1.00 for left or right

INTERSECTION CAPACITY ANALYSIS WORKSHEETS

Lanes, Volumes, and Timings Summary

	7	\rightarrow	J	Ţ		L	4	1	2	وا	1	له
	<u>EBL</u>	<u>EBT</u>	<u>EBR</u>	WBL	<u>WBT</u>	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Volume (vph.)	355	1310	245	220	900	355	175	645	65	170	330	315
Adj. Lane Grp. Vol.	362	1745	Q	224	1408	0	179	761	0	173	692	0
Lanes	1	3	0	1	3	0	1	2	0	1	2	0
Satd. Flow (Prot.)	1770	5471		1770	5370		1770	3677		1770	3465	
Satd. Flow (Perm.)	233	5471		276	5370		324	3677		324	3465	
Left Turn Type		P/P			P/P			P/P			P/P	
Phase Number	7	4		3	8		5	2		1	6	
Phase Lagging?		Yes			Yes			Yes			Yes	
Current Split (s.)	22	41		13	32		8	28		8	28	
Yellow Time (s.)	4.0	6.0		4.0	6.0		4.0	6.0		4.0	6.0	
V/C Ratio	0.76	0.80		0.75	0.87		0.82	0.81		0.79	0.78	
Platoon Factor	1.00	1.00		1.71	1.22		1.00	1.00		1.00	1.00	
Average Delay (s.)	19	20		29	32		27	28		24	27	
Level of Service	С	С		D	D		D	D		С	Ď	

Cycle Length: 90

Offset: 0 (0%), Referenced to phase 2-NBT, Begin Of Green

Intersection V/C Ratio: 82% Intersection Delay: 25.4 Intersection LOS: C

Splits and Phases: Sheppard Ave. W. & Beecroft Rd.

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Lane Group	<u>EBL</u>	<u>EBT</u>	<u>WBL</u>	<u>WBT</u>	<u>NBL</u>	<u>NBT</u>	SBL	<u>SBT</u>
Lane Group Volume	362	1745	224	1408	179	761	173	692
Queue Length 50%ile	(m.)63.2	97.2	40.3	57.7	21.4	67.7	20.6	61.1
Queue Length 95%ile	(m.)83.2	135.3	51,4	113.2	45.7	97.4	44.8	89.5
Link Length (m.)	109.5	109.5	197.5	197.5	174.5	174.5	75.9	75.9
% of Link Used	76%	124%	26%	57%	26%	56%	59%	118%
Blocks Upstream?		Yes						Yes
Storage Length (m.)								
% of storage Used	79%	129%	69%	151%	51%	108%	43%	85%
Fills Storage?	105.0	Yes	75 .0	Yes	90.0	Yes	105.0	

Lanes, Volumes,	and	Timings	Summary
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	<u>EBL</u>	EBT	EBR	<u>WBL</u>	<u>WBT</u>	<u>WBR</u>	NBL	<u>NBT</u>	NBR	SBL	SBT	<u>SBR</u>
Volume (vph.)	310	940	150	140	1195	220	305	300	165	355	580	435
Adj. Lane Grp. Vol.	316	1223	Ó	143	1588	0	311	498	0	362	1087	0
Lanes	1	3	0	1	3	0	1	2	0	1	2	0
Satd. Flow (Prot.)	1770	5482		1770	5471		1770	3535		1770	3498	
Satd. Flow (Perm.)	276	5482		276	5471		276	3535		389	3498	
Left Turn Type		P/P			P/P			P/P			P/P	
Phase Number	7	4		3	8		5	2		1	6	
Phase Lagging?		Yes			Yes			Yes			Yes	
Current Split (s.)	12	32		12	32		14	32		14	32	
Yellow Time (s.)	4.0	6.0		4.0	6.0		4.0	6.0		4.0	6.0	
V/C Ratio	1.07	0.74		0.49	0.97		0.93	0.47		0.97	1.04	
Platoon Factor	1.00	1.00		2.07	1.31		1.00	1.00		1.00	1.00	
Average Delay (s.)	76	23		19	42		37	20		39	55	
Level of Service	F	С		С	Ε		D	С		D	Ë	

Offset: 0 (0%), Referenced to phase 2-NBT, Begin Of Green

Intersection V/C Ratio: 94% Intersection Delay: 39.3 Intersection LOS: D

Splits and Phases: Sheppard Ave. W. & Beecroft Rd.

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Queue Lengths, and Potential Blocking Problems

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Lane Group	<u>EBL</u>	<u>EBT</u>	<u>WBL</u>	<u>WBT</u>	NBL	<u>NBT</u>	SBL	<u>SBT</u>
Lane Group Volume	316	1223	143	1588	311	498	362	1087
Queue Length 50%ile (r	n.)60.0	69.7	25.2	86.2	58.1	38.5	68.1	103.2
Queue Length 95%ile (r	n.)76.5	96.6	32.0	126.9	81.1	56.2	87.9	132.0
Link Length (m.)	77.1	77,1	193.4	193.4	163.2	163.2	70.5	70.5
% of Link Used	99%	125%	17%	66%	50%	34%	125%	187%
Blocks Upstream?		Yes					Yes	Yes
Storage Length (m.)								
% of storage Used								

Filis Storage?

Lanes.	Volumes.	and	Timinas	Summary
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	<u>EBL</u>	EBT	EBR	WBL	WBT	WBR	NBL	<u>NBT</u>	<u>NBR</u>	<u>SBL</u>	SBT	SBR
Volume (vph.)	115	1095	320	335	1285	275	155	1780	385	100	1880	80
Adj. Lane Grp. Vol.	117	1229	327	342	1442	281	158	1998	393	102	2110	82
Lanes	1	3	1	1	3	1	1	3	1	1	3	1
Satd. Flow (Prot.)	1770	5588	1583	1770	5588	1583	1770	5588	1583	1770	5588	1583
Satd. Flow (Perm.)	311	5588	1583	311	5588	1583	212	5588	1583	212	5588	1583
Left Turn Type		P/P			P/P			P/P			P/P	
Phase Number	7	4		3	8		5	2		1	6	
Phase Lagging?		Yes			Yes			Yes			Yes	
Current Split (s.)	13	29		13	29		8	40		8	40	
Yellow Time (s.)	5.0	6.0		5.0	6.0		5.0	6.0		5.0	6.0	
V/C Ratio	0.37	0.82	0.62	1.08	0.97	0.53	0.74	0.92	0.49	0.48	0.97	0.10
Platoon Factor	1.00	1.00	1.00	1.08	0.82	0.53	2.27	1.44	1.32	1.00	1.00	1.00
Average Delay (s.)	10	26	20	79	32	10	26	34	13	8	30	8
Level of Service	В	D	С	F	D	В	D	D	В	В	Ð	В

Offset: 0 (0%), Referenced to phase 2-NBT, Begin Of Green

Intersection V/C Ratio: 91% Intersection Delay: 30.1 Intersection LOS: D

Splits and Phases: Sheppard Ave. E. & Yonge St.

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Lane Group	<u>EBL</u>	<u>EBT</u>	EBR	WBL	<u>WBT</u>	WBR	<u>NBL</u>	NBT	<u>NBR</u>	SBL	<u>SBT</u>	SBR
Lane Group Volume	117	1229	327	342	1442	281	158	1998	393	102	2110	82
Queue Length 50%ile (m.)11.8	73.1	50.4	45.1	88.2	26.1	28.9	101.1	36.4	8.8	131.1	7.6
Queue Length 95%ile (m.)15.3	98.3	68.3	55.8	112.9	36.8	23.7	153.6	44.4	11.0	164.0	9.5
Link Length (m.)	23.3	23.3	. 23.3	211.8	211.8	211.8	376.2	376.2	376.2	71.8	71.8	71.8
% of Link Used	66%	422%	293%	26%	53%	17%	6%	41%	12%	15%	228%	13%
Blocks Upstream?		Yes	Yes								Yes	
Storage Length (m.)												
% of storage Used	31%	197%	98%	62%	125%	74%	30%	192%	56%	22%	328%	38%
Fills Storage?	50.0	Yes	70.0	90.0	Yes	50.0	80.0	Yes	80.0	50.0	Yes	25.0

Lanes, Volumes, and	<u>i imings</u>	Summ	ary			_						
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	<u>EBL</u>	EBT	EBR	WBL	<u>WBT</u>	<u>WBR</u>	<u>NBL</u>	<u>NBT</u>	<u>NBR</u>	<u>SBL</u>	SBT	<u>SBR</u>
Volume (vph.)	65	1290	165	270	1120	195	270	1770	450	130	1895	125
Adj. Lane Grp. Vol.	66	1448	168	276	1257	199	276	1987	459	133	2127	128
Lanes	1	3	1	1	3	1	1	3	1	1	3	1
Satd. Flow (Prot.)	1770	5588	1583	1770	5588	1583	1770	5588	1583	1770	5588	1583
Satd. Flow (Perm.)	311	5588	1583	311	5588	1583	220	5588	1583	220	5588	1583
Left Turn Type		P/P			P/P			P/P			P/P	
Phase Number	7	4		3	8		5	2		1	6	
Phase Lagging?		Yes			Yes			Yes			Yes	
Current Split (s.)	11	29		11	29		11	39		11	39	
Yellow Time (s.)	5.0	6.0		5.0	6.0		5.0	6.0		5.0	6.0	
V/C Ratio	0.24	0.97	0.29	1.00	0.84	0.34	1.01	0.94	0.61	0.49	1.01	0.17
Platoon Factor	1.00	1.00	1.00	2.09	0.44	0.41	1.34	1.41	1.33	1.00	1.00	1.00
Average Delay (s.)	10	37	14	67	14	6	59	36	17	8	38	9
Level of Service	В	D	В	F	В	В	É	D	C	В	D	В

Offset: 0 ($\tilde{0}$ %), Referenced to phase 2-NBT, Begin Of Green

Intersection V/C Ratio: 94% Intersection Delay: 32.0 Intersection LOS: D

Splits and Phases: Sheppard Ave. E. & Yonge St.

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Lane Group	EBL	<u>EBT</u>	EBR	WBL	<u>WBT</u>	<u>WBR</u>	<u>NBL</u>	<u>NBT</u>	NBR	<u>SBL</u>	<u>SBT</u>	<u>SBR</u>
Lane Group Volume	66	1448	168	276	1257	199	276	1987	459	133	2127	128
Queue Length 50%ile (m.) 6.7	90.6	21.8	52.1	64.5	18.2	35.0	112.1	51.4	11.2	134.7	13.2
Queue Length 95%ile (116.0	28.5	49.4	100.2	25.5	63.3	151.8	62.8	14.0	164.7	16.5
Link Length (m.)	23.3	23.3	23.3	211.8	211.8	211.8	376.2	376.2	376.2	71.8	71.8	71.8
% of Link Used	37%	498%	122%	23%	47%	12%	17%	40%	17%	19%	229%	23%
Blocks Upstream?		Yes	Yes								Yes	
Storage Length (m.)												
% of storage Used	17%	232%	41%	55%	111%	51%	79%	190%	79%	28%	329%	66%
Fills Storage?	50.0	Yes	70.0	90.0	Yes	50.0	80.0	Yes	80.0	50.0	Yes	25.0

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	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	<u>SBT</u>	SBR
Volume (vph.)	195	1400	85	140	1715	625	40	460	310	245	525	230
Adj. Lane Grp. Vol.	19 9	1666	0	143	2627	0	41	825	0	250	808	0
Lanes	1	3	0	1	3	0	1	2	Ō	1	2	0
Satd. Flow (Prot.)	1770	5532		1770	5320		1770	3442		1770	3509	
Satd. Flow (Perm.)	177	5532		177	5320		354	3442		311	3509	
Left Turn Type		P/P			P/P			Perm			P/P	
Phase Number	7	4		3	8			2		1	6	
Phase Lagging?		Yes			Yes			Yes				
Current Split (s.)	11	45		11	45			24		10	34	
Yellow Time (s.)	5.0	6.0		5.0	6.0			6.0		2.0	6.0	
V/C Ratio	0.75	0.65		0.54	1.06		0.50	1.03		1.04	0.67	
Platoon Factor	1.61	1.52		1.00	1.00		1.00	1.00		1.00	1.00	
Average Delay (s.)	23	22		7	50		26	58		75	20	
Level of Service	С	С		В	E		D	Ε		F	С	

Offset: 0 (0%), Referenced to phase 2-NBT, Begin Of Green

Intersection V/C Ratio: 101% Intersection Delay: 39.1 Intersection LOS: D

Splits and Phases: Sheppard Ave. E. & East Service Rd.

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Lane Group	<u>EBL</u>	<u>EBT</u>	<u>WBL</u>	<u>WBT</u>	<u>N</u> BL	NBT	SBL	SBT
Lane Group Volume	199	1666	143	2627	41	825	250	808
Queue Length 50%ile	` '	78.5	10.8	166.3	6.7	78.3	47.5	65.3
Queue Length 95%ile	(m.)38.7	102.8	30.9	200.8	9.6	106.8	63.0	96.0
Link Length (m.)	211.8	211.8	284.9	284.9	372.8	372.8	80.1	80.1
% of Link Used	18%	49%	11%	70%	3%	29%	79%	120%
Blocks Upstream?								Yes
Storage Length (m.)								
% of storage Used	52%	137%	36%	236%	38%	427%	47%	71%
Filis Storage?	75.0	Yes	85.0	Yes	25.0	Yes	135.0	

	_	\rightarrow	7	F		Ł	€ĭ	1	7	4	↓	4
	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Volume (vph.)	220	1600	95	275	1245	460	40	295	385	495	530	280
Adj. Lane Grp. Vol.	224	1903	0	281	1913	0	41	728	0	505	868	0
Lanes	1	3	0	1	3	0	1	2	٥	1	2	0
Satd. Flow (Prot.)	1770	5532		1770	5314		1770	3327		1770	3483	
Satd. Flow (Perm.)	233	5532		233	5314		373	3327		324	3483	
Left Turn Type		P/P			P/P			Perm			P/P	
Phase Number	7	4		3	8			2		1	6	
Phase Lagging?		Yes			Yes			Yes				
Current Split (s.)	11	35		11	35			23		21	44	2
Yellow Time (s.)	5.0	6.0		5.0	6.0			6.0		2.0	6.0	
V/C Ratio	0.84	0.97		1.05	1.01		0.49	0.98		1.11	0.55	
Platoon Factor	1.78	1.63		1.00	1.00		1.00	1.00		1.00	1.00	
Average Delay (s.)	32	45		69	41		27	49		84	14	
Level of Service	D	Ε		F	E		D	E		F	В	

Offset: 0 (0%), Referenced to phase 2-NBT, Begin Of Green

Intersection V/C Ratio: 102% Intersection Delay: 43.7 Intersection LOS: E

Splits and Phases: Sheppard Ave. E. & East Service Rd.

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21	23	11	35	5	
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Lane Group	EBL	EBT	<u>WBL</u>	WBT	<u>NBL</u>	<u>NBT</u>	<u>SBL</u>	<u>SBT</u>
Lane Group Volume	224	1903	281	1913	41	728	505	868
Queue Length 50%ile	(m.)32.4	120.5	30.3	121.1	6.8	68.8	95.9	59.7
Queue Length 95%ile	(m.)49.6	148.9	65.7	149.2	9.9	95.7	123.3	84.9
Link Length (m.)	211.8	211.8	284.9	284.9	372.8	372.8	80.1	80.1
% of Link Used	23%	70%	23%	52%	3%	26%	154%	106%
Blocks Upstream?							Yes	Yes
Storage Length (m.)								
% of storage Used	66%	199%	77%	176%	40%	383%	91%	63%
Fills Storage?	75.0	Yes	85.0	Yes	25.0	Yes	135.0	

Lanes, Volumes, and Timings Summary

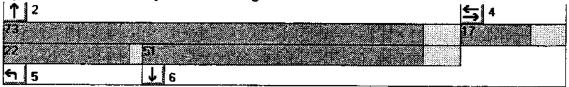
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	<u>EBL</u>	<u>EBT</u>	EBR	<u>WBL</u>	<u>WBT</u>	WBR	<u>NBL</u>	NBT	NBR	SBL	SBT	SBR
Volume (vph.)	50	0	450	20	0	10	550	2010	150	40	2400	50
Adj. Lane Grp. Vot.	51	0	459	20	0	10	561	2424	0	47	2872	0
Lanes	1	0	1	1	0	1	1	3	0	1	3	0
Satd. Flow (Prot.)	1770		1583	1770		1583	1770	5538		1751	5571	
Satd. Flow (Perm.)	1773		1583	1773		1583	145	5538		694	5571	
Left Turn Type		Perm			Perm			P/P			Perm	
Phase Number		4			4		5	2			6	
Phase Lagging?											Yes	
Current Split (s.)		17			17		22	73			51	
Yellow Time (s.)		6.0			6.0		2.0	6.0			6.0	
V/C Ratio	0.22		0.82	0.08		0.05	1.18	0.58		0.13	1.01	
Platoon Factor	1.00		1.00	1.00		1.00	1.69	0.05		0.53	0.83	
Average Delay (s.)	27		26	26		26	125	0		5	29	
Level of Service	D		D	D		D	F	Α		Α	D	

Cycle Length: 90

Offset: 0 (0%), Referenced to phase 2-NBT, Begin Of Green

Intersection V/C Ratio: 102% Intersection Delay: 26.1 Intersection LOS: D

Splits and Phases: Poyntz Ave. & Yonge St.



	1	3	F	L	5	1	وا	II.
Lane Group	<u>EBL</u>	<u>EBR</u>	WBL	<u>WBR</u>	<u>NBL</u>	NBT	SBL	<u>SBT</u>
Lane Group Volume	51	459	20	10	561	2424	47	2872
Queue Length 50%ile ((m.) 8.6	79.0	3.3	1.6	106.6	3.7	3.7	181.8
Queue Length 95%ile ((m.)12.8	127.4	9.8	4.8	127.8	174.9	4.6	219.5
Link Length (m.)	185.6	185.6	25.6	25.6	201.7	201.7	174.5	174.5
% of Link Used	7%	69%	38%	19%	63%	87%	3%	126%
Blocks Upstream?								Yes
Storage Length (m.)								
% of storage Used					85%	117%	31%	1463%
Fills Storage?					150.0	Yes	15.0	Yes

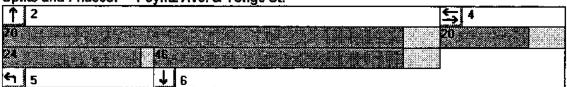
Lanes.	Volumes.	and	Timinas	Summary
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	1	\rightarrow	7	F	—	L	5	1	7	دا	↓	۴
	<u>EBL</u>	<u>EBT</u>	<u>EBR</u>	<u>WBL</u>	<u>WBT</u>	<u>WBR</u>	NBL	<u>NBT</u>	<u>NBR</u>	<u>SBL</u>	<u>SBT</u>	<u>SBR</u>
Volume (vph.)	50	0	550	90	0	60	450	2305	20	10	2300	50
Adj. Lane Grp. Vol.	51	0	561	92	0	61	459	2609	0	10	2638	0
Lanes	1	0	1	1	0	1	1	3	0	1	3	0
Satd. Flow (Prot.)	1770		1583	1770		1583	1770	5583		1770	5571	
Satd. Flow (Perm.)	1773		1583	1773		1583	162	5583		227	5571	
Left Turn Type		Perm			Perm			P/P			Perm	
Phase Number		4			4		5	2			6	
Phase Lagging?											Yes	
Current Split (s.)		20			20		24	70			46	
Yellow Time (s.)		6.0			6.0		2.0	6.0			6.0	
V/C Ratio	0.17		0.86	0.31		0.23	0.89	0.65		0.10	1.04	
Platoon Factor	1.00		1.00	1.00		1.00	1.55	0.12		0.38	0.72	
Average Delay (s.)	24		26	25		25	39	1		4	38	
Level of Service	Ç		D	С		С	D	Α		Α	D	

Offset: 0 (0%), Referenced to phase 2-NBT, Begin Of Green

Intersection V/C Ratio: 96% Intersection Delay: 21.6 Intersection LOS: C

Splits and Phases: Poyntz Ave. & Yonge St.



	1	3	4	2	4	1	دا	↓
Lane Group	<u>EBL</u>	<u>EBR</u>	<u>WBL</u>	WBR	NBL	NBT	SBL	SBT
Lane Group Volume	51	5 6 1	92	61	459	2609	10	2638
Queue Length 50%ile	(m.) 8.3	97.1	15.3	10.0	77.9	11.2	8.0	167.0
Queue Length 95%ile	(m.)12.0	151.6	29.7	19.0	104.2	13.8	0.9	202.5
Link Length (m.)	192.2	192.2	30.4	30.4	202.0	202.0	174.2	174.2
% of Link Used	6%	79%	98%	63%	52%	7%	1%	116%
Blocks Upstream?								Yes
Storage Length (m.)								
% of storage Used					69%	9%	6%	1350%
Fills Storage?					150.0		15.0	Yes

Lanes	Volumes	and Timings	Summary
Lants,	voiunies.	and minings	Summary

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	<u>EBL</u>	<u>EBT</u>	<u>EBR</u>	<u>WBL</u>	<u>WBT</u>	<u>WBR</u>	<u>NBL</u>	NBT	NBR	<u>SBL</u>	SBT	SBR
Volume (vph.)	35	0	190	535	0	100	290	2605	575	155	2410	35
Adj. Lane Grp. Vol.	36	0	194	562	0	102	296	2924	587	158	2744	0
Lanes	1	0	1	2	0	1	1	3	1	1	3	0
Satd. Flow (Prot.)	1770		1583	3533		1583	1770	5588	1583	1770	557 1	
Satd. Flow (Perm.)	1770		1494	3533		1494	170	5588	1494	170	5571	
Left Turn Type		Split			Split			P/P			P/P	
Phase Number	4	4		8	8		5	2		1	6	
Phase Lagging?	Yes	Yes						Yes			Yes	
Current Split (s.)	12	12		19	19		12	47		12	47	
Yellow Time (s.)	6.0	6.0		6.0	6.0		5.0	6.0		5.0	6.0	
V/C Ratio	0.20		0.60	0.89		0.23	1.04	1.07	0.58	0.55	1.01	
Platoon Factor	1.00		1.00	1.00		1.00	1.00	1.00	1.00	2.63	1.13	
Average Delay (s.)	28		16	38		17	62	53	4	14	35	
Level of Service	D		С	D.		C	F	E	Α	В	Ð	

Offset: 0 (0%), Referenced to phase 2-NBT, Begin Of Green

Intersection V/C Ratio: 94% Intersection Delay: 39.8 Intersection LOS: D

Splits and Phases: Avondale Ave. & Yonge St.

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Lane Group	<u>EBL</u>	<u>EBR</u>	<u>WBL</u>	<u>WBR</u>	<u>NBL</u>	<u>NBT</u>	<u>NBR</u>	<u>SBL</u>	SBT
Lane Group Volume	36	194	562	102	296	2924	587	158	2744
Queue Length 50%ile	(m.) 6.2	23.5	52.1	14.3	31,2	185.1	30.6	24.9	173.7
Queue Length 95%ile	(m.)10.7	62.1	75.3	20.8	36.7	217.6	40.4	30.2	209.0
Link Length (m.)	59.3	59.3	216.1	216.1	240.0	240.0	240.0	376.2	376.2
% of Link Used	18%	105%	35%	10%	15%	91%	17%	8%	56%
Blocks Upstream?		Yes							
Storage Length (m.)									
% of storage Used	27%		84%		41%	242%	40%	55%	380%
Fills Storage?	40.0		90.0		90.0	Yes	100.0	55.0	Yes

Lanes, Volume	s, and Timings	Summary
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	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Volume (vph.)	105	0	220	595	0	125	190	2345	505	100	2685	35
Adi. Lane Grp. Vol.	107	0	224	-625	0	128	194	2632	515	102	3053	0
Lanes	1	0	1	2	0	1	1	3	1	1	3	0
Satd. Flow (Prot.)	1770		1583	3533		1583	1770	5588	1583	1770	5577	
Satd. Flow (Perm.)	1770		1494	3533		1494	162	5588	1494	162	5577	
Left Turn Type		Split			Split			P/P			P/P	
Phase Number	4	4		8	8		5	2		1	6	
Phase Lagging?				Yes	Yes			Yes			Yes	
Current Split (s.)	11	11		18	18		11	49		11	49	
Yellow Time (s.)	6.0	6.0		6.0	6.0		5.0	6.0		5.0	6.0	
V/C Ratio	0.68		0.77	1.06		0.31	0.73	0.92	0.50	0.38	1.07	
Platoon Factor	1.00		1.00	1.00		1.00	1.00	1.00	1.00	2.70	1.05	
Average Delay (s.)	38		33	76		14	17	20	5	11	54	
Level of Service	Ď		D	F		В	С	С	Α	В	Ε	

Offset: 0 (0%), Referenced to phase 2-NBT, Begin Of Green

Intersection V/C Ratio: 99% Intersection Delay: 37.3 Intersection LOS: D

Splits and Phases: Avondale Ave. & Yonge St.

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Lane Group	EBL	EBR	WBL	WBR	<u>NBL</u>	NBT	<u>NBR</u>	<u>SBL</u>	<u>SBT</u>
Lane Group Volume	107	224	625	128	194	2632	515	102	3053
Queue Length 50%ile	(m.)19.6	40.4	59.3	15.3	35.1	153.9	43.0	17.3	193.3
Queue Length 95%ile	(m.)31.9	67.0	82.2	22.0	42.6	197.9	56.6	20.8	231.0
Link Length (m.)	59.3	59.3	216.1	216.1	240.0	240.0	240.0	376.2	376.2
% of Link Used	54%	113%	38%	10%	18%	82%	24%	6%	61%
Blocks Upstream?		Yes							
Storage Length (m.)									
% of storage Used	80%		91%		47%	220%	57%	38%	420%
Fills Storage?	40.0		90.0		90.0	Yes	100.0	55.0	Yes

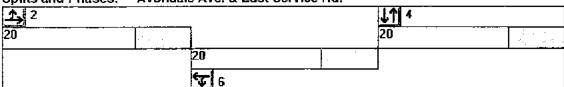
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Lanes.	volumes.	апо	ıımıngş	Summary

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	EBL	<u>EBT</u>	<u>EBR</u>	WBL	<u>WBT</u>	WBR	NBL	<u>NBT</u>	NBR	SBL	SBT	<u>SBR</u>
Volume (vph.)	560	90	50	0	105	75	115	30	0	30	70	460
Adj. Lane Grp. Vol.	0	784	0	0	107	77	117	32	0	31	71	469
Lanes	1	2	0	1	1	1	1	2	0	1	1	1
Satd. Flow (Prot.)	1770	3559		1770	1863	1583	1770	3725		1770	1863	1583
Satd. Flow (Perm.)	1770	3559		1770	1863	1583	1416	3725		1615	1863	1583
Left Turn Type		Split			Split			Perm			Perm	
Phase Number	2	2		6	6			4			4	
Phase Lagging?				Yes	Yes							
Current Split (s.)	20	20		20	20			20			20	
Yellow Time (s.)	6.0	6.0		6.0	6.0			6.0			6.0	
V/C Ratio		0.52			0.20	0.17	0.29	0.03		0.07	0.13	0.52
Platoon Factor		0.85			0.85	0.85	0.85	0.85		0.85	0.85	0.85
Average Delay (s.)		13			11	10	11	10		10	10	5
Level of Service		В			В	В	В	В		₿	В	Α

Offset: 0 (0%), Referenced to phase 2-EBTL, Begin Of Green

Intersection V/C Ratio: 42% Intersection Delay: 10.0 Intersection LOS: B

Splits and Phases: Avondale Ave. & East Service Rd.



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Lane Group	EBT	<u>WBT</u>	WBR	NBL	<u>NBT</u>	<u>SBL</u>	<u>SBT</u>	SBR
Lane Group Volume	784	107	77	117	32	31	71	469
Queue Length 50%ile	(m.)30.3	10.3	7.3	11.5	1.4	2.8	6.6	32.2
Queue Length 95%ile	(m.)48.9	21.2	14.9	26.1	3.0	4.4	10.4	72.3
Link Length (m.)	216.1	142.4	142.4	144.2	144.2	372.8	372.8	372.8
% of Link Used	23%	15%	10%	18%	2%	1%	3%	19%
Blocks Upstream?								
Storage Length (m.)								
% of storage Used	70%	85%	99%	65%	8%	18%	42%	
Fills Storage?			15.0	40.0		25.0		

Lanes, Volumes, and	l Timings	Summ	ary									
	7		J	Ţ		1	4	1	€	L ₂	1	وخ
	<u>EBL</u>	EBT	<u>EBR</u>	WBL	<u>WBT</u>	WBR	<u>NBL</u>	NBT	<u>NBR</u>	SBL	SBT	SBR
Volume (vph.)	420	90	95	0	125	60	140	45	0	75	35	555
Adj. Lane Grp. Vol.	0	674	0	0	128	61	143	48	0	77	36	566
Lanes	1	2	0	1	1	1	1	2	0	1	1	1
Satd. Flow (Prot.)	1770	3531		1770	1863	1583	1770	3725		1770	1863	1583
Satd. Flow (Perm.)	1770	3531		1770	1863	1583	1572	3725		1544	1863	1583
Left Turn Type		Split			Split			Perm			Perm	
Phase Number	4	4		8	8			2			2	
Phase Lagging?	Yes	Yes										
Current Split (s.)	20	20		20	20			20			20	
Yellow Time (s.)	6.0	6.0		6.0	6.0			6.0			6.0	
V/C Ratio		0.45			0.24	0.14	0.32	0.05		0.18	0.07	0.63

0.85

11

В

0.85

10

В

0.85

11

В

0.85

10

В

0.85

10

В

0.85

10

В

0.85

6

В

Cycle Length: 60

Level of Service

Platoon Factor

Average Delay (s.)

Offset: 0 (0%), Referenced to phase 2-NB-SB, Begin Of Green

0.85

12

В

Intersection V/C Ratio: 50% Intersection Delay: 9.7 Intersection LOS: B

Queue Lengths, and Potential Blocking Problems								
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Lane Group	<u>EBT</u>	WBT	<u>WBR</u>	<u>NBL</u>	<u>NBT</u>	SBL	SBT	SBR
Lane Group Volume	674	128	61	143	48	77	36	566
Queue Length 50%ile	(m.)25.1	12.4	5.7	14.2	2.2	7.3	3.3	42.7
Queue Length 95%ile	(m.)43.1	25.8	11.5	30.3	4.3	11.2	5.0	99.0
Link Length (m.)	216.1	142.4	142.4	144.2	144.2	372.8	372.8	372.8
% of Link Used	20%	18%	8%	21%	3%	3%	1%	27%
Blocks Upstream? Storage Length (m.)								
% of storage Used	62%	172%	77%	76%	11%	45%	20%	
Fills Storage?		Yes	15.0	40.0		25.0		

	 	_	 _



APPENDIX C

NOISE IMPACT ASSESSMENT FOR THE PROPOSED EAST SERVICE ROAD

S.S. WILSON AND ASSOCIATES DIV. OF M.H.G. ENGINEERING INC. Consulting Engineers

REPORT NO. W95-01

NOISE IMPACT ASSESSMENT FOR THE PROPOSED EAST SERVICE ROAD DOWNTOWN AREA SOUTH OF SHEPPARD AVENUE NORTH YORK, ONTARIO

PREPARED FOR:

COLE, SHERMAN & ASSOCIATES LTD.
75 COMMERCE VALLEY DRIVE EAST
THORNHILL, ONTARIO
L3T 7N9

PREPARED BY:

HAZEM GIDAMY, P.Eng. PRINCIPAL

AUGUST 30, 1996

NOISE IMPACT ASSESSMENT FOR THE PROPOSED EAST SERVICE ROAD DOWNTOWN AREA SOUTH OF SHEPPARD AVENUE NORTH YORK, ONTARIO

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1	
1.0 BACKGROUND	1
2.0 SOUND LEVEL CRITERIA	2
3.0 ANALYSIS AND RESULTS	8
4.0 CONCLUSIONS AND RECOMMENDATIONS	15
TABLES	
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APPENDIX A: MOEE/MTO PROTOCOL FOR PROVINCIA	L HIGHWAYS NOISE
APPENDIX B: TRAFFIC NOISE PREDICTION MODEL	
APPENDIX C: RECEPTOR LOCATIONS	

1.0 BACKGROUND

- The services of S.S. Wilson and Associates were retained by Cole, Sherman & Associates Ltd. to prepare an environmental noise impact study related to traffic associated with the proposed road known as the East Service Road in the Downtown Area south of Sheppard Avenue in the City of North York.
- 1.2 This report analyzes the existing ambient sound levels and the future impact on the ambient sound levels due to vehicular traffic movements on the East Service Road.

Figures 1 and 2 illustrate the 2 proposed alignment alternatives of the proposed East Service Road.

- 1.3 The purposes of this study are:
 - a. To determine the potential changes to the ambient environment due to future vehicular traffic on the proposed East Service Road.
 - b. To assess the significance of the above changes and to recommend measures to mitigate noise impact; where warranted.
 - c. To advise on the noise compatibility of possible land use changes, the applicable criteria and requirements for noise control in the vicinity of the proposed road.
- 1.4 In future, the East Service Road is expected to have four lanes with an Average Annual Daily Traffic (AADT) of 10,000 vpd with a posted speed limit of 50 km/hr.
- 1.5 This study represents a joint effort with the Consulting Engineering firm Cole, Sherman & Associates Ltd., who provided the necessary road and traffic data and overall project direction.

2.0 SOUND LEVEL CRITERIA

2.1 MOEE/MTO PROTOCOL FOR RESIDENTIAL LAND USE

The MOEE/MTO Protocol is a joint effort of both the Ministry of the Environment & Energy (MOEE) and Ministry of Transportation (MTO) as outlined in the document titled "A Protocol for Dealing with Noise Concerns During the Preparation, Review and Evaluation of Provincial Highways Environmental Assessments", February 1986; a copy of which is included in Appendix A. It primarily applies to Provincial highway undertakings such as Freeways and King's Highways.

The MOEE has informally extended the use of the MOEE/MTO Protocol criteria to also cover other roadways such as Regional and local Municipal roads subject to the provisions of the Environmental Assessment Act (EAA) administered by the MOEE. Since there is no formal direction published by the MOEE on the Protocol application, it is recommended that the same direction with regards to mitigation that applies to the MTO projects be applied also for this municipal project. It should be noted that the MTO may also be involved in granting noise control subsidies related to municipal roads. In other words, the criteria should apply to mitigation within the road r-o-w and also to consider noise impact assessment primarily in Outdoor Living (amenity) Areas alone. the Protocol does not specify if the Leq sound levels are based on 24 hr time base or else, the MOEE extended the appropriate technical logic to municipal roads by requesting calculations be done on the basis of daytime Leq (16 hrs.).

The other point worth noting is that despite the presence of a Provincial objective for outdoor levels of Leq 55 dBA, the decision for mitigation depends primarily on the significance of relative noise increases attributable to the future road expansion above the ambient situation when dealing with urban roads.

With regards to the specific sound level criteria, the following statements are quoted from the Protocol:

"1. The objective for outdoor sound levels is the higher of the Leq 55 dBA or the existing ambient. The significance of a noise impact will be quantified by using this objective in addition to the change in noise level above the ambient.

- Mitigation will attempt to achieve levels as close to, or lower than, the objective level as is technically, economically, and administratively feasible.
- 3. The following Table summarizes the degree of mitigation effort to be applied for various noise level increases."

SUMMARY OF MITIGATION EFFORT

CHANGE IN NOISE LEVEL ABOVE AMBIENT	MITIGATION EFFORT
0 - 5 dBA	- None
> 5 dBA	- Investigate noise control measures on R.O.W.
	- If project cost is not significantly affected introduce noise control measure within R.O.W.
	- Noise control measures, where introduced, should achieve a minimum of 5 dBA attenuation, over first row receivers.
	- Mitigate to ambient, as administratively, economically and technically feasible.

2.2 <u>SOUND LEVEL CRITERIA FOR NOISE IMPACT ON OFFICES AND COMMERCIAL LAND USE</u>

a. In order to maintain acceptable indoor sound levels in private offices and commercial land use, the outdoor sound levels should not exceed Leq 55 and 60 dBA respectively during the daytime assuming standard building construction with open windows. These maximum level outdoors are based on the MOEE's indoor acceptable Leq sound levels of 45 and 50 dBA in private offices and commercial land uses respectively which are included in the MOEE Publication LU-131, Table 131-1. If the windows are sealed or closed during the summer time as a result of the use of central air conditioning system, then the maximum allowable outdoor levels to meet the MOEE indoor objectives would be Leq 70 dBA and 75 dBA for private and general offices respectively.

b. Since it is difficult to decide on what constitutes a private office or a general office for the purposes of this noise study, we are recommending the use of the private office criterion, which is more conservative, for impact assessment purposes.

Therefore, for the purposes of this study we are recommending the use of a maximum sound level Leq 70 dBA outside the building facades as the level below which there will be no concern for traffic noise interfering with the indoor activities of office and commercial land use occupants.

2.3 MTO DIRECTIVE A-1

Although aimed at Provincial Highways, the MTO also applies Directive A-1 to arterial and municipal roads.

The following are some of the applicable highlights of the MTO Directive supplemented also by our discussions with the MTO:

- The MOEE/MTO Protocol is the applicable technical guide and all assessment work to be performed for the outdoor situations
- No subsidy for off r-o-w mitigation.
- 3. The MTO favours the institution of retrofit programs for residential land use where the present or future sound levels exceed Leq 70 dBA irrespective of how small the excess of future level is above the present ambient, or the future-do-nothing ambient.

2.4 MTO DIRECTIVE B-11

To be eligible for MTO subsidy, several conditions must be met as detailed in Directive B-11. However, the most serious concern is the fact that municipalities that ignored the MOEE guidelines for noise control in new land use plans after 1980 are NOT eligible for the subsidy.

2.5 SOUND LEVEL CRITERIA FOR RE-DEVELOPMENT PURPOSES

As a result of the potential changes to the land use in the subject area and the possibility of developing new residential land use on some of the vacant and/or existing properties, the following paragraphs provide an outline of the criteria recommended by the MOEE.

i) Surface Transportation Criteria

The surface transportation noise is to be based on the objective sound levels recommended by the Ontario Ministry of the Environment and Energy (Ref.: Publication LU-131) and Metropolitan Toronto for different land uses and spaces.

The following is summary of the applicable sound level criteria for surface transportation sources:

Outdoor Living Areas (OLA)

Area & Time Period	L _{eq} (16) (dBA) Road and Rail
Individual or Common Outdoor Living Areas (16 hr, 07:00 - 23:00)	55

Indoor Areas

Type of Space	L _{eq} (Time Period) (dBA) Road
Living/dining areas of residences, hospitals, schools, nursing/ retirement homes, day-care centres, etc. (Time period: 16 hr, 07:00 - 23:00)	45
Sleeping quarters of residences, hospitals, nursing/retirement homes, etc. (Time period: 8 hr, 23:00 - 07:00)	40
General offices, reception areas, retail stores, etc. (Time period: 16 hr, 07:00 - 23:00)	50
Living/dining areas of residences, hospitals, schools, nursing/ retirement homes, day-care centres, theatres, places of worship, libraries, individual or semi-private offices, conference rooms, reading rooms, etc.	45
Sleeping quarters of hotels/motels (Time period: 8 hr, 23:00 - 07:00)	45

The criteria for acceptable outdoor and indoor sound levels are to be based on "free-field" predicted and/or measured sound levels at the applicable receiver locations, thus the effects of sound reflections and reverberant sound fields are not considered.

If the sound level is less than or equal to the sound level criteria, no control measures will be required.

The outdoor sound levels may exceed the outdoor sound level criterion by up to 5 decibels, provided that it can be demonstrated that it is not technically feasible to achieve the criterion and that the occupants are informed of a potential disturbance due to the excess noise by means of a warning clause or cautionary note to be registered on title and included in all Development Agreement(s) and Offers of Sale and Purchase or Lease.

Central air conditioning is required when the night-time sound level at the outside wall of the sleeping quarters or bedrooms is equal to or exceeds Leq_{16hrs}. 65 dBA.

If the night-time sound level at the outside wall exceeds Leq_{8hrs.} 50 dBA but is less than 60 dBA, or if the daytime sound level at the outside wall exceeds 55 dBA but is less than Leq_{16hrs} 65 dBA, then forced air heating with provision for future installation of central air conditioning is required.

ii) Criteria For Stationary Noise Sources

The following criteria apply to the impact of Stationary Sources of noise as defined by the MOEE to include commercial facilities. The criteria equally apply to, firstly the impact of Stationary Sources external to the development on the proposed development or, secondly to the impact of any proposed Stationary Sources internal to the development on the development itself or on to other existing noise-sensitive land uses external to the development.

The criteria to be used are based on the guidelines prepared by the Ontario Ministry of the Environment and Energy for the assessment of planned "Stationary Sources" of sound, Publications NPC-133, NPC-205 and NPC-232 included in the Model Municipal Noise Control by-law, 1978.

The predicted and/or measured "predictable worst case" 1-hour equivalent sound levels (Leq $_{1hr}$) of the stationary source(s) are normally compared with the higher of the corresponding Leq $_{1hr}$ of road traffic or the following criteria:

Outdoor Points of Reception

The criteria for outdoor points of reception in any area amenable for use are:

Area	Time Of Day	Sound Level, dBA
Major population centres or urban areas (MOEE Class 1 Area)	Daytime and Evening 07:00 - 23:00	Leq _{1hr} 50

In the Plane of a Window

The criteria for bedrooms, living/dining areas of residences, hospitals, schools, nursing/retirement homes, day-care centres, etc. during the day and evening time periods are:

Area	Time Of Day	Sound Level, dBA
Major population centres or urban areas (MOEE Class 1 Area)	Evening 19:00 - 23:00	Leq _{1br} 45

The criteria for bedrooms or sleeping quarters during the night-time period are:

Area	Time Of Day	Sound Level, dBA
Major population centres or urban areas (MOEE Class 1 Area)	Night-time 23:00 - 07:00	Leq _{lbr} 45

For specific impulsive sources, reference should be made to the more date-stringent criteria in the MOEE Publication NPC-105.

3.0 ANALYSIS AND RESULTS

3.1 Noise Impact Methodology

1. Noise impact is a comparative evaluation of the new or intruding noise versus the existing or ambient noise in the area. Noise impact is also a comparative evaluation of the new or intruding noise versus a pre-set sound level limit (criterion) such as Leq 55 dBA. The degree of noise impact varies directly as the ratio between the intruding and existing noise levels; i.e. the more the intruding noise level exceeds the existing noise level, the higher the impact.

Since the proposed corridor traffic noise represents a future consideration, predictions must be made as to the sound noise levels which will be generated by the proposed undertaking after the roadway has been in operation for a period of at least 10 years.

2. Road traffic sound levels in this study have been predicted using the technique developed by the U.S. Federal Highway Administration (FHWA) enhanced by the Ministry of Transportation and the Ministry of the Environment and Energy.

The U.S. FHWA model was jointly revised by the MTO and the MOEE to incorporate procedures for the calculation of additional attenuation due to ground (the additional attenuation is due to the type of ground cover; for example hard, soft, ...etc. and also due to the terrain configuration or topographic features). The computerized version of the ORNAMENT model, STAMSON 5.0 was used for calculating the sound levels in all sections of the proposed undertaking. The technical data of the ORNAMENT model used and the various adjustments implemented are summarized in Appendix B.

3. The calculations are primarily based on the Peak P.M. Traffic volumes, percentages of medium and heavy trucks, posted speed limit, road to receptor distance and elevation differentials between road and the receptor, roadway gradient, pavement type and the type of ground cover between the road and the receptor in question.

Further adjustment has been applied to the P.M. Peak Leq sound levels to convert the results to the equivalent Leq 16 hrs. based on P.M. Peak - 16 hr. relationships for urban arterials in the City of North York.

Based on the MOEE directions the equivalent daytime sound level in dBA, Leq corresponding to the average hourly volume of the 16 hours traffic was used, i.e. Leq₁₆ in dBA.

3.2 STUDY OF THE ALTERNATIVES OF THE PROPOSED ROAD ALIGNMENT

(a) <u>Description of the Receptors</u>

For impact assessment purposes, the worst case receptors have been selected for the alternative alignments based on consideration of their close proximity to the proposed East Service Road, the largest angle of exposure to the proposed East Service Road and possibly the lowest ambient sound levels.

For convenience, the selected points of reception have been given code names based on abbreviations of the street names and based on the municipal street number. For example, GA76 refers to # 76 Glendora Avenue. The selected street codes are as follows:

- BP Bonnington Place - AD Anndale Drive - GA = Glendora Avenue - AA = Avondale Avenue ~ MR Marathon Reality Office Towers = .N = North building .S = South building .E = East Face .W = West Face .S = South Face - SC-APT = Sheppard Centre Apartment Tower

In accordance with the MTO/MOEE protocol, the points of reception have been taken as the closest **outdoor** living areas close to the edge of the dwelling units closest to the proposed East Service Road.

The figures included in Appendix C show the selected receptor locations.

Although for some alternatives the building facades overlooking a collector street are exposed to higher levels of ambient noise, the lower sound levels in the backyards have been used for assessment purposes where the proposed East Service Road is likely to be of concern to these homes. This approach is conservative.

In certain cases, the impact on the dwelling facades may be a little higher than the impact on the outdoor living area.

(b) <u>Description Of The Sources Of Ambient Noise</u> (Existing)

dominant sources of noise in the area are vehicular traffic movements on Sheppard Avenue to the north, Yonge Street to the west, Highway 401 to the south and several local collectors within the study In particular, the influence of Sheppard Avenue, Yonge Street and Highway 401 are dominant within the first 2 or 3 rows of houses, beyond which the so-called "urban hum" is the dominant noise which locations practically from all at all The urban hum prevails most of the time directions. within the study area until a vehicle goes by on the nearest local street to become the dominant source for a few seconds and the levels start to recede down again to the urban hum background level.

The actual sample sound level readings taken by S.S. Wilson & Associates in the summer of 1994 in the entire east and west study areas during the PM peak hours provided further assistance in establishing some form of ambient levels in the areas where predictions are less accurate and where traffic data are not available.

The measured urban hum or residual sound levels along the local roads and further away from the major roadways show minimum hourly Leq of not less than 56 dBA during the PM peak hour (equivalent to Leq day 52-53 dBA based on a 16 hour day).

When the sound levels due to local traffic is added to the urban hum, the measured PM peak hours Leq reached 62 dBA (equivalent to Leq day 59 dBA) at several locations representing the property line of the closest dwellings.

Therefore, the following are the generalized conclusions:

- i) Residences located on local collector roads in the study area may have PM peak hour Leq 60 dBA (equivalent to Leq day 57 dBA).
- ii) Residences located on Avondale Avenue are currently exposed to PM peak hour Leq 66 dBA for a typical flanking lot based on the predicted sound levels at 15 metres (equivalent to Leq day 63 dBA). These levels are the

levels expected at the exposed building facades. As most of the houses on Avondale have their backyards on the other shielded house face, it is expected that a minimum reduction of 10 to 12 dBA due to the houses themselves will reduce the sound levels in the backyards to PM peak hour Leq 55 dBA (equivalent to Leq day 52 dBA).

iii) Residences located on local streets or dead-end streets are expected to have ambient sound levels of approximately PM peak hour Leq 55 dBA (equivalent to Leq day 52 dBA).

Table 1 shows sample ambient levels based p.m. peak hours.

It is important to note that while the first row of dwellings flanking on a collector street could have sound levels up to Leq 60 dBA PM peak, and up to Leq 66 dBA PM peak hour along a "major" collector street, the sound levels are expected to go down quickly to the Leq 55 dBA urban hum level within a range of 3 to 4 rows of houses due to the following reasons:

- i) Reduced angle of exposure to the street.
- ii) Increased distance setback from the street.
- iii) The presence of fences and mature vegetation in this established community.
- iv) The presence of some minor structures such as garages.

The effect of the distance and angle of exposure have been accounted for in developing the expected ambient sound levels at the receptors of concern in the analysis to follow.

(c) <u>Future Sound Levels</u>

The proposed East Service Road may bring some of the outdoor living areas of the existing residences as close as 15 to 18 metres from the road centre line. As a result of the alignment alternatives and the expected removal of some dwelling units, there could be buffering distances up to 35 metres from the East Service Road centre line to the closest dwellings.

With the projected future PM peak hour traffic volume on the East Service Road, the following levels are predicted.

- At the closest backyards (15-18m) = Leq 69 dBA (1 hr. PM peak).
- At the further backyards (35m) = Leg 64 dBA (1 hr. PM peak).

(d) Impact Assessment

Ambient sound levels were calculated at all the receptors excluding the noise generated by the proposed road. These ambient sound levels are due to the vehicular traffic on Hwy. 401, Yonge Street, Sheppard Avenue and local streets.

Sound levels due to vehicular traffic on the proposed road were calculated with the latest traffic and road information. Tables 2 and 3 include the ambient sound levels, the calculated sound levels due to the proposed road and the excess sound levels over the ambient for the alternatives.

The data in the tables show the following parameters:

- Existing ambient sound levels.
- Future sound levels due to the proposed East Service Road.
- Applicable sound level objectives for both residential and commercial buildings.
- Calculated excesses above the ambient and objective.
- · Subjective assessments of the calculated excesses.

Figures 3 (a & b) and 4 (a & b) show graphically the predicted sound levels and excesses.

Presently, the 2 office commercial buildings owned by Marathon Reality are exposed to varying levels of traffic noise from Sheppard Avenue, Yonge Street and Doris Avenue depending on the direction of the building facade. The quietest faces are the south facades.

Several points of reception have been selected as shown in the figures in Appendix C. The ambient sound levels for the "Do-nothing" future years have been calculated and the future sound levels from the proposed East Service Road are also predicted at typical 2nd storey levels. It should be noted that the predicted ambient sound levels above the 2nd or 3rd storey levels are expected to be considerably higher than those shown in Tables 2 and 3, i.e. will result in lower noise impact.

The highest predicted sound levels due to the widening for both alternatives is a maximum Leq day 66 dBA and excess of up to 10 dBA. While the change is considered significant, the resulting outdoor sound levels on the east facade of the building are comparable and in fact lower than the Leq 70 dBA for the offices facing north, east and west.

With a predicted Leq day of 66 dBA due to the East Service Road, the anticipated indoor sound level is 45 to 50 dBA which is well within the acceptable range of indoor sound levels in offices in general.

Concerning the potential impact on the existing high rise apartment tower at the north-west corner of Sheppard and Doris, the calculated ambient due to Sheppard Avenue is Leq day 70 dBA along the south face and approximately 68 dBA along the east face. With the worst case scenarios for the re-alignment of Doris Avenue, with the mid block the predicted sound levels will result in acoustically insignificant changes for the building facing east.

(e) Noise Control Measures

In order to reduce the significance of the impact, there are two basic noise control measures which include the use of buffering distances and the use of sound barriers. A combination of such measures may offer more flexibility in meeting other planning and objectives.

Table 4 shows summary of the buffering distances for the first row of houses to meet the shown sound levels.

From the table, it is concluded that at the highest impact receptor(s), where it is desirable to meet the lowest possible objective level of Leq 52 dBA, the road set back should ideally be approximately 120 metres (measured from the road centre line to the subject residential property). As up to 5 dBA excess is allowed under the Protocol without the need for mitigation, a more realistic, but then hypothetical, setback is 60 metres (the corresponding objective sound level is Leg day 57 dBA). Therefore, it is expected that all dwelling units with low ambient sound levels within 60 metres from the East Service Road centre line may require consideration for noise control measures.

The use of sound barriers may also be considered as one of the noise control alternatives. There are 2 possibilities for sound barriers:

- a. Sound barriers to be constructed along the road r-o-w, where required, at a typical distance of 13 metres from the East Service Road centre line.
- b. Sound barrier to be constructed along the property line(s) of the dwellings of concern.

In all cases, the proposed sound barrier alternatives are aimed at protecting the ground-related outdoor amenity areas such as the backyards with little or no reduction for the 2nd storeys of the subject dwellings.

The acoustical effectiveness of the planned sound barriers depend on their locations with respect to the road and the area(s) to be protected.

The minimum required height of a barrier depends on the predicted excess above the criteria. Therefore, dwellings located further away from the East Service Road may require lower barrier heights.

Table 5 provides typical information to show minimum required barrier heights to achieve Leq day 52 and 57 dBA for a barrier located along the proposed East Service Road r-o-w.

The calculated barrier heights are approximate only as the exact barrier height depends on the actual ground elevations at the house, the base of the barrier and the road elevation as well as the location of the receptor.

The use of sound barriers, however, may introduce some negative effects such as sun shading, snow accumulation and drifting, wind effect, security and the need for periodic maintenance. Other important considerations are the visual impact of building long, continuous and high structures in existing residential areas and the associated costs of building the barrier and making the necessary changes to the existing landscaping of the areas on both sides of the barriers.

context of the overall planning redevelopment of the subject area, another viable option for noise mitigation is the "redevelopment" of limited parcels of land immediately adjacent to the selected East Service Road alignment for land uses that are more compatible with transportation noise. This may also include <u>new residential dwellings</u> or clusters of residential dwellings that incorporate noise control measures as part of the redevelopment plans in accordance with the proposed criteria in Section 3. The noise control measures may include one or a combination of the following measures:

- a) Site planning techniques for noise control to protect the new homes as well as the existing residential dwellings.
- b) Improved building acoustical insulation and design
- principles that are noise defensive.
 c) The use of localized sound barriers that can be integrated as part of the new development plan.

4.0 CONCLUSIONS AND RECOMMENDATIONS

4.1 SUMMARY

A study has been carried out to research all aspects related to the potential noise impact of the proposed East Service Road on the noise sensitive receptor locations along the proposed road. The study dealt with the documentation of the established existing ambient sound levels, the future noise associated with the movement of the vehicular traffic on the proposed road.

The excess sound levels associated with the proposed road and existing ambient have been calculated.

Tables 2 and 3 provide a summary of the existing ambient and future sound levels with the impact above the existing ambient. They also indicate if mitigation is required or not.

From the tables the following paragraphs summarize the results:

For the residential receptors located along the alignments, the calculated sound levels are in excess of 5 to 11 dBA when compared with the existing ambient sound levels. This has warranted the need for further review of the noise control measures for these receptors.

The highest predicted sound levels due to the East Service Road at the points of reception for the two office commercial buildings are up to 66 dBA. These are the worst case locations.

There is a change of up to 7 dBA in excess of the present ambient sound levels at the 2 office buildings. While the change by itself is significant, the resulting outdoor levels at these locations are comparable and in fact lower than the acceptable outdoor criterion of 70 dBA for the private and general offices. With a predicted Leq day of 66 dBA due to the East Service Road, the anticipated indoor sound level is 45 to 50 dBA, which is well within the acceptable range of indoor sound levels in general. Therefore, the sound levels Service Road to the proposed East will have acoustically insignificant impact on the commercial/office building receptors and there is no need of noise control measures for these commercial receptor locations.

It is worth noting that the north, east and west facades of the north commercial building are currently exposed to high sound levels due to Sheppard Avenue, and in fact the current levels are higher than the future sound levels due to the East Service Road.

4.2 Recommendations

1. Noise Control During Construction

In addition to the noise emitted by the operation of vehicles on the proposed undertaking, noise during the construction phase is an issue that should also be addressed.

Unlike operational noise, construction noise is temporary in nature depending on the type of work required and its location relative to the noise-sensitive receptors.

The significance of the construction noise impact depends on the number of pieces of equipment, their types, time of operation and their proximity to the receptors in question.

The following is a brief outline of the procedures to be followed in handling construction noise during the Detail Design and Construction phases:

- a. Noise sensitive areas will be identified.
- b. Applicable local municipal noise control by-laws will be identified and obeyed. The by-laws include those enacted under the authority of the Municipal; Act, the Environmental Protection Act or any other Provincial Legislation. Where timing constraints or any other provisions of the municipal by-law may cause hardship to the proponent, an explanation of this will be outlined in a submission to the MOEE and an exemption from such by-law will be sought directly from the area municipality in question.
- c. "General noise control measures" (not sound level criteria) will be referred to, or placed into the contract documents.
- d. Should the municipality receive any complaint from the public, the municipality staff will verify that the "general noise control measures" agreed to are in effect. The municipality will investigate any noise concerns, warn the contractor of any problems and enforce its contract.

- e. If the "general noise control measures" are complied with, but the public still complain about noise, the municipality will require the contractor to comply with the MOEE sound level criteria for construction equipment contained in the MOEE's Model Municipal Noise Control By-Law. Subject to the results of field investigation, alternative noise control measures will be required, where these are reasonably available.
- f. In selecting the appropriate construction noise control and mitigation measures, the municipality will give consideration to the technical, administrative, and economic feasibility of the various alternatives.

The above noted procedures are based on the construction noise provisions included in Section 8 of the MOEE/MTO Protocol.

2. Noise Control Measures

In order to reduce the significance of the impact, three basic noise control measures may be applied. These include the selection of the alternative alignment with the least impact, creation of the buffering distances and the use of sound barriers. When selecting sound barriers as sound control measures, the extent of these barriers, their top elevations and material specifications should be studied during the detail design stage of the proposed road.

3. Planning of Future Residential Land Use Adjacent to East Service Road

In the course of preparing the Environmental Assessment for the subject road, the existing and future sound levels at typical existing residential neighbourhoods along this road have been predicted. In general, the future sound levels exceeded Leq 55 dBA, which is the Provincial Objective sound level for new residential developments.

With the potential future increase in traffic volumes along the proposed East Service Road and the existing roads, the sound levels are expected to be in excess of the Provincial Objective.

Therefore, it is recommended that future development and re-development proposals for planning of new residential developments along the proposed road be examined for their noise compatibility. The Provincial and Ministry of the Environment and Energy policies and guidelines should, therefore, be consulted concerning implementation at the municipal planning levels. The noise control measures may include one or a combination of the following measures:

- a) Site planning techniques for noise control to protect the new homes as well as the existing residential dwellings.
- b) Improved building acoustical insulation and design principles that are noise defensive.
 c) The use of localized sound barriers that can be integrated as part of the new development plan.

TABLES

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TABLE 1

Location	Existing Ambient Leq (PM peak hours)
Residences located on Avondale Avenue	55 dBA
Residences on dead end roads and minor streets (e.g. Anndale Dr.)	56 dBA

S.S. Wilson & Associates

Table2 PREDICTED AMBIENT SOUND LEVELS AND FUTURE SOUND LEVELS EAST SERVICE ROAD NOISE IMPACT TRADEWIND

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- Significant	MR-S-SF	420		2 6	.			
		32.0	0.7c	/۵	2	5.0	Significant	-13.0
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		· ·						
	(mm n = 1)							

0 to < 3 dB change : Insignificant => 5 to < 10 dB change: Significant => 3 to < 5 dB change : Noticeable => 10 dB change : Very Significant

Table3 PREDICTED AMBIENT SOUND LEVELS AND FUTURE SOUND LEVELS FUTURE EAST SERVICE ROAD MIDBLOCK

MIDBLOCK NOISE IMPACT

Change due to the Future Leq, dBA Minus Ambient Leq, dBA Very Significant Very Significant Very Significant Very Significant Very Significant Very Significant Very Significant Very Significant Significant Significant Significant Significant Significant Significant Significant Significant Significant Significant				Applicable	Excess	Future Leg, dBA	Significance of the	Future Leg. dBA
S2.0 G6.0 S5 S T4.0 Very Significant S2.0 G6.0 S5 S T4.0 Very Significant S2.0 G6.0 S5 S T4.0 Very Significant S2.0 G6.0 S5 S T4.0 Very Significant S2.0 G6.0 S5 S T4.0 Very Significant S2.0 G6.0 S5 S T4.0 Very Significant S2.0 G6.0 S5 S T4.0 Very Significant S2.0 G6.0 S5 S T4.0 Very Significant S2.0 G6.0 S5 S T4.0 Very Significant S2.0 G6.0 T4.0 Very Significant S2.0 G6.0 T4.0 Very Significant S4 S2.0 T4.0 Very Significant S5 S T4.0 Very Significant S4 S2.0 T4.0 T6 S S6 Significant S5 S6 S6 S6 Significant S5 S6 S6 Significant S5 S6 S6 S6 Significant S5 S6 S6 S6 Significant S5 S6 S6 S6 S6 S6 S6 S6	Receptor No.	Ambient Leq, dBA	Future Leg, dBA	Sound Level	Criteria for	Minus	Change due to the	Minus
140 Very Significant 152.0 66.0 55 5 14.0 Very Significant 152.0 66.0 55 5 12.0 Very Significant 152.0 66.0 55 5 11.0 Very Significant 152.0 66.0 55 5 14.0 Very Significant 152.0 66.0 70 5 3.0 Very Significant 152.0 66.0 70 5 3.0 Very Significant 152.0 66.0 70 5 5.0 Significant 152.0 55.0 55.0 Significant 152.0				Criteria	mitigation	Ambient Leg, dBA	Future Leg, dBA Minus Ambient Leg. dBA	Criteria
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52.0 64.0 55 5 12.0 Very Significant 52.0 66.0 55 5 14.0 Very Significant 52.0 66.0 55 5 14.0 Very Significant 52.0 66.0 55 5 14.0 Very Significant 52.0 65.0 55 5 11.0 Very Significant 52.0 65.0 55 5 11.0 Very Significant FF 52.0 65.0 70 5 11.0 Very Significant FF 52.0 66.0 70 5 3.0 Noticeable FF 52.0 57.0 5 7.0 Significant SF 52.0 50.0 5 5.0 Significant SF 52.0 50.0 5 50.0 Significant SF 52.0 50.0 50.0 Significant SF 52.0 50.0 Significant SF 52.	GA42	52.0-	66.0	55	5	14.0	Very Significant	11.0
52.0 63.0 55 5 11.0 Very Significant 52.0 66.0 55 5 14.0 Very Significant 52.0 66.0 55 5 14.0 Very Significant 52.0 65.0 65.0 55 5 11.0 Very Significant 52.0 63.0 55 5 11.0 Very Significant 52.0 68.0 71.0 70 5 3.0 Very Significant EF 59.0 66.0 70 5 7.0 Significant EF 57.0 50.0 5 7.0 Significant SF 52.0 56.0 70 Significant SF 52.0 56.0 70 Significant SF 52.0 Significant SF 50.0 Significant SF 50.0 Significant SF 70 Significant	GA53	52.0	64.0	55	5	12.0	Very Significant	0.6
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52.0 65.0 55 5 13.0 Very Significant F1-ES 68.0 71.0 5 11.0 Very Significant FF 68.0 71.0 70 5 Noticeable FF 52.0 66.0 70 5 7.0 Significant SF 57.0 70 5 5.0 Significant SF 52.0 59.0 70 5 Significant SF 52.0 59.0 70 5 7.0 Significant SF 52.0 59.0 70 5 7.0 Significant	****				5			
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57.0 65.0 70 5 8.0 Significant 52.0 59.0 70 5 7.0 Significant	MR-N-SF	52.0	57.0	22	5	5.0	Significant	-13.0
52.0 65.0 70 5 8.0 Significant 52.0 59.0 70 5 3.0 Significant 5.0 5.0 Significant 5.0 5.0 Significant 5.0 Sign	MR-S-EF			70	5		Nipolitical in the control of the co	2:0
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					,	2	Significant	0.11.0
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0 to < 3 dB change; Insignificant => 5 to < 10 dB change; Significant => 3 to < 5 dB change; Noticeable => 10 dB change; Very Significant

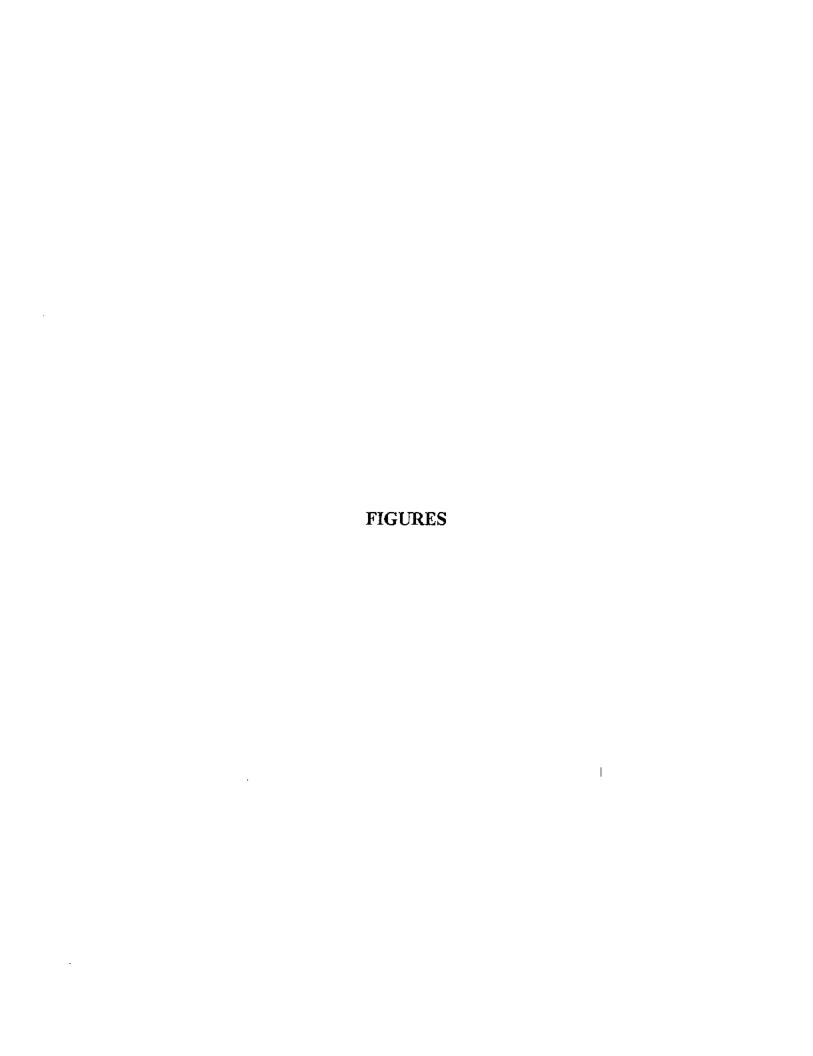
TABLE 4

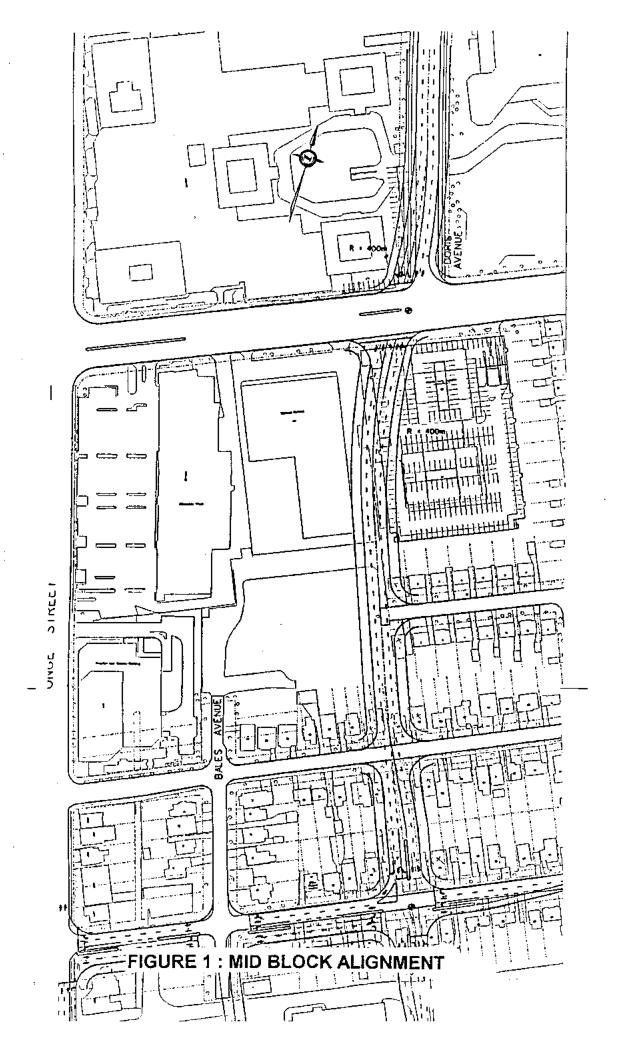
Desired Leq Day Sound Level dBA	Minimum Distance from the Road Centre Line (m)
66	18
65	20
64	23
63	26
62	30
61	35
60	40
59	46
58	53
57	61
56	70
55	80
54	92
53	106
52	121

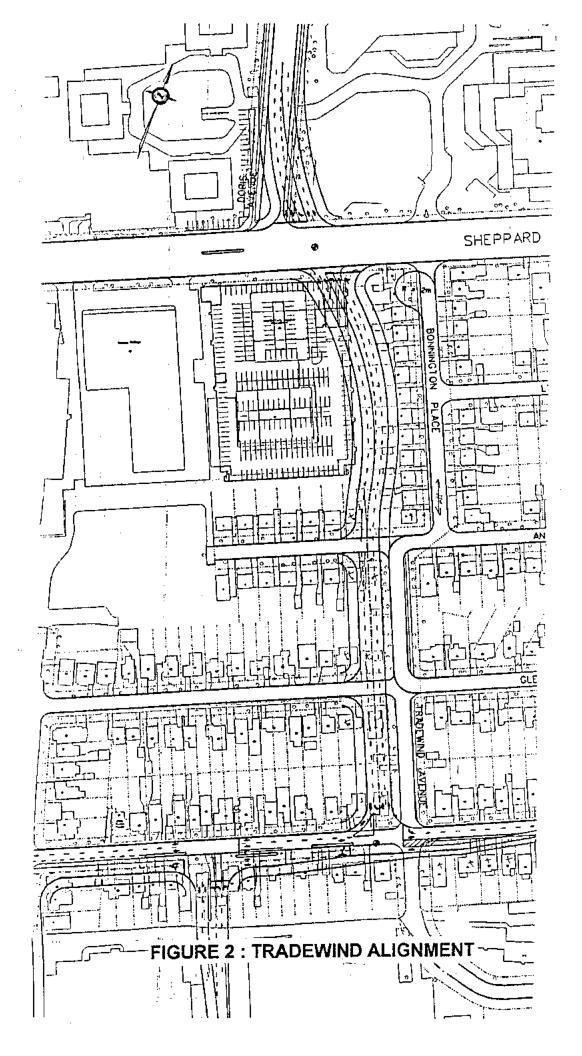
TABLE 5

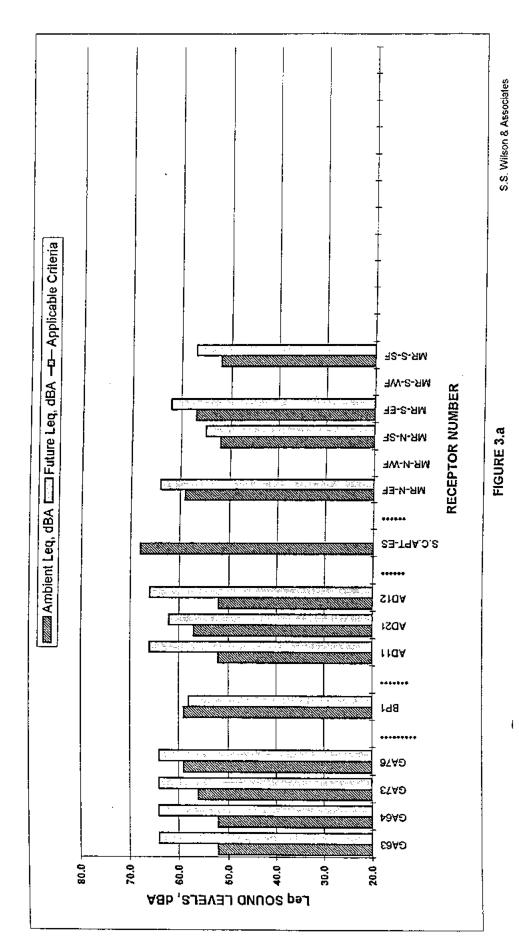
	Barrier Heig	ht to Achieve
Distance from East Service Road Centre Line to Dwelling Property Line (m)	52 dBA	Leq (d) 57 dBA (m)
15	5.0	3.0
20	4.7	2.8
25	4.5	2.5
30	4.2	2.1
35	3.9	2.0
40	3.6	2.0
50	3.0	1.8
60	2.4	Not Required

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PREDICTED AMBIENT SOUND LEVELS AND FUTURE SOUND LEVELS EAST SERVICE ROAD NOISE IMPACT TRADEWIND

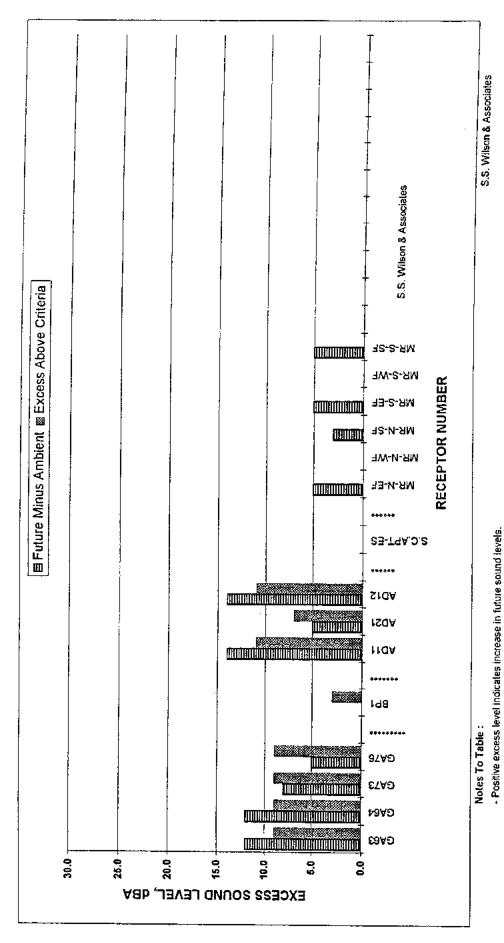
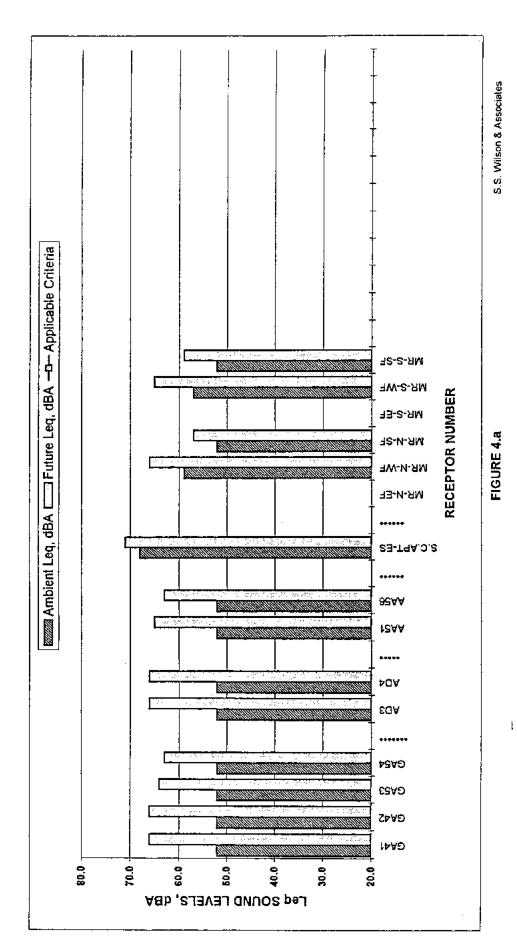


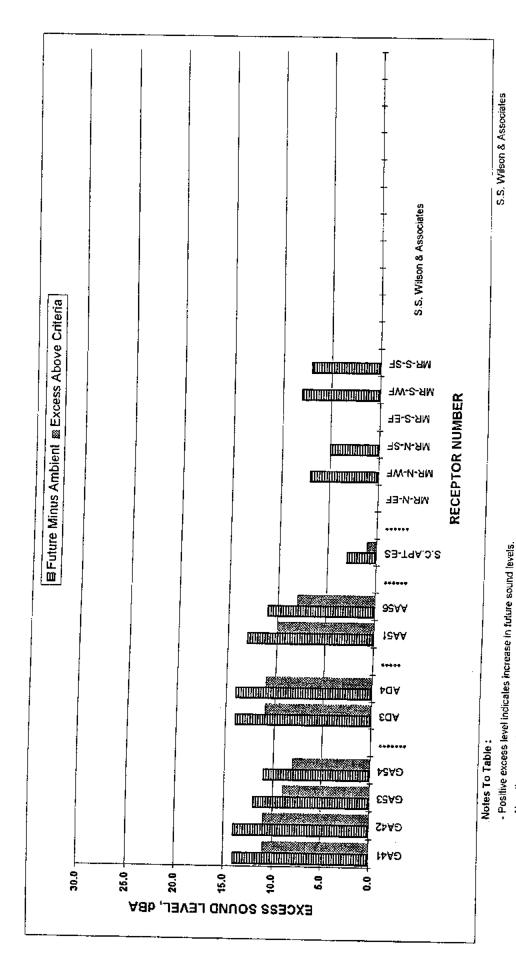
FIGURE 3.b

- Negative excess-level indicates decrease in future sound levels.

RECEPTORS EXPERIENCING INCREASED SOUND LEVELS EAST SERVICE ROAD NOISE IMPACT TRADEWIND



PREDICTED AMBIENT SOUND LEVELS AND FUTURE SOUND LEVELS
FUTURE EAST SERVICE ROAD
MIDBLOCK
NOISE IMPACT



RECEPTORS EXPERIENCING INCREASED SOUND LEVELS FUTURE EAST SERVICE ROAD FIGURE 4.b MIDBLOCK Negative excess level indicates decrease in future sound levels.

NOISE IMPACT

APPENDIX A:

MOEE/MTO PROTOCOL FOR PROVINCIAL HIGHWAYS NOISE

This Protocol contains areas of policy agreement between the Ministries of Transportation and Communications, and Environment for dealing with noise concerns during the preparation, review, and evaluation of environmental assessments for Provincial Highway undertakings.

As common understandings are resolved for any outstanding issues, these will be added to the Protocol by formal agreement.

D.P. Caplice

Assistant Deputy Minister Operations Division Ministry of Environment J.R. Barr

Assistant Deputy Minister Engineering and Construction Ministry of Transportration and Communications

FEDRUARY 1906 Retrofft The MTC policy for retrofft of existing freeways with sound barriers will remain in effect and unchanged.

Scope of Protocol

This protocol applies to the MTC Capital Construction Program for all classes of MTC Provincial roads, both urban and rural. The policy for each situation may require different noise control measures and further, that an assessment of the feasibility of providing noise control measures includes technical and economic considerations.

3. Definition of Noise Sensitive Areas

To be clearly defined, as guided by the One-Stage Procedural Guidelines and the specific definitions of "residential areas" and "quiet zones" found in the municipal noise control by-laws, approved by MOE under the Environmental Protection Act.

4. Establishing Existing and Future Hoise Levels

Presently used prediction methodologies and measurement procedures are satisfactory. Any future changes, in noise prediction methodologies or measurement procedures, shall be compatible with those of both MOE and MTC.

Staff of MTC and MOC together shall set a standard for ambient noise levels in rural areas where predictions cannot be done.

Impact Assessment

Noise impacts for all MTC Provincial roads will be predicted based on traffic projections ten years after completion, or best available data when 10-year projections are not available.

The study area shall be defined using the smaller of one of the two following methods: using 5 decibe) contour lines extending from the source to the point where there is no increase above the ambient level, or a distance of 600 m from the source.

The noise impact on noise-sensitive land uses will be determined for outdoor spaces.

All reference to 65 dDA as a "target" and 70 dDA as a "maximum" will be removed from MTC directives A-1 and B-94. Further, reference to a 70 dBA maximum should be removed from the Provincial Policy. The objective for outdoor sound levels is the higher of the Leq 55 dDA or the existing ambient. The significance of a noise impact will be quantified by using this objective in addition to the change in noise level above the ambient.

Mitigation will attempt to achieve levels as close to, or lower than, the objective level as is technically, economically, and adminis-

G. Hoise Control Measures

The attached Table summarizes the degree of mitigation effort to be applied for various noise level increases.

On right-of-way mitigation measures will be identified, considered

Mitigation measures within the right-of-way include: berms, vertical and horizontal alignments, pavement surfaces, etc. barriers.

Where noise increases above the ambient do not exceed 5 dBA no mitigation is required.

Where noise increases above the ambient exceed 5 dDA MTC will:

- investigate noise control measures within the right-of-way - If project costs are not significantly affected and where averaged over first row receivers, a minimum attenuation of 5 dbA can be achieved, MTC will introduce the selected measures within the right-of-way.

Where a freeway is to be expanded through an existing residential area that has been included on the retrofit priority list, noise attenuation measures should be considered as part of the freeway expansion project when the MTC policy for Retrofit of Existing Freeways can be satisfied.

7. Documentation

MTC will increase its E.A. documentation with respect to the feasibility of all potential mitigation measures within the right-of-way. The feasibility of each measure would be evaluated by such factors as effectiveness and technical and economic feasibility.

B. Construction Noise

The following is a brief outline of the procedures to be followed in handling construction noise during the Environmental Assessment process and during the construction phase. following shall be made in all E.A. Documents: Commitment to the

- (a) Noise sensitive areas will be identified;
- (b) Applicable municipal noise control by-laws will be identified and obeyed. Where timing constraints, or any other municipal by-law may cause hardship to MIC, an explanation of this will be outlined in the EA document, and an exemption from such by-law will be sought directly from the municipality in question.

- (c) General noise control measures (not sound level criteria) will be referred to, or placed into MTC contract documents;
- (d) Any initial complaint from the public will require verification by MTC that the general noise control measures agreed to are in effect; MTC will investigate any noise concerns, warn the contractor of any problems, and enforce its contract;
- (e) Notwithstanding compliance with the "general noise control measures", a persistent complaint will require a contractor to comply with MOE sound level criteria for construction equipment contained in the MOE Model Municipal Noise Control Dy-Law. Subject to the results of field investigation, alternative noise control measures will be required, where these are reasonably available: and
- In selecting the appropriate construction noise control mitigation measures, MTC will give consideration to technical, administrative, and economic feasibility of the various alternatives.

9. Miscellaneous

- (a) All future technical documents referred to in this agreement and prepared to become part of the Protocol shall be Jointly approved by MOE and MTC. These include:
 - o ambient levels in Rural Areas where predictions cannot be
 - o general construction noise control measures; and
 - o any other alterations to this Protocol.
- (b) As the intent of this Protocol will be followed during their preparation, joint MOE/MTC approval is not required for MOE or MTC procedural/operational documents such as:
 - o internal directives;
 - o contract documents; and
 - o E.A. procedural/technical guidelines.

TABLE 1: SUMMARY OF MITIGATION EFFORT

CHANGE IN NOISE LEVEL ADOVE AMDIENT	MITIGATION EFFORT
0 - 5 dBA > 5 dBA	- None - Investigate noise control measures on R.O.W. - If project cost is not significantly affected introduce noise control measure within R.O.W. - Noise control measures, where introduced, should achieve a minimum of S dBA attenuation, over first row receivers. - Mitigate to ambient, as administratively, economically, and technically feasible.

APPENDIX B: TRAFFIC NOISE PREDICTION MODEL

GENERAL PROCEDURES AND ADJUSTMENTS

1.1 MOE ROAD TRAFFIC NOISE PREDICTION TECHNIQUE

The road traffic noise assessment method is based on a model originally developed by the U.S. Federal Highway Administration in 1978 as modified by the Ontario Ministry of the Environment to suit the provincial requirements.

The analytical model predicts hourly Leq due to road traffic. It is modular in structure and thereby lends itself to applications requiring detailed analysis.

The variables required for the road traffic assessment include the following: road traffic volume per hour, percentages of automobiles, medium trucks and heavy trucks, average speed of traffic flow, roadway gradient, source to receiver distance(s), type of ground cover, road element size and shielding applicable.

The details of the model could be found in the publication "Ontario Road Noise Analysis Method for Environment and Transportation (ORNAMENT)1", Ministry of the Environment, November 1988.

The applicable procedures are summarized in the following paragraphs. Sample calculations are included in this report for a typical receiver location.

1.1.1. Predicted sound level data are generally based on two daily periods or the full 24 hour period as requested by the MOE for specific sources:

07:00 to 23:00 hours 23:00 to 07:00 hours

1.1.2. Roadway traffic volumes (AADT) split:

Regional Roads

Provincial Highways

07:00 to 23:00 hours = 91% 07:00 to 23:00 hours = 85%

23:00 to 07:00 hours = 9% 23:00 to 07:00 hours = 15%

1.1.3. Reference Hour Sound Level:

$$Leq_{ref} = 10 \log \sum_{i=1}^{3} \{K_g P_i 10^{\frac{(L_0)_i}{10}}\} = 10 \log S + 2.76$$

The computerized versions of this model are 'STAMSON 3.0 and STAMSON 4.1'.

$$(L_0)_{AUTOMORIL}$$
 = 38.1 log(S) - 2.4

$$(L_0)_{MEDIUM\ TRUCK} - 33.9 \log(S) + 16.4$$

$$(L_0)_{HEAVY\ TRUCK} = 24.6 \log(S) + 38.5$$

₽, as fraction of the total volume;

the reference energy mean emission level of ith vehicle class;

the posted speed limit in km/h. S

Adjustments to Reference Level (dB) 1.1.4.

o Traffic Volume:

Adjustment = 10 log (V/V_{ref}) = 10 log (V/40)

where V is the total traffic volume.

O Distance:

Adjustment = 10 log $(D_{ref}/D)^{1+\epsilon}$

where D, is reference distance of 15 m.

a = 0 for reflective surfaces (hard ground)

 $\alpha = 0.66$ for absorptive surfaces (soft ground) where h_{ar}, ≤ 3 m

 α = 0.75(1-(h_{eff}/25)) for absorptive surfaces where 3 < h_{eff} \leq 25 m

 $\alpha = 0$ for absorptive surfaces where $h_{aff} > 25$ m

$$h_{eff} = s + p + t + r$$

where h,, is the total effective height.

a is ground absorbtion coefficient.

Road Segment

Non-Reflective Surface :

Adjustment - 10
$$\log \left\{ \frac{1}{\pi} \int_{\Phi_1}^{\Phi_2} \cos^{\alpha} \Phi \ d\Phi \right\}$$

Reflective Surface :

Adjustment = 10 log
$$\{\frac{\Phi_2 - \Phi_1}{\pi}\}$$

where ϕ_1 is the negative angle of view; ϕ_2 is the positive angle of view.

1.1.5. Typical Receiver and Source Heights:

Outdoor Living Areas (OLA) = 1.5 m

Second Storey Bedroom = 4.5 m

Source Height = 0.5 m where $P_{pr} < 0.01$

Source Height = $\sqrt[4]{100 \ P_{HT}}$ where 0.01 \leq P_{RT} \leq 0.30

Source Height = 2.4 m where $P_{pr} > 0.30$

where P_{mr} is the percentage of heavy trucks, unadjusted by the gradient factor, expressed as a fraction of the total volume.

1.2 BARRIER CALCULATION MODEL

- 1.2.1. Barrier attenuation is calculated using optical diffraction theory.
- 1.2.2. Attenuation for road traffic noise is calculated at 500 Hz for an incoherent infinite line source.
- 1.2.3. The barrier prediction model has been developed by the National Research Council which is somewhat more conservative than the Kurze and Anderson original model.

Barrier Atenuation - 0 dB,

for
$$(N_0)_i \cos \phi \le -0.1916$$

Barrier Attenuation -
$$10\log\{\frac{1}{\Phi_2-\Phi_1}\int_{\Phi_1}^{\Phi_2}\frac{\tan^2\sqrt{2\pi}|N_0|_i\cos\Phi}{\sqrt{10}|2\pi|N_0|_i\cos\Phi}|d\Phi\}$$
,

for -0.1916
$$\leq$$
 $(N_0)_1 \cos \phi \leq 0$

Barrier Attenuation -
$$10\log\{\frac{1}{\Phi_2-\Phi_1}\int_{1}^{\Phi_2}\frac{\tanh^2\sqrt{2\pi}\ (N_0)_i\cos\Phi}{\sqrt{10}\ 2\pi\ (N_0)_i\cos\Phi}\ d\Phi\},$$

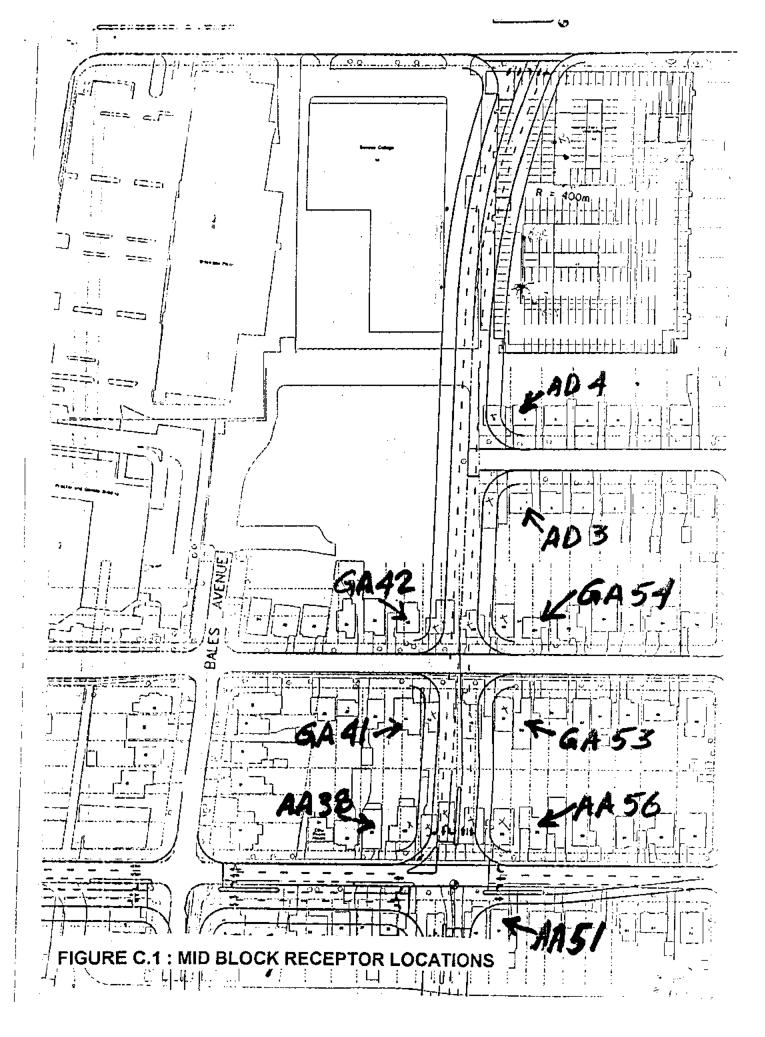
for
$$0 \le (N_0)_{\pm} \cos \phi \le 5.03$$

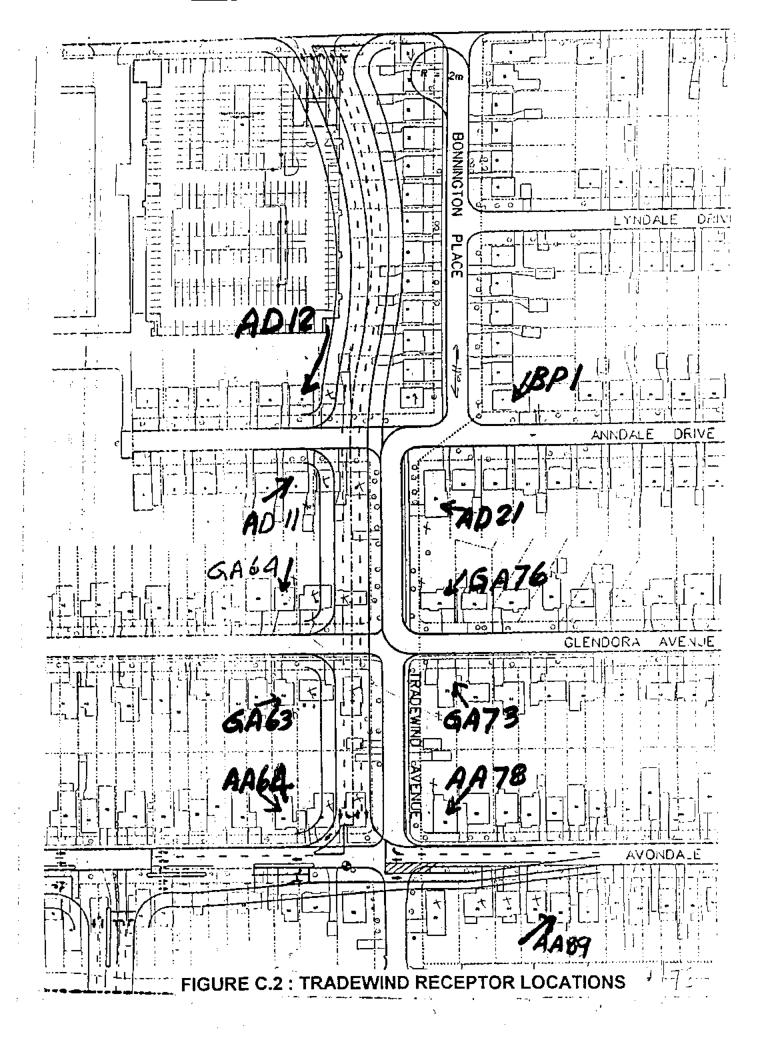
Barrier Attenuation - 20 dBA

for
$$(N_0)_i \cos \phi \ge 5.03$$

where N_0 is Fresnel Number, $N_0 = 2.915 \times (P.L.D.)$ Master Disk/APPENDIX/ROAD/APPENDIX.A

APPENDIX C: RECEPTOR LOCATIONS







APPENDIX D

AIR QUALITY ASSESSMENT FOR THE EAST SERVICE ROAD, NORTH YORK, ONTARIO

Consulting Engineers Microclimate Specialists

Rowan Williams Davies & Irwin Inc.

AIR QUALITY ASSESSMENT FOR EAST SERVICE ROAD NORTH YORK, ONTARIO

Report 95-199T-14B September 4, 1996

Submitted to:

COLE SHERMAN AND ASSOCIATES LTD.

By:

ROWAN WILLIAMS DAVIES & IRWIN Inc.
GUELPH, ONTARIO

PROJECT TEAM

David S. Chadder, Hon. B.Sc., QEP Project Manager / Principal

Marion L. Baldwin, B.Sc. (Eng.)
Technical Co-ordinator

Anton E. Davies, Ph.D., P.Eng., QEP Principal



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	2.1 Vehicular Emission Analysis	2
	2.2 Vehicular CO and NO _x Emission Rates	4
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1. INTRODUCTION

Rowan Williams Davies and Irwin Inc. (RWDI) was retained by Cole Sherman and Associates to address air quality concerns resulting from the proposed North York South Downtown Development. The initial study was completed under RWDI Report Number 95-199T-14, dated April 26, 1995. Both qualitative and quantitative air quality assessments were performed in the initial study, with the prediction that future vehicular traffic in the North York South Downtown Development will not produce pollutant levels of carbon monoxide (CO) and nitrogen dioxide (NO₂) that exceed the applicable provincial criteria.

The present report details further study of the proposed East Service Road. Air quality concerns were addressed by numerically modelling vehicular emissions of CO and oxides of nitrogen (NO_x) for a representative intersection along the proposed route. NO_x consists primarily of nitric oxide (NO) and nitrogen dioxide. The objectives of this study were to:

- i) conduct a qualitative review of the seven initial roadway route alternatives, and
- quantify, under worst-case conditions, the impact of the preferred route alternative on the local air quality.

The qualitative review involved an evaluation of a number of signalized intersections, number of vehicle movements, proximity to receptors of interest, and the amount of vehicle queuing. The results of this review were forwarded to Cole Sherman in a letter dated April 4, 1996, and are attached in Appendix A.

2. METHODOLOGY

The purpose of this assessment was to determine the impact of emissions from vehicles using the proposed East Service Road for the build year 2020. The assessment was conducted using both worst-case meteorological and traffic assumptions. The pollutants examined were tailpipe emissions of CO and NO_x (specifically NO₂) from both cars and trucks idling at nearby intersections and travelling along adjacent roadways. These pollutants both have readily available emissions data and provincial criteria as established by the Ontario Ministry of Environment and Energy (MOEE). The numerical analysis concentrated on the intersection with the highest predicted traffic volumes, which was found to be the morning rush-hour period.

2.1 Vehicular Emission Analysis

Environment Canada's MOBILE5C vehicular emissions model was used to determine emission rates of CO and $\mathrm{NO_x}$ [1]. Table 1 presents the key inputs into the MOBILE5C model. The vehicle mix was based on information provided by Cole Sherman [3], which indicated that 15% of future traffic is trucks and buses (one-third buses, one-third medium trucks, and one-third heavy trucks). The MOBILE5C model classifies all vehicles that weigh more than 3 860 kg (8 500 lb) as "heavy duty diesel vehicles". This classification encompasses the Ministry of Transportation classifications of both medium trucks (4 500 kg to 12 000 kg) and heavy trucks (> 12 000 kg).

Table 1: MOBILE5C Input Parameters

Design Year: 2020

Ambient Temperature:

-6.6°C, based on the mean daily temperature at Downsview Airport for the coldest month of the year (i.e., January) [2].

Vehicle Mix:

Vehicle mix from data obtained from Cole Sherman [3] and MOBILE5C default values.

light-duty gas vehicles	49.8%
light-duty gas trucks	30.9%
heavy-duty gas vehicles	3.1%
light-duty diesel vehicles	0.2%
light-duty diesel trucks	0.6%
heavy-duty diesel vehicles	15.0%
(includes buses)	
motorcycles	0.4%

Ontario vehicle statistics and default cold-start vehicle fraction as given by the MOBILE5C manual.

Vehicle Speeds:

Default vehicle speed (33 km/h) for urban roads as given by the MOBILE5C model.

2.2 Vehicular CO and NO_x Emission Rates

The vehicular CO and ${
m NO_x}$ emission rates obtained from the MOBILE5C model are summarized in Table 2.

Table 2: Predicted Vehicle Emission Rates

Emission Source	Pollutant Emission Rate			
	со	NO _x		
Idling (g/veh/min)	5.43	0.159		
Mobile (g/veh/km)	18.7	1.50		

2.3 Air Quality Criteria

Emissions from vehicles are currently regulated by Transport Canada (Federal) regulations. Provincial regulations do not directly control the emissions from vehicles or pollutant concentrations arising from vehicular activities. However, Ontario Regulation 337 provides desirable ambient air quality objectives under which emissions from vehicles can be evaluated [4]. Table 3 presents Ontario's Ambient Air Quality Criteria (AAQC) for 1-hour CO and 1-hour NO₂. Note that there are no AAQCs for NO_x or NO.

Table 3: Ontario's Ambient Air Quality Criteria

Pollutant	Averaging Period	Air Quality Criteria (ppm)
Carbon Monoxide (CO)	1-hour	30
Nitrogen Dioxide (NO₂)	1-hour	0.20

2.4 Dispersion Analysis

The vehicular emissions obtained from the MOBILE5C model were used to predict worst-case concentrations of NO_x and CO at selected areas using dispersion modelling techniques. The dispersion simulation model used was CAL3QHC. This model, which was originally developed by the U.S. Environmental Protection Agency, was designed specifically for modelling the dispersion of emissions from motor vehicles travelling near roadway intersections [5]. By including emissions from idling vehicles, CAL3QHC represents a reliable model for predicting pollutant concentrations near signalized intersections where idling vehicles interact with moving vehicles. The model has been accepted by the MOEE for use in roadway environmental assessments.

2.5 Modelled Scenario

The air quality impact due to highway emissions are, among other factors, dependent upon the traffic volume, vehicle speed, and the roadway cross-sections. The assessment considered the proposed East Service Road bound by Greenfield Ave. to the north and Avondale Ave. to the south. The modelled roadway scenario was based on the drawing entitled Midblock - North York South Downtown Class Environmental Assessment Study, as supplied by Cole Sherman [6]. For detailed numerical modelling, the intersection of the proposed East Service Road with Sheppard Ave. was selected, as it is predicted to service the greatest volume of future traffic of all intersections along the East Service Road study area (see Figure 1).

2.6 Input Parameters for CAL3QHC Dispersion Model

The CAL3QHC model required the following input parameters to assess the pollutant levels.

i) Roadway and Receptor Coordinates

Figure 1 illustrates the roadways that were modelled and the receptor locations at which pollutant levels were predicted. Twenty-two receptors were selected, including entrances to nearby buildings and residences, and other sensitive locations. Receptors were placed at specific locations to evaluate the impact on pedestrian traffic, such as at entrances to the Sheppard Centre and Marathon commercial buildings. Nearby residences were also selected as receptors, as persons



residing within are exposed to the ambient air quality on a permanent basis. All of the receptors were located at least 3 m away from the edge of the roadways in order to be outside of the mixing zone created by the wake of moving vehicles. For simplicity, all roadways and receptors were assumed to be located at grade level, producing conservative results.

ii) Traffic Volumes and Traffic Light Cycles

Morning and evening peak hourly traffic volumes for the adjacent roadways were supplied by Cole Sherman [3], together with the information on traffic light cycles at the associated intersections [6]. Analysis of the traffic data indicated that maximum traffic volumes occurred during the morning peak period; therefore, predicted hourly traffic volumes at the East Service Road/Sheppard Ave. intersection for the morning rush-hour were used in the dispersion analysis. A traffic light cycle of 110 seconds was used, with green time equal to two thirds of the cycle time in the east-west direction (along Sheppard Ave.) [7]. Appendix B contains the traffic volumes and model co-ordinates for each traffic link modelled.

iii) Surface Roughness

Mechanical turbulence is generated by air flowing over a surface. This turbulence influences the dispersion of pollutants near the surface. For modelling purposes, the study area was considered to be an office area and, therefore, a generic roughness (Z_o) equal to 175 cm (city land use/offices) was selected.

iv) Meteorological Conditions

Worst-case meteorological conditions used in the CAL3QHC dispersion analysis are documented in Table 4.

Table 4: Meteorological Inputs to the CAL3QHC Model

Parameter	1- Hour Meteorological Conditions
Pasquill Stability Class	Class E
Wind Speed (m/s)	1.0
Mixing Height (m)	300

v) Background Concentrations

As part of the assessment of vehicle emissions, background concentrations of the contaminants within the ambient air were required. Background levels were added to the levels predicted by CAL3QHC for comparison with the provincial AAQC. Table 5 presents the 99th percentile 1-hour background levels obtained from the MOEE's monitoring station at Hendon Avenue (Yonge/Finch) Station (ID Number 34020) [8] for the year 1993. The background levels in this year were slightly greater than the three-year average background values for this station (1991 to 1993).

Table 5: Ambient Air Concentrations, MOEE's Hendon Avenue Station, 1993

Pollutant	1-Hr Averaging Period		
	99 th Percentile (ppm)		
Carbon Monoxide (CO)	2.5		
Nitrogen Dioxide (NO ₂)	0.060		
Oxides of Nitrogen (NO _x)	0.169		
Ozone (O ₃)	0.0619		

The ozone data presented in Table 5 is required to predict the worst-case NO_2 concentrations. Vehicles emit NO_x (approximately 95% NO and 5% NO_2) and the NO component of the NO_x emission reacts photochemically with O_3 to form NO_2 . The reaction rate is restricted by the availability of O_3 and light. The Ozone Limiting Method was used to predict worst-case NO_2 concentrations [9]. Equations 1 and 2 define the method.

$$|f[O_3]_B < (A+B(1-A))[NO_x]_R [NO_2]_B = A[NO_x]_B + [O_3]_B + [NO_2]_B$$
(1)

$$|f[O_3]_B \ge (A+B(1-A)) [NO_x]_R [NO_2]_R = A [NO_x]_R + B(1-A)[NO_x]_R + [NO_2]_B$$
(2)

where: $[O_a]_B$ = the background ozone level (ppm);

[NO_x]_B = total NO_x contribution from vehicles at the selected receptor location (ppm);

[NO₂]_R = the predicted worst-case NO₂ concentration at the receptor location (ppm);

 $[NO_2]_B$ = the background NO_2 concentration (ppm);

A = the fraction of NO_x emitted vehicle exhaust as NO₂ (assumed to be 0.05)

[10][11]; and

B = the fraction of NO_x converted to NO₂ as it disperses towards the receptors

(assumed to be 0.25) [12].

In Equation 1, the 99th percentile values used for NO_2 and O_3 are assumed to occur concurrently (i.e., NO_2 plus O_3 , as shown in Table 5), which is a conservative assumption.

3. RESULTS

Table 6 summarizes the results of the CAL3QHC dispersion modelling. The table shows the worst-case predicted 1-hour CO and NO₂ concentration at each receptor and the respective 1-hour AAQC. The background concentration of 2.5 ppm is included in the predicted CO values. The predicted NO₂ values were calculated using the Ozone Limiting Method, as described in Section 2.6(v), and include the NO₂ background concentration of 0.060 ppm. The maximum concentrations are presented in bold.

Table 6: Predicted Worst-Case 1-Hour CO and NO2 Concentrations (ppm) By Receptor

Receptor	Description	1-hour CO	1-hour NO ₂
1	NW of intersection (Sheppard Centre)	9.1	0.141
2	NW of intersection (Sheppard Centre)	7.1	0.134
3	NW of intersection (Sheppard Centre)	5.7	0.106
4	SW of intersection (Seneca College entrance)	7.6	0.138
5	SE of intersection (Marathon Bldg)	10.8	0.145
6	SE of intersection (Marathon Bldg entrance)	8.9	0.139
7	SE of intersection (Marathon Bldg entrance)	7.3	0.135
8	Sheppard Ave. and Bonnington Pl. (entrance to residence)	8.7	0.141
9	Sheppard Ave. and Bonnington Pt. (entrance to residence)	7.1	0.135
10	Sheppard Ave. and Bonnington Pl. (residence - backyard)	6.2	0.133
11	Sheppard Ave, and Bonnington Pl. (entrance to residence)	10.0	0.147
12	Sheppard Ave. and Bonnington Pl. (entrance to residence)	6.9	0.136
13	Sheppard Ave. and Bonnington Pl. (entrance to residence)	9.4	0.144
14	SE of intersection (outside Marathon Bldg)	7.0	0.135
15	East Service Road and Anndale Dr.	5.4	0.109
16	NE of intersection (100 Sheppard Ave)	5.8	0.115
17	NE of intersection (park)	9.8	0.144
18	NE of intersection (park)	9.0	0.141
19	NE of intersection (park)	8.1	0.138
20	NE of Intersection (park)	7.4	0.136
21	NE of intersection (park)	6.9	0.134
22	SE of intersection (outside Seneca College)	8.0	0.137
AAQC		30.0	0.20

The results of the dispersion modelling indicate that the impact of vehicle emissions of CO and NO₂ are all predicted to be below their applicable 1-hour AAQC at all receptors. Maximum levels of CO are predicted to be about one-third of the AAQC value of 30 ppm at receptors showing the greatest concentrations. The results demonstrate that receptors farther away from the intersection are predicted to exhibit lower CO concentrations. Maximum NO₂ levels range from approximately 50% to 75% of the AAQC value among the measured receptor points.



Among the receptors representing commercial or public sites, receptor 5 (outside the Marathon building, nearest the Sheppard Ave./East Service Road intersection) exhibited the greatest concentrations of CO and NO₂. CO and NO₂ levels were predicted to be 10.8 ppm and 0.145 ppm, respectively. This is expected due to its near proximity to the intersection, and associated idling traffic. Among the residences examined, the two receptors representing homes with entrances nearest Sheppard Ave (Receptors 11 and 13) exhibited the greatest CO and NO₂ levels.

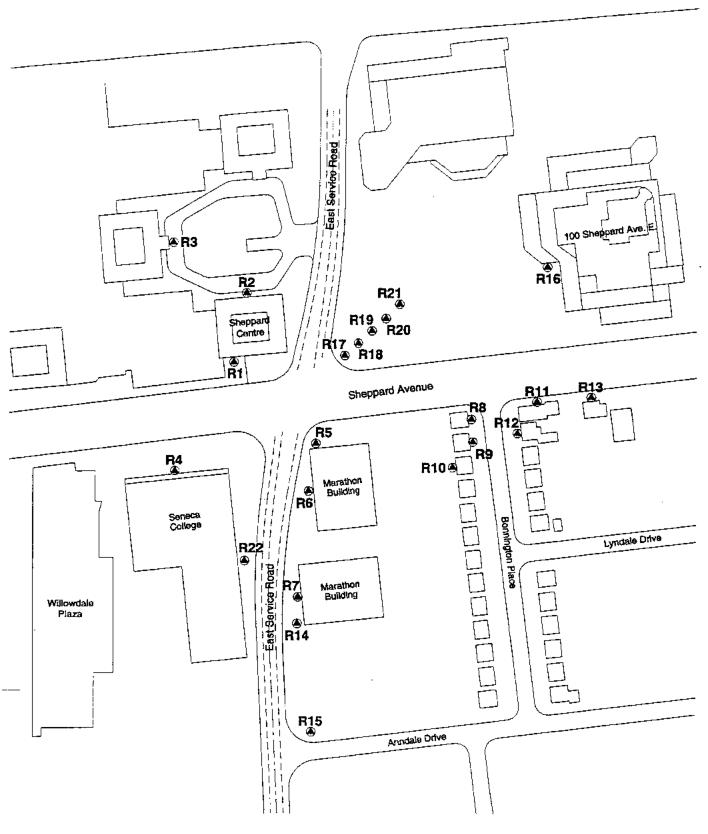
4. CONCLUSIONS

The present study addressed air quality concerns with respect to the proposed construction of the North York East Service Road by numerically modelling vehicular emissions of CO and NO_x for a representative intersection along the proposed route. NO_x consists of several species including NO and NO₂, but only NO₂ is regulated in Ontario. It was predicted that, for the design year 2020, vehicular traffic along the proposed North York East Service Road will not produce ambient levels of CO and NO₂ that exceed the AAQC. This conclusion is based on the results of dispersion modelling under a combination of worst-case meteorological conditions, peak traffic, and high background pollutant levels. As this combination occurs very infrequently, it is expected that the levels of CO and NO₂ at the receptors examined, as well as for the intersection as a whole, will frequently be less than the values predicted in the present report.

5. REFERENCES

- 1. Philpott, S., "MOBILE5C User Guide", Transportation Systems Division, Industrial Pollution Prevention, Environment Canada, 1993.
- 2. "Canadian Climate Norms, 1961 1990, Volume 2, Temperature". Atmospheric Environment Service, Environment Canada, 1992.
- 3. Facsimile to Mr. David S. Chadder, RWDI, from Mr. Paul Hudspith, Cole Sherman and Associates, March 27, 1996.
- 4. Environmental Protection Act, "Ambient Air Quality Criteria Regulation", R.R.O. 1990, Reg. 337 (as amended by O. Reg. 794/94).
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- 7. Facsimile to Ms. Marion Baldwin, RWDI, from Mr. Paul Hudspith, Cole Sherman and Associates, April 15, 1996.
- 8. Ontario Ministry of Environment and Energy, "Air Quality in Ontario 1993".
- 9. Personal Communication between Mr. Mark Vanderheyden, RWDI, and Dr. Robert Bloxam, Ontario Ministry of Environment and Energy, Air Resources Branch, March 2, 1992.
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- 11. Lenner, M., "Nitrogen Dioxide Exhaust Emissions from Motor Vehicles", Atmospheric Environment, Vol. 21, No. 1, pp. 37-43, 1987.
- 12. Innes, W.B., "Effects of Nitrogen Dioxide Levels on Ozone Levels in Metropolitan Regions", Environmental Science and Technology, Vol. 12, pp. 904-911, 1981.

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Location Plan of Air Quality Receptors	True North	Figure No.	1	
	\mathcal{D}	Scale: 1:2000		RWDI
East Service Road - North York, Ont.	Job No. 95-199	Date: Apr. 22,199	3 6	

APPENDIX A

April 4, 1996

Mr. Paul Hudspith, P.Eng. Cole Sherman and Associates 75 Commerce Valley Drive East Thornhill, Ontario L3T 7N9

Re:

North York South Downtown EA East Service Road Alternatives Air Quality Assessment

RWDI Reference Number: 95-199T

Dear Mr. Hudspith:

We have completed our qualitative assessment with regard to air quality impacts of the proposed North York East Service Road, and the following comments have been prepared. Our review is based on the information supplied to us by Cole Sherman including seven road alignment alternatives (M1, M2, M3, T1, T2, T5, and Poyntz (P)) and future peak AM and PM traffic volumes. It was assumed that the future AM/PM peak traffic volumes are common to all alternatives. Our qualitative assessment considered the amount of traffic queuing and the number of residences impacted by the proposed roadways.

Based on our qualitative assessment, the seven alternatives have been ranked as follows, in order of preference:

- 1. Poyntz.
- 2. M1 and M2
- 3. M3
- 4. T2
- 5. T1 and T5

In general, the "midblock" alternatives (M1, M2, M3) will impact fewer residences than the "Tradewind" alternatives (T1, T2, T5), as the East Service Road is routed to the west of the two Marathon office buildings, away from Bonnington Place and the nearby houses. There are no substantive differences among the "midblock" alternatives with regard to air quality impacts. With respect to the impact on the Marathon buildings, M3 is the least desirable of the three "midblock" alternatives, as it is the closest.

Among the "Tradewind" alignments, alternative T2 is more favourable than T1 or T5 from an air quality standpoint, as it does not intersect with Glendora Ave. or Anndale Drive. Tradewind Ave. would remain unchanged, servicing the local streets. A decrease in the number of intersections would reduce the vehicular pollutant emissions (e.g. suspended particulate matter, oxides of nitrogen, carbon monoxide) associated with deceleration, idling and acceleration.

The Poyntz alignment (P) is unique in that it does not intersect with Avondale Ave., instead it curves west to meet Yonge St. This would result in lower vehicular pollutant levels in the residential area east of Bales Ave. compared to the other six alternatives. However, there will be an increase in traffic along Yonge St., as the East Service Road would not carry

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traffic all the way to Avondale Ave. It is expected that the overall effect would be an increase in ambient airborne contaminants at locations adjacent to Yonge St., between the proposed East Service Road(Poyntz Ave.)/Yonge St. intersection and the Yonge St./Avondale Ave. intersection.

Overall, the air quality impacts among the seven alternatives are not vastly different, due to the fact that traffic volumes and speeds are assumed to be the same in each case. No particularly sensitive receptors were identified by Cole Sherman within the study area, thus no alternative was selected based on its impact at a specific location. In all cases, it is predicted that the average pollutant emissions *per vehicle* will decrease in the future-build scenario as a result of a more fuel-efficient vehicle fleet in the future and more stringent emissions standards.

In conclusion, the Poyntz alternative is deemed to be the most favourable of the seven alignments. This alternative intersects only two other roads (Sheppard Ave. and Yonge St.), reducing the number of times vehicles must queue at intersections which, in turn, will reduce the amount of emissions from idling and accelerating vehicles. In addition, the Poyntz alternative impacts the fewest number of residences along its route.

It should be noted that these comments are qualitative in nature; a more detailed assessment of the impact on air quality from the preferred roadway alternative will be conducted using numerical models. The present assessment considered only the number of times vehicles would queue and the number of residences impacted for each alternative; whereas, the impacts based on the length of time spent queuing and the distance of receptors from roadways will be assessed for the selected alternative. The resulting quantitative predictions provide a more refined analysis of ambient pollutant levels.

Please don't hesitate to call if you require additional information with respect to this letter.

Yours very truly,

ROWAN WILLIAMS DAVIES & IRWIN Inc.

David S. Chadder, Hon. B.Sc. Principal

Marion L. Baldwin, B.Sc. (Eng.) Technical Co-ordinator

DSC/MLB/jt

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APPENDIX B

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Input Data to CAL3QHC Disperion Model North York East Service Road

				Ş	Co-ordinates		Effective		Peak a.m Cycle	Cycle	Total Red
	Link #	Link Description	×	Σ	X	72	Width (m)	# of Lanes	Traffic	Length (s	Length (s) Time (s)
Mobile	M	East Service Rd Approach from S	6.0	0	•8.0	-75.0	13	2	770	1	
	M1b	East Service Rd Approach from S	0.0	0	-12.0	-75.0	9.5	-	40		1
	M2	8g	-8.0	-75	-11.0	-133.0	13	2	810		•
	M2b	1	-11.0	-133	æ. 0.ĕ	-500.0	13	2	810		1
	M3	East Service Rd Depart to N	10.0	-	22.0	75.0	13	7	1280		•
	M4	East Service Rd Depart to N	22.0	75	25.0	900.0	13	2	1280	,	
	₩ 2	East Service Rd Approach from N	-2.0	0	13.0	62.0	13	7	755		1
	MSb	8	1.0	0	16.0	0.09	13	-	245		
	M6		13.0	62	20.0	500.0	13	7	1000		
	Μ7	East Service Rd Depart to S	-5.0	0	-16,0	-60.0	13	2	750		1
	MB	East Service Rd Depart to S	-16.0	ဓှ	-19.0	-123.0	13	2	750		•
	M8b	East Service Rd Depart to S	-19.0	-123	-15.0	-500.0	13	2	750	•	1
	ω	Sheppard Ave Approach from W	1.0	φ	-494.0	-59.0	16.5	8	1680		•
	M10	Sheppard Ave, - Depart to E	1.0	ဆု	500.0	51.0	16.5	6	1955	•	,
	M 11	Sheppard Ave Approach from E	0.0	9	500.0	67.0	16.5	65	2480		•
	M12	Sheppard Ave Depart to W	0.0	9	-499.0	-30.0	16.5	ო	1895		1
ldling	Ξ	Sheppard Ave - L. turn north	-30.0	ကု	-199.0	-19.0	4	-	195	110	37
•	2		-29.0	,	-199.0	-27.0	10,5	က	1485	110	37
	<u>6</u>	Sheppard Ave - L. turn south	31.0	ო	249.0	28.0	4	-	140	110	37
	4	Sheppard Ave through (bound W)	31.0	9	249.0	34.0	10.5	ო	2340	110	37
	छ	East Service Rd L. turn east	8.0	6	16.0	60.0	3.5	-	122	110	73
	92	East Service Rd. through (bound S)	2.0	9	13.0	62.0	7	8	878	110	7.3
	13	East Service Rd L. turn west	-3.0	-17	-12.0	-75.0	3.5	-	40	110	73
	<u>8</u> 2	East Service Rd. through (bound N)	3.0	-16	-8.0	-75.0	7	2	770	110	73

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Consulting Engineers Microclimate Specialists

Rowan Williams Davies & Irwin Inc.

AIR QUALITY ASSESSMENT FOR NORTH YORK - SOUTH DOWNTOWN DEVELOPMENT

Report 95-199T-14-REV1 June 19 1996

Submitted to:

COLE SHERMAN AND ASSOCIATES LTD.

By:

ROWAN WILLIAMS DAVIES & IRWIN Inc.
GUELPH, ONTARIO

PROJECT TEAM

David S. Chadder, Hon. B.Sc. Project Manager / Principal

Brian Handy, B.Sc. Project Co-ordinator

Anton E. Davies, Ph.D., P.Eng., QEP Principal

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APPENDICES

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1. INTRODUCTION

Rowan Williams Davies and Irwin Inc. (RWDI) was retained by Cole Sherman and Associates to address air quality concerns resulting from the proposed North York South Downtown Development. The present study included both qualitative and quantitative air quality assessments. The qualitative review considered the amount of traffic queuing and number of residences impacted for three East Service Road alternatives and two West Service Road alternatives. A letter outlining the results of the review was provided to Cole Sherman, and is reproduced in Appendix A. For the quantitative assessment, air quality concerns were addressed by numerically modelling vehicular emissions of carbon monoxide (CO) and oxides of nitrogen (NO_x) for selected roadways and intersections, including Yonge Street, in the proposed development.

The following report presents the methodology, results and conclusions of the numerical modelling assessment. A summary of the findings of this study was prepared into a letter report. A copy of this report can be found in Appendix B.

2. METHODOLOGY

The purpose of this assessment was to determine the impact of emissions from vehicles using roadways adjacent to the North York South Downtown Development for the build year 2021. The assessment was conducted using both worst-case meteorological and traffic assumptions. Figure 1 summarizes the steps of the methodology. The emissions examined were tailpipe emissions of carbon monoxide (CO) and nitrogen dioxide (NO_x) from both cars and trucks idling at nearby intersections and travelling along adjacent roadways. These pollutants both have readily available emissions data and provincial criteria as established by the Ontario Ministry of the Environment and Energy (MOEE). The analysis concentrated on the roadways and intersections with the highest predicted traffic volumes, (i.e., evening rush-hour period).

2.1 Vehicular Emission Analysis

Environment Canada's MOBILE5C vehicular emissions model was used to determine emission rates of NO_x and CO [1]. This model is a modification of the U.S. Environmental Protection Agency's (EPA) MOBILE5. The modified version better reflects the emission's performance of Canada's automobile fleet. Table 1 presents the key inputs into the MOBILE5C model. The design year was 2021; however, 2020 was modelled as this is the last year in the MOBILE5C dataset for which emissions information are currently available. Any differences in emissions are expected to be minimal over these two successive years.

Table 1: MOBILE5C Input Parameters

Design Year:

2020, last year in MOBILE5C dataset for which emissions information is available.

Ambient Temperature:

-4.5°C, based on the mean daily temperature at Downsview Airport for the coldest month of the year (i.e., January) [2].

MOBILE5C default values:

default vehicle mix	light-duty gas vehicles	57.0%
	light-duty gas trucks	31.9%
	heavy-duty gas vehicles	3.1%
	light-duty diesel vehicles	0.2%
	light-duty diesel trucks	0.6%
	heavy-duty diesel vehicles	7.8%
	(includes buses)	
	motorcycles	0.4%

Ontario vehicle statistics; and default cold-start vehicle fraction as given by the MOBILE5C manual.

Vehicle speeds:

Default vehicle speed (32 km/h) for urban roads as given by the MOBILE5C model.

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2.1.2 Vehicular CO and NO_x Emission Rates

The vehicular CO and NO_x emission rates obtained from the MOBILE5C model are summarized in Table 2.

Table 2: Predicted Vehicle Emission Rates

Emission Source	Pollutant Er	mission Rate
	co	NO _x
Idling (g/veh/hr)	333	7.8
Mobile (g/veh/km)	19.1	1.28

2.2 Air Quality Criteria

Emissions from vehicles are currently regulated by Transport Canada (Federal) regulations. Provincial regulations do not directly control the emissions from vehicles or pollutant concentrations arising from vehicular activities. However, Ontario Regulation 337 provides desirable ambient air quality objectives under which emissions from vehicles can be evaluated [3]. Table 3 presents Ontario's Ambient Air Quality Criteria (AAQC) for 1-hour CO and 1-hour NO₂.

Table 3: Ontario's Ambient Air Quality Criteria

Poliutant	Averaging Period	Air Quality Criteria (ppm)
Carbon Monoxide (CO)	1-hour	30
Nitrogen Dioxide (NO ₂)	1-hour	0.20

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2.3 Dispersion Analysis

The vehicular emissions obtained from the MOBILE5C model were used to predict worst-case concentrations of NO_x and CO at selected areas using dispersion modelling techniques. The dispersion simulation model used was CAL3QHC. This model, which was originally developed by the U.S. Environmental Protection Agency, was designed specifically for modelling the dispersion of emissions from motor vehicles travelling near roadway intersections [4]. By including emissions from idling vehicles, CAL3QHC represents a reliable model for predicting pollutant concentrations near signalized intersections where idling vehicles interact with moving vehicles. The model has been accepted by the Ontario Ministry of the Environment and Energy—for use in roadway environmental assessments.

2.3.1 Modelled Scenario

The air quality impact due to highway emissions are, among other factors, dependant upon the traffic volume, vehicle speed, and the roadway cross-sections. The modelled roadway scenario was based on the design plan review drawing entitled East Service Road #3 (Midblock)/West Service #1 as supplied by Cole Sherman [5].

2.3.2 Input Parameters for CAL3QHC Dispersion Model

The CAL3QHC model required the following input parameters to assess the pollutant levels:

i) Roadway and Receptor Coordinates

Figure 2 illustrates the roadways that were modelled. Also shown in Figure 2 are the receptor locations at which pollutant levels were predicted. The receptors were located at least 3 m from the edge of the roadways. These locations are outside of the mixing zone created by the wake of moving vehicles. For simplicity, all roadways and receptors were assumed to be located on the same plane (i.e., grade level). This would produce conservative results.

ii) Traffic Volumes and Traffic Light Cycles

Morning and evening peak hourly traffic volumes for the adjacent roadways were supplied by Cole Sherman, together with the traffic light cycles at the associated intersections [6]. Analysis of the traffic data indicated that maximum traffic volumes occurred during the evening peak period; therefore, hourly traffic volumes from the evening rush-hour were used in the dispersion analysis. The traffic volumes used in the study are shown in Appendix C along with the coordinates for each roadway link.

iii) Surface Roughness

Mechanical turbulence is generated by air flowing over a surface. This turbulence influences the dispersion of pollutants near the surface. The modelling purposes the study area was considered to be an office area and, therefore, a generic roughness (Z_p) equal to 175 cm (city land use/offices) was selected.

iv) Meteorological Conditions

Worst-case meteorological conditions used in the CAL3QHC dispersion analysis are documented in Table 4.

Table 4: Meteorological Inputs into the CAL3QHC Model

Parameter	1- Hour Meteorological Conditions
Pasquill Stability Class	Class E
Wind Speed (m/s)	1.0
Mixing Height (m)	300

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v) Background Concentrations

As part of the assessment of vehicle emissions, background concentrations of the contaminants within the ambient air were required. Maximum background levels were added to the levels predicted by CAL3QHC for comparison with the provincial AAQC. Table 5 presents the maximum background levels obtained from the MOEE's monitoring station at Hendon Avenue (Yonge/Finch) Station (ID Number 34020) [8]. The latest available data were for the 1992 calender year.

Table 5: Maximum 1-hour Concentrations, MOEE's Hendon Avenue Station, 1992.

Pollutant	Averaging Period
	1-hour Maximum (ppm)
Carbon Monoxide (CO)	6
Nitrogen Dioxide (NO₂)	0.09
Oxides of Nitrogen (NO _x)_	0.50
Ozone (O ₃)	0.106

The ozone data presented in Table 5 is required to predict the worst-case NO_2 concentrations. Vehicles emit NO_x (approximately 95% nitric oxide (NO) and 5% NO_2) and the NO component of the NO_x emission reacts photochemically with O_3 to form NO_2 . The reaction rate is restricted by the availability of O_3 and light. The Ozone Limiting Method was used to predict worst-case NO_2 concentrations [9]. Equations 1 and 2 define the method.

$$if [O_3]_B < 0.95 [NO_x]_R [NO_2]_R = A [NO_x]_R + [O_3]_B + [NO_2]_B$$
 (1)

$$if [O_3]_8 \ge 0.95 [NO_x]_R [NO_2]_R = A [NO_x]_R + B(1-A)[NO_x]_R + [NO_2]_B$$
 (2)

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where $[O_3]_{\theta}$	=	the background ozone level;
$[NO_x]_B$	=	total NO _x contribution from vehicles at the selected receptor location;
[NO ₂] _#	=	the predicted worst-case NO ₂ concentration at the receptor location;
$[NO_2]_8$	=	the background NO ₂ concentration;
Α	#	the fraction of $\mathrm{NO_x}$ emitted vehicle exhaust as $\mathrm{NO_2}$ (assumed to be 0.05); and
В	=	the fraction of NO_{x} converted to NO_{2} as it disperses towards the receptors
		(assumed to be 0.10).

In Equation 1, the maximum values used for NO_2 and O_3 are assumed to occur concurrently (i.e., NO_2 plus O_3 , as shown in Table 5).

3. RESULTS AND CONCLUSIONS

Table 6 summarizes the results of the CAL3QHC dispersion modelling. The table shows the predicted 1-hour CO and NO₂ concentration at each receptor, together with the relevant 1-hour AAQC. The predicted CO values include the maximum 1-hour background concentrations for 1992 as shown in Table 5 (i.e., 6 ppm CO). The predicted NO₂ values were calculated using the Ozone Limiting Method as described in Section 2.3.3 (v). The predicted NO₂ values include the maximum 1-hour background concentration of 0.09 ppm.

Table 6: Results of Dispersion Modelling

Receptor Number	1-hour CO (ppm)	1-hour NO ₂ (ppm)	Receptor Number	1-hour CO (ppm)	1-hour NO ₂ (ppm)	Receptor Number	1-hour CO (ppm)	1-hour NO ₂ (ppm)
1	19.3	0.17	16	23.0	0.17	31	15.1	0.15
2	17.2	0.16	17	19.6	0.16	32	12.8	0.15
3	19.3	0.16	18	22.1	0.17	33	11.6	0.15
4	19.1	0.16	19	20.8	0.17	34	10.6	0.15
5	20.7	0.17	20	19.7	0.16	35	18.2	0.16
6	21.3	0.16	21	19.2	0.16	36	14.8	0.15
7	18.5	0.16	22	14.6	0.15	37	13.1	0.15
8	20.6	0.16	23	12.7	0.15	38	12.3	0.15
9	19,1	0.16	24	11.6	0.15	39	18.1	0.16
10	20.2	0.16	25	16.1	0.16	40	17.2	0.16
11	19.5	0.16	26	12.9	0.15	42	17.5	0.16
12	21.4	0.17	27	11.4	0.15	42	17.7	0.16
13	20.0	0.16	28	17.9	0.16	43	13.7	0.15
14	22.1	0.17	29	13.3	0.15	44	13.8	0.15
15	18.9	0.16	30	12.0	0.15			
AAQC	30.0	0.20		30.0	0.20		30.0	0.20

The results of the dispersion modelling indicate that the impact of vehicle emissions of CO and NO₂ are all below their applicable 1-hour AAQC at all receptors. This is consistent with monitoring data collected by the MOEE in 1992 which showed that there were no readings in excess of the 1-hour CO and NO₂ criteria at any of their monitoring stations. This includes stations located next to heavily-used roadways such as Hendon Avenue (Yonge/Finch), 381 Yonge Street, and the Evans Street/Arnold Avenue station in Etobicoke, which is located next to the Queen Elizabeth Way.

In summary, it is unlikely that, for the design year 2021, vehicular traffic in the proposed North York South Downtown Development will produce ambient levels of CO and NO₂ that will exceed the AAQC. This conclusion is based on the results of dispersion modelling under worst-case meteorological and traffic conditions and maximum background pollutant levels.

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4. REFERENCES

- 1. Philpott, S., "MOBILE5C User Guide", Transportation Systems Division, Industrial Pollution Prevention, Environment Canada, 1993.
- 2. "Canadian Climate Norms, 1961 1990, Volume 2, Temperature". Atmospheric Environment Service, Environment Canada, 1992.
- 3. Regulation 337 Under The Ontario Environmental Protection Act, R.S.O. 1992.
- "CAL3QHC A Modelling Methodology for Predicting Pollutant Concentrations Near Roadway Intersections", Schattanek, G., Kahng, J. and Stratou, T., Parsons Brinckerhoff Quade and Douglas, Inc. New York 10119, September 1990.
- Memorandum from Cole Sherman to RWDI, March 9, 1995.
- Facsimile from Cole Sherman to RWDI, March 16, 1995.
- Personal communication between Mr. Brian Handy, RWDI, and Mr. Chris Murray of Cole Sherman, March 15, 1995.
- 8. Ontario Ministry of the Environment and Energy, "Air Quality in Ontario 1992".
- Personal Communication between Mr. Mark Vanderheyden, RWDI, and Dr. Robert Bloxam,
 Ontario Ministry of the Environment and Energy, March 2, 1992.

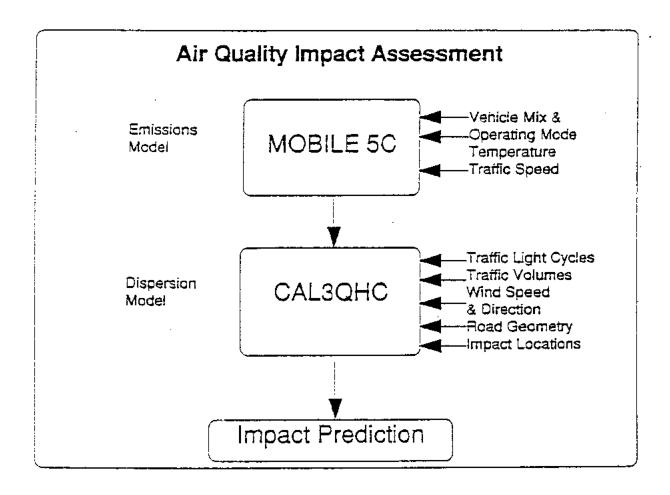


Figure 1: Numerical Modelling Methodology

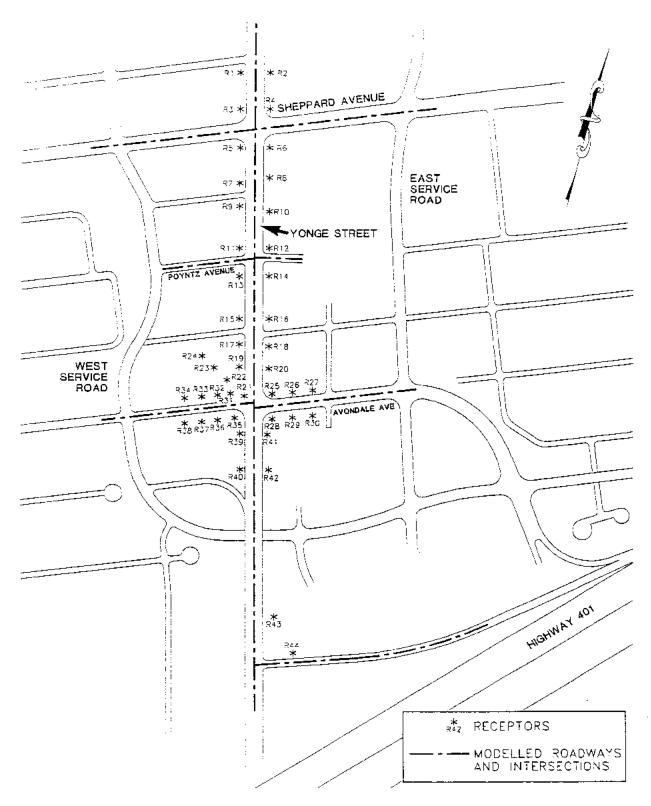


Figure 2: Modelled Roadways and Receptor Locations Approximate Scale: 1:5000

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APPENDIX A

January 24, 1995

Mr. Chris Ricketts, P.Eng. Cole Sherman and Associates 75 Commerce Valley Drive East Thornhill, Ontario L3T 7N9

Re: North York South Downtown Secondary Plan Review/Class EA Air Quality Assessment RWDI Reference Number 95-199T

Dear Chris:

We have reviewed the roadway alternatives for the proposed North York South Downtown Development and the following comments have been prepared. Our review has been qualitative and is based on the information supplied to us by Cole Sherman and included mapping for the three East Service Road alternatives: Numbers 1, 2 and 3A, and the two West Service Road alternatives: Numbers 1 and 2 and peak (AM and PM) traffic volumes. It was assumed that the AM/PM peak traffic volumes are applicable to all alternatives and that the optimum level of service (i.e., light cycle time, traffic speeds, design for traffic volumes, pedestrian crossings) at the intersections will be incorporated into the final project design for the preferred alternative. Our qualitative assessment considered the number of vehicle movements, the amount of traffic queuing and the number of residences impacted by the proposed roadways.

In general, the new service roads, when completed, are expected to divert traffic away from Yonge Street. From an air quality context, contaminant levels along Yonge Street are expected to decline due to a predicted reduction in the number of vehicle movements and in vehicular emissions, the latter as proposed by the federal government. The areas to the east and west of the downtown, where the service roads are planned, will experience a small increase in ambient levels of airborne contaminants (e.g., suspended particulate matter, oxides of nitrogen, carbon monoxide) related to vehicular emissions. Overall, the net effect of the proposed roadway development will be positive for the Yonge Street area and marginally worse for residents near the service roads.

With respect to the two West Service Road Alternatives, where the curvature of the road north of Florence Avenue varies, there are no substantive differences between the alternatives, which would improve or adversely impact the local air quality. The number of residences being impacted is similar and the traffic volumes and speeds would be the same.



With respect to the proposed East Service Road, Alternative Number 3A (Midblock) is deemed to be the most favorable of the three alternatives. In general terms, Alternative 3A (Midblock) includes a ramp that connects traffic from the westbound Highway 401 to the northbound East Service Road by going around the intersection at Avondale Avenue. This Alternative also has a reduced number of intersections along Avondale/Florence Avenues. When combined, these two factors offer potentially less queuing which, in turn, will reduce the amount of emissions from idling and accelerating vehicles.

It should be noted that these comments are qualitative in nature; a more detailed assessment of the impact on air quality from the preferred roadway alternative will be conducted using numerical models.

Please don't hesitate to contact me if you require additional information with respect to this letter.

Yours very truly,

ROWAN WILLIAMS DAVIES & IRWIN Inc.

David S. Chadder, Hon. B.Sc. Principal

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APPENDIX B

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March 22, 1995

Mr. Chris Murray
Environmental Planner
Cole Sherman and Associates
75 Commerce Valley Drive Street
Thornhill, Ontario
L3T 7N9

Re: North York Class Environmental Assessment Air Quality Assessment

RWDI Reference Number: 95-199T

Dear Chris:

We have completed our assessment of the air quality impact from roadways associated with the North York South Downtown Development. This letter report provides a brief outline of the methodology, results and conclusions. A more detailed report will follow at a later date.

The purpose of this assessment was to determine the worst-case impact of emissions from vehicles using roadways adjacent to the North York South Downtown Development for the build year 2021. The emissions examined were tailpipe emissions of carbon monoxide (CO) and nitrogen dioxide (NO_x) from both cars and trucks idling at nearby intersections and travelling along adjacent roadways. These pollutants both have readily available emissions data and provincial criteria. Our analysis concentrated on the roadways and intersections with the highest predicted traffic volumes, (i.e., pm rush-hour period).

Environment Canada's MOBILE5C vehicular emissions model was used to determine vehicular emission rates of NO_x and CO. The vehicular emissions obtained from the MOBILE5C model were used to predict worst-case concentrations of NO₂ and CO at selected pedestrian areas (receptors) using dispersion modelling techniques. A total of 44 receptors were selected for analysis. The dispersion simulation model used was CAL3QHC. This model, developed by the U.S. Environmental Protection Agency, was designed specifically for modelling the dispersion of emissions from motor vehicles travelling near roadway intersections. By including emissions from idling vehicles, CAL3QHC represents a reliable model for predicting pollutant concentrations near signalized intersections where idling vehicles interact with moving vehicles. The model has been accepted by the Ontario Ministry of the Environment and Energy (MOEE) for use in roadway environmental assessments.

March 22, 1995 Mr. Chris Murray Cole Sherman and Associates

Page 2

The results of the dispersion modelling indicate that the impact of vehicle emissions of CO and NO₂ are all below their applicable 1-hour Ambient Air Quality Criteria (AAQC) at all receptors. This is consistent with monitoring data collected by the MOEE in 1992 which showed that there were no readings in excess of the 1-hour CO and NO₂ criterion at any of their monitoring stations. This includes stations located next to heavily-used roadways such as Hendon Avenue (Yonge/Finch), 381 Yonge Street, and the Evans Street/Arnold Avenue station in Etobicoke, which is located next to the Queen Elizabeth Way.

In summary, it is unlikely that vehicular traffic in the proposed North York South Downtown Development will produce impacts of CO and NO₂ that exceed AAQC.

We would be happy to respond to any questions or comments that you might have - feel free to contact either of the undersigned.

Yours very truly,

ROWAN WILLIAMS DAVIES & IRWIN Inc.

David S. Chadder, Hon. B.Sc. Principal

Brian Handy, B.Sc. Project Co-ordinator

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APPENDIX C



NORTH YORK SOUTH DOWNTOWN DEVELOPMENT

YONGE STREET NORTH/SOUTH THROUGH LINKS		YONGE STREET NORTH/SOUTH QUEUE LANES C Total COORDINATES				TRAFFIC						
	X1	COORI	INATES	5 Y2	TRAFFIC Veh/hr		Width (m)	Х1	-00RD	X2	Y2	Veh/hr
	.,.			-								
NORTH OF SHEPPARD						YONGE AND SHEPPARD						
Northbound Link	10.0	1.0	7.0	175.0	2140	Northbound Through and Right Turn Lane (3)	11,1	5.6	-20	5.6	-155	2090
Southbound Link	-7.0	-1.0	-7.D	175.0	2590	Northbound Left Turn Lane (1)	3.7	0	-20	0	-60	410
SHEPPARD TO POYNTZ						Southbound Right Turn Lane (1)	3.7	-10	20	-11	81	290
						Southbound Through Lanes (3)	11.1 3.7	-3 4	20 21	-3 6	155 81	22 2 0 80
Northbound Link	7.0 -7.0	1.0 -1.0	70 -70	-175.D -175.D	2500 2780	Southbound Left Turn Lane (1)	3.1	•	٠.	3	O1	50
Southbound Link	-1.0	1.5	-, 🗸	-11 5.5	2.00	YONGE AND POYNTZ						
POYNTZ TO AVONDALE						Northbound Through and Right Turn Lanes (3)	11.4	8.5	-186	9.5	-37t	2460
Northbound Link	7.0	-175.0	7.0	-371.0	2580	Northbound Left Turn Lane (1)	3	1.5	-186	0	-228	120
Southbound Link	-7.0	-175.0	-7 Q	-371.D	2870					_		
						Southbound Through and Right Turn Lane (3)	11. 4 3	-7 -1.5	-166 -166	-7 0	-1 -106	2680 20
AVONDALE TO NEW INTERSECTION	IN					Southbound Left Turn Lane (1)	3	-1.3	-100	•	-100	
First Northbound Link	17.0	-549.0	50.0	-718.0	2350	YONGE AND AVONDALE						
Second Northbound Link	7.0	-371.0	17.0	-549.0	3D10	Northbound Through Lanes (3)	11.1	8.5	-394	8.5	-718	2560
First Southbound Link	-7.0	-371.0	-3.0	-491.0	3440	Nonnbound Left Tem Lane (1)	3.7	1.5	-395	0	-455	200
Second Southbound Link	-3.0	-491.0	36.0	-725.0	2580	Northbound Right Turn Lane (1)	3.7	16	-394	15	-482	250
						Southbound Through and Right Turn Lane (3)	11.1	-8.5	-354	-7	-175	2850
SOUTH OF NEW INTERSECTION						Southbound Left Turn Lane (1)	3.7	-1.5	-352	ò	-293	150
Northbound Link	50.0	718.0	50.0	-856.0	1400							
Southbound Link	36.0	-725.0	36.0	-855.0	2580	YONGE AND NEW INTERSECTION						
						Northbound Through Lanes (2)	7.4	49	-735	50	-856	1400
YONGE STREET EAST/WE	ST TH	ROUGH	LINKS			Southbound Through Lanes (2)	7.4	35	-717	-4	-482	2580
SHEPPARD AT YONGE						YONGE STREET EAST/N	NEST QUEU	E LANI	ES			
	0.0	0.0	207.0	24.0	3450	YONGE AND SHEPPARD						
East Link West Link	0.0	0.0	-178.0	-18.0	2950	TOMBE AND SHEFF AND						
TAGE STORE						Eastbound Through and Right Turn Lanes (3)	11.1	-16	-11	-162 -76,5	-24.5 -8	1450 150
POYNTZ AT YONGE						Eastbound Left Turn Lane (1)	3.7	-16.5	·3.5	-10,5	-0	130
East Link	0.0	175.0	80.0	-175.0	260	Westbound Through and Right Turn Lanes (3)	11.1	21	12	2:3	32	1280
West Link	0.0	-175.0	-135.0	-191,3	270	Westbound Left Turn Lane (1)	3.7	21 5	4	80	8.5	120
AVONDALE AT YONGE						YONGE AND POYNTZ						
						Control of Top Lane (4)	3.7	-15	-178.5	-123.5	-161	20
East Link West Link	0.0		216.0 -164.0		770 960	Eastbound Left Turn Lane (1) Eastbound Right Turn Lane (1)	3.7	-14.5	-182	-123.3	-162.5	
1753 CAR	0.0	0,		544.4	***							
NEW INTERSECTION AT YONGE						Westbound Left and Right Turn Lane (1)	3.8	16	-172.5	31	-176.5	210
Sast Link	50.0	-7180	200.0	-710,0	1600	YONGE AND AVONDALE						
						Control of Top Leasts	3.7	-25	-175 5	-346.5	-388.5	110
						Eastbound Left Turn Lane (1) Eastbound Right Turn Lane (1)	3.7	-24	-379.5		-391.5	
						Westbound Left Turn Lanes (2)	7.4 3.7	18 18	-372 -366	39 39	-363 -359	370 190
						Westbound Right Turn Lane (1)	J.1		500		224	
						YONGE AND NEW INTERSECTION						
						 Westbound Left Turn Lanes (2)	7,4	58	-721	200	-710	650
						Westbound Right Turn Lane (1)	3.7	58	-714	221	-602	950